

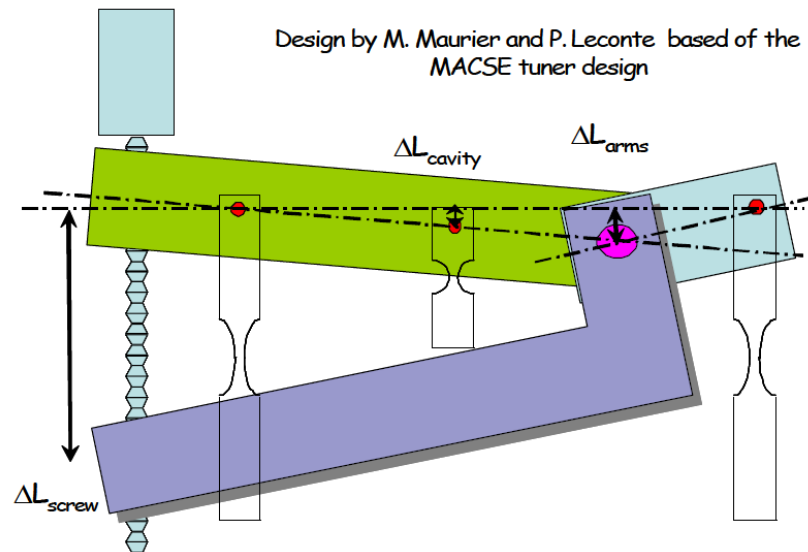
TUNER DEVELOPMENT AT CEA-SACLAY

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CEA-Irfu, Saclay

Cold tuning system design started at Saclay for the MACSE cryomodules, 1.5 GHz CW e- linac (3-cells and 5-cells cavities) : need for cold tuner, operating in LHe.

Followed in the early 90's by the TTF (Saclay-I) with an asymmetric, simplified lever arm design

Mechanical Principle of Present TTF Tuner



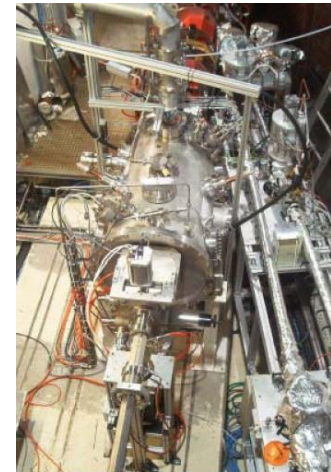
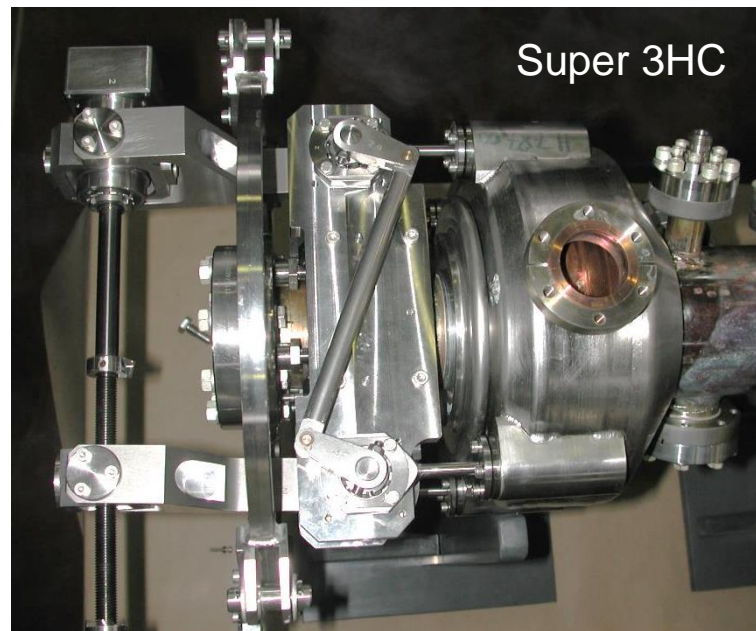
- Double lever system ratio ~1:17
- Stepping motor with harmonic drive gear box
- Screw-nut system : lubricant treatment (balzers Balinit C coating) for working at cold and in vacuum
- $\Delta Z = \pm 5$ mm and $\Delta f = \pm 2.6$ MHz
- Theoretical resolution : $\delta z = 1.5$ nm !

P. Bosland

Addition of piezo actuators by DESY, operated since the beginning of TTF, basis of the XFEL tuner

- Then SOLEIL cavities (352 MHz) : symmetric dual lever arms prompted by the tuning range and dimensions
- Elettra Trieste and PSI-SLS Super3-HC cryomodules dual single-cell 1.5 GHz, scaled down version of Soleil tuner. Total of 4 tuners in operation since 2003

Heavy use of tuner on circular machines, full range operation on a daily basis

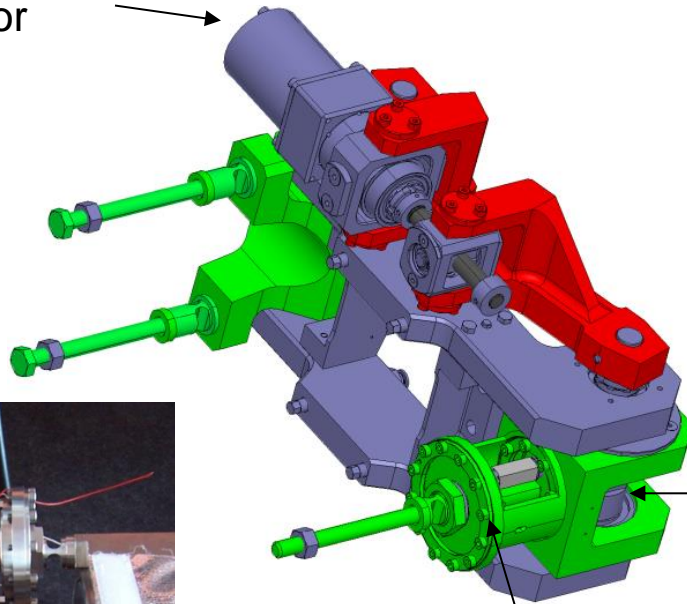


In the 6th European Framework Program, a new cold tuner implemented with fast piezoelectric actuators has been developed (CARE/SRF) based on the experience gained from the former cold tuner designs. This new tuner should meet the needs for Lorentz forces or microphonics compensation on the 9-cell elliptical cavities used in the future linear collider (ILC) or Free Electron Laser linacs

Design choices

- Excentric rods transfer rotation into displacement like Saclay SR cavities tuners
- Achieve a stiffness at least 10x the stiffness of the cavity
- Remove the neutral point from the tuning range to suppress backlash : equivalent to choose to only lengthen the cavity. The room temperature frequency must be shifted accordingly
- Always use increasing forces to tune the cavity to higher frequency (for both slow tuner and piezo parts)
- Tune the cavity to operation frequency at cold by using a fraction of the positive tuning range
- Use the cavity reaction force to preload the PZTs (aiming at $F_{\text{preload}} > 500 \text{ N}$). No other adjustment
- Typical fast tuning range +1kHz to compensate for the LFD i.e. 3 micrometers cavity lengthening

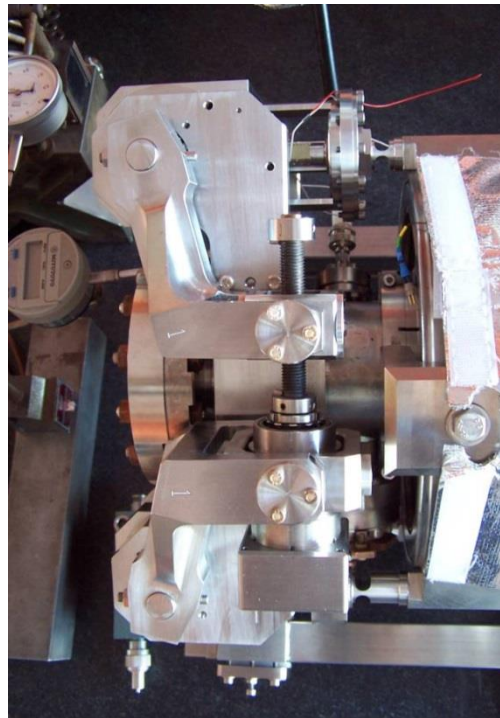
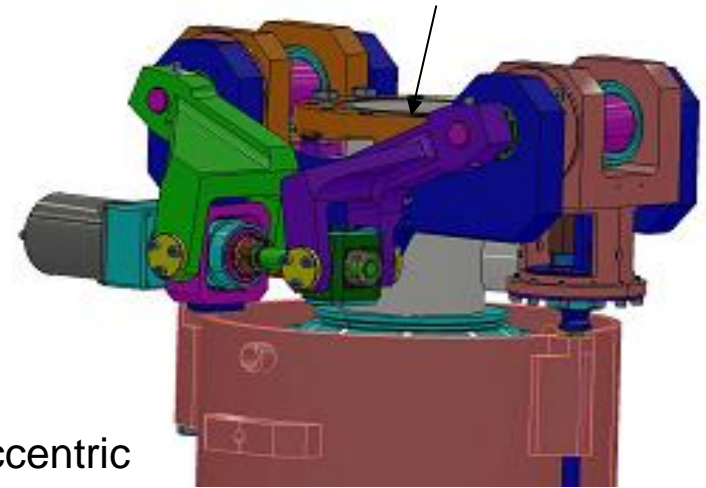
Stepper motor



Eccentric shaft

Dual piezo support

Cavity flange



Stiff tuner (meas. 35kN/mm)

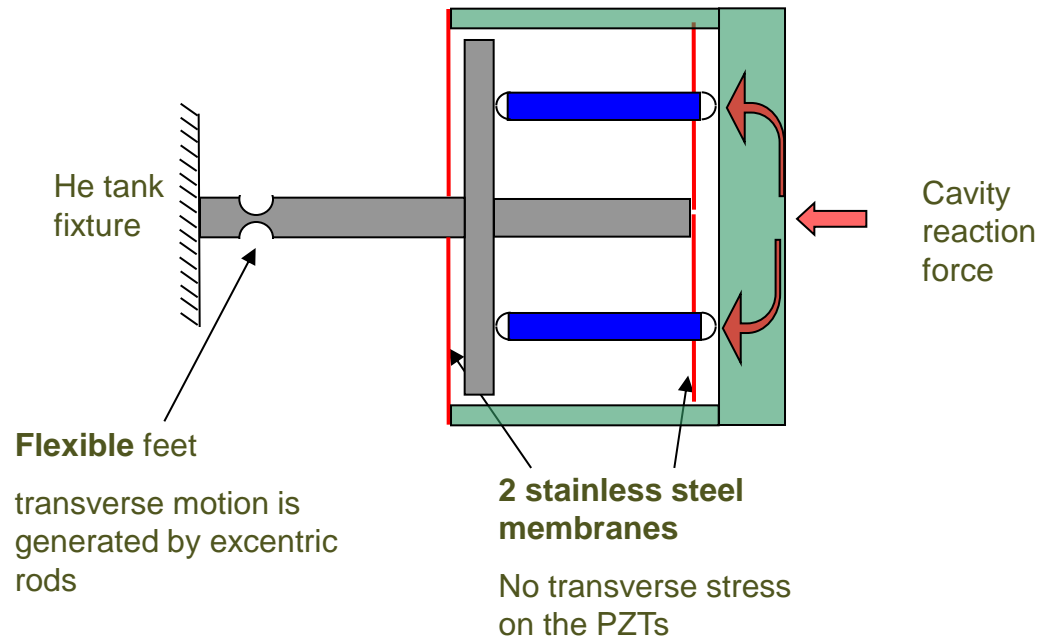
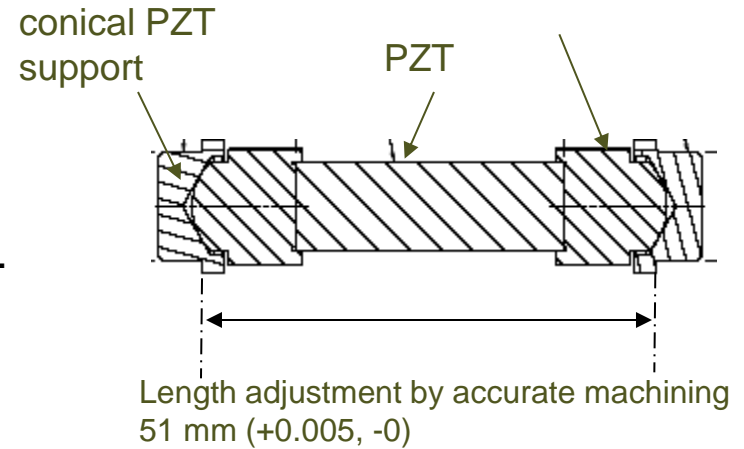
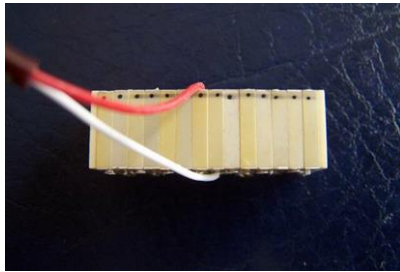


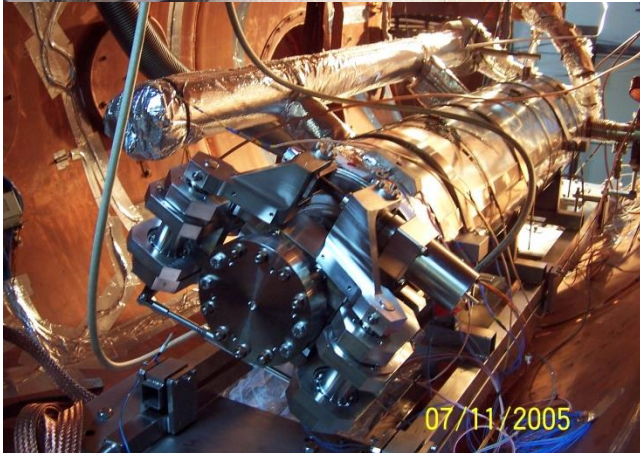
SACLAY-II PIEZO SUPPORT

We were worried about damaging piezos

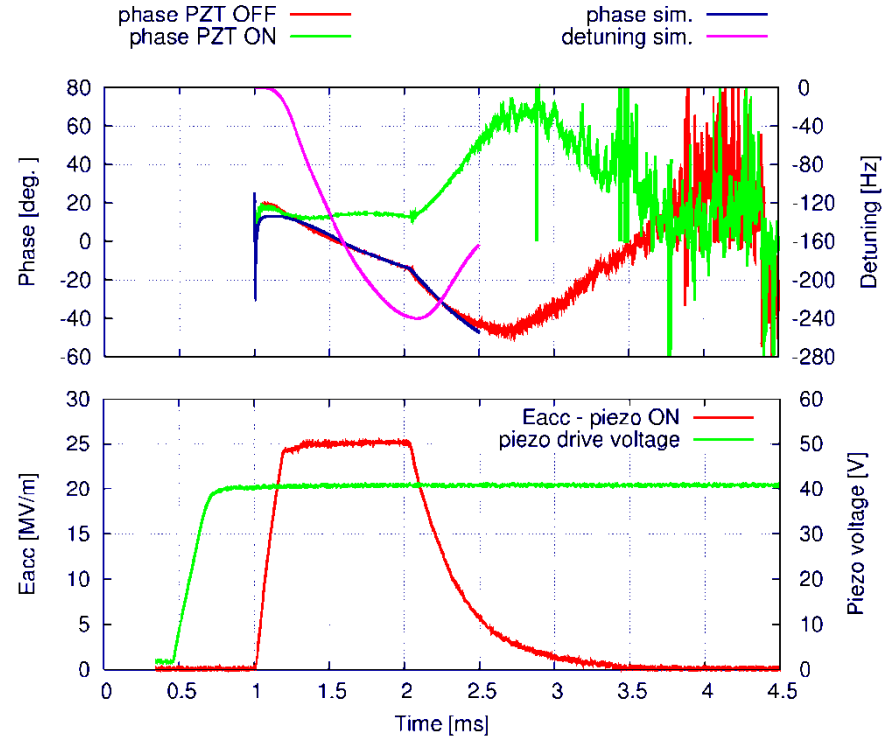
- due to shear and bending forces
- due to insufficient preload

2 piezos were considered as safer than one...





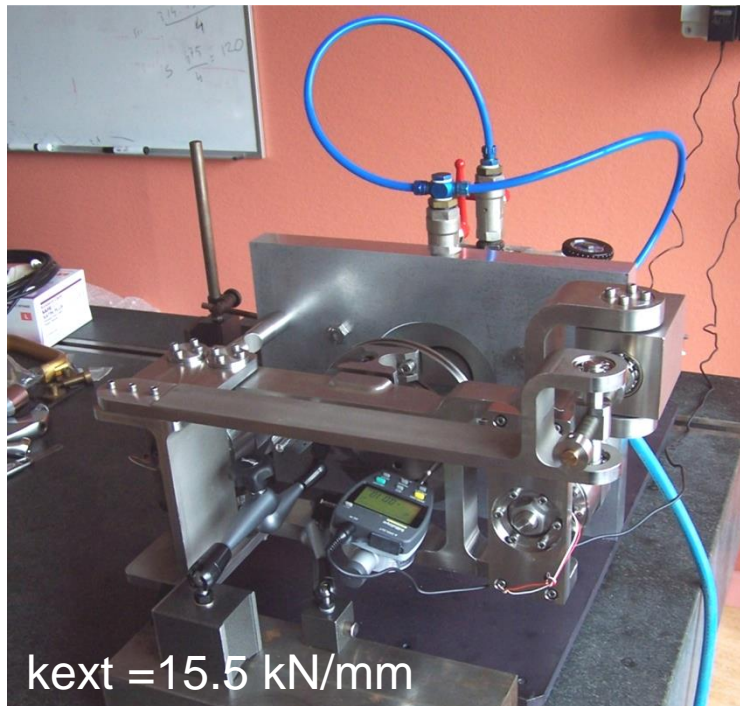
Tested on C45 DESY 9-cell in
CryHoLab.
Pulse operation at $E_{acc} = 25$ MV/m



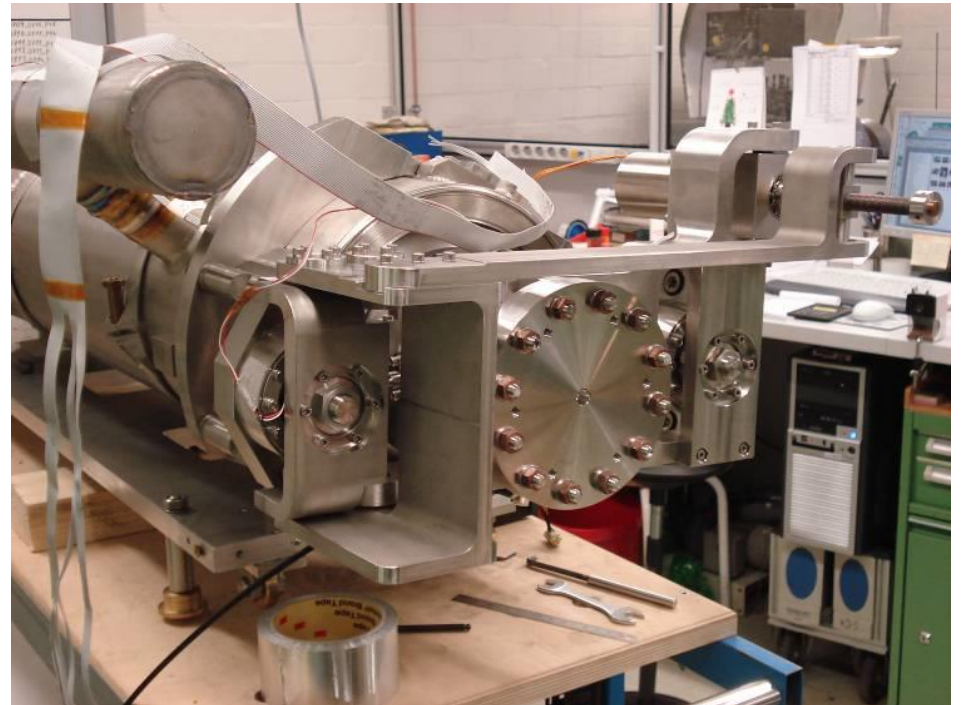
- LFD compensation achieved (20Hz estimated residual detuning)
- But difficult to have both piezo loaded correctly simultaneously in the same support

- for 1.3 GHz 9-cell cavities
- asymmetrical , with simpler structural parts to reduce cost (like Saclay-I, TTF and XFEL tuner) aiming at reducing the cost
- Still 2 piezos this time not in the same support but one on each side of the flange
- The piezo support was also using stainless steel membranes to prevent shear forces (coaxial design) -> still expensive

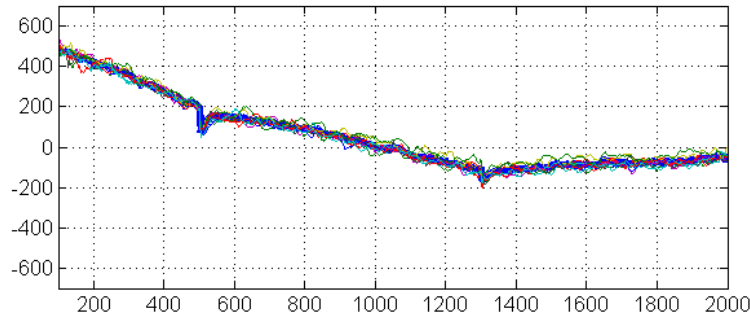
Stiffness measurement on pneumatic jack



Preparation for the pulsed test in Chechia @ DESY (2007)



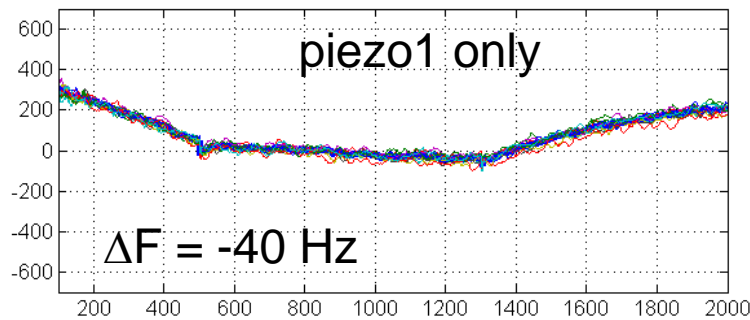
SACLAY-IV LFD COMPENSATION IN CHECHIA



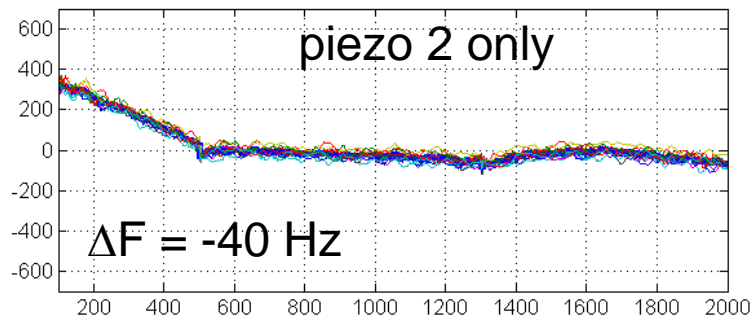
compensation OFF

$$\Delta F = -300 \text{ Hz}$$

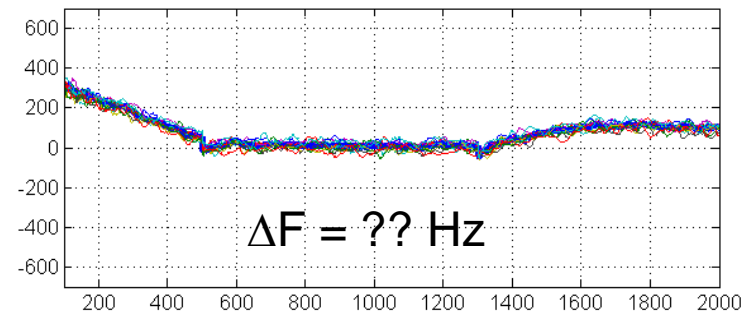
25 MV/m in
Chechia
(w/ L. Lilje)



compensation ON

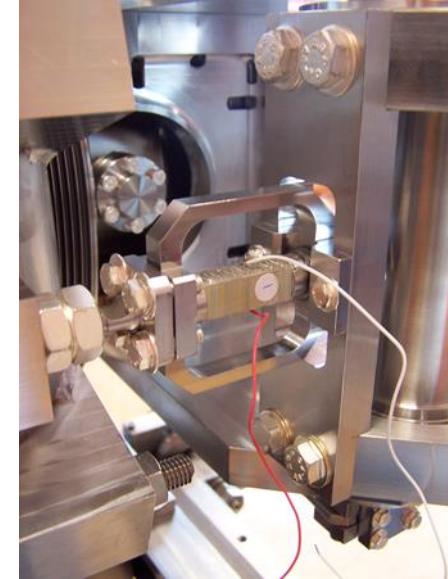
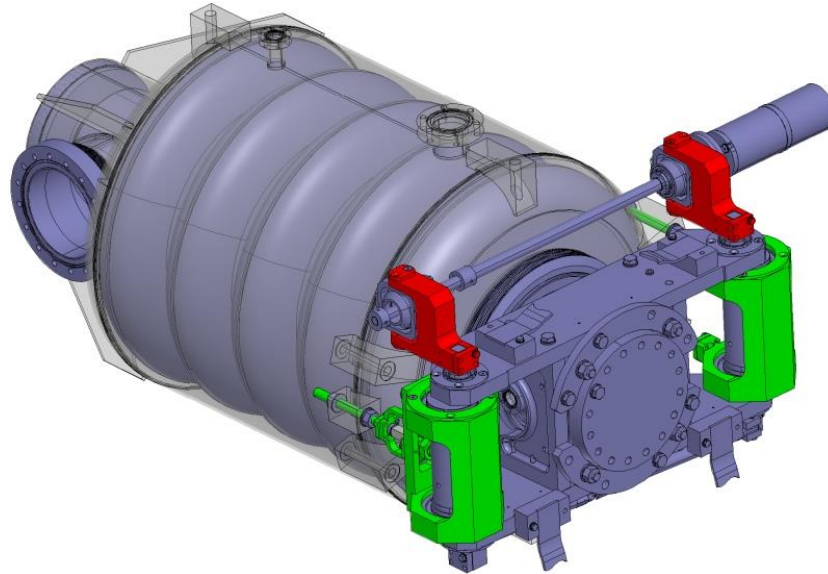


Both piezos



Good performance for piezo LFD compensation

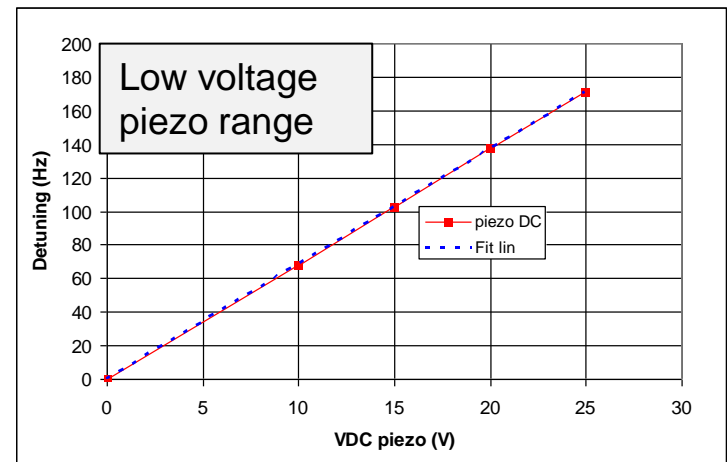
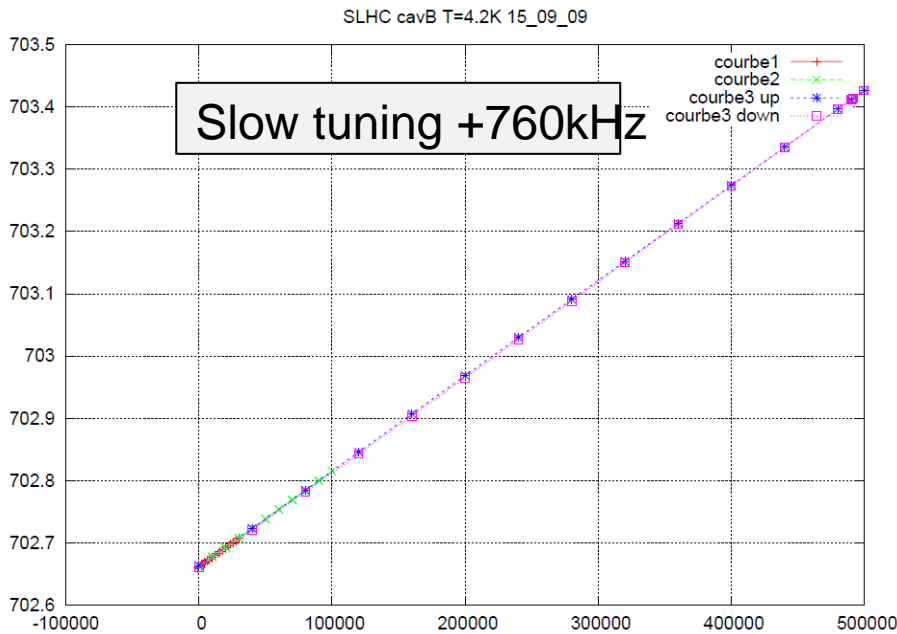
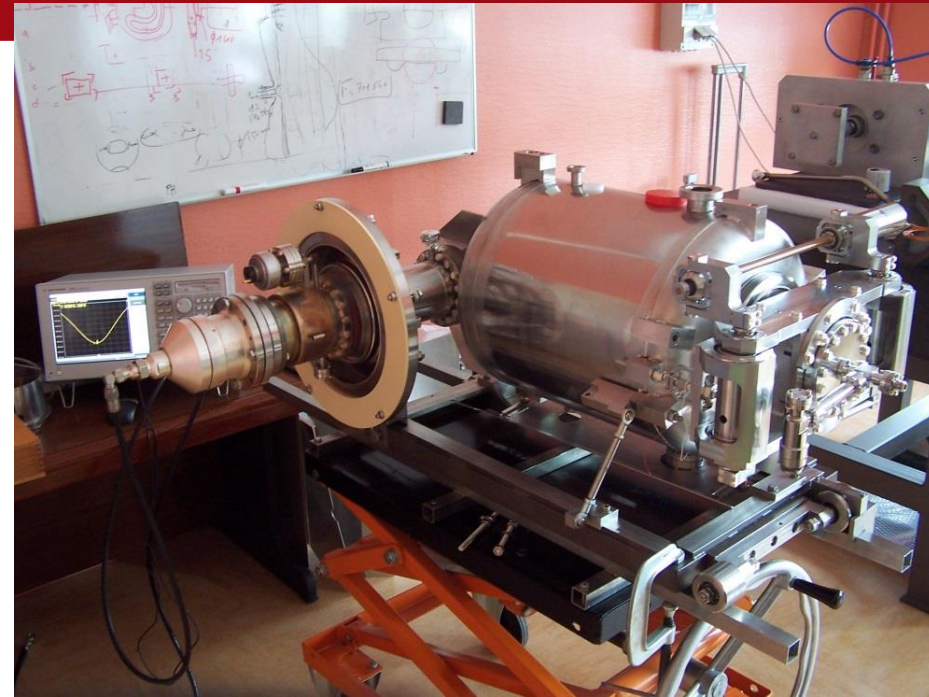
Drawbacks: cost of the piezo supports, relying on the cavity springback force is not very practical



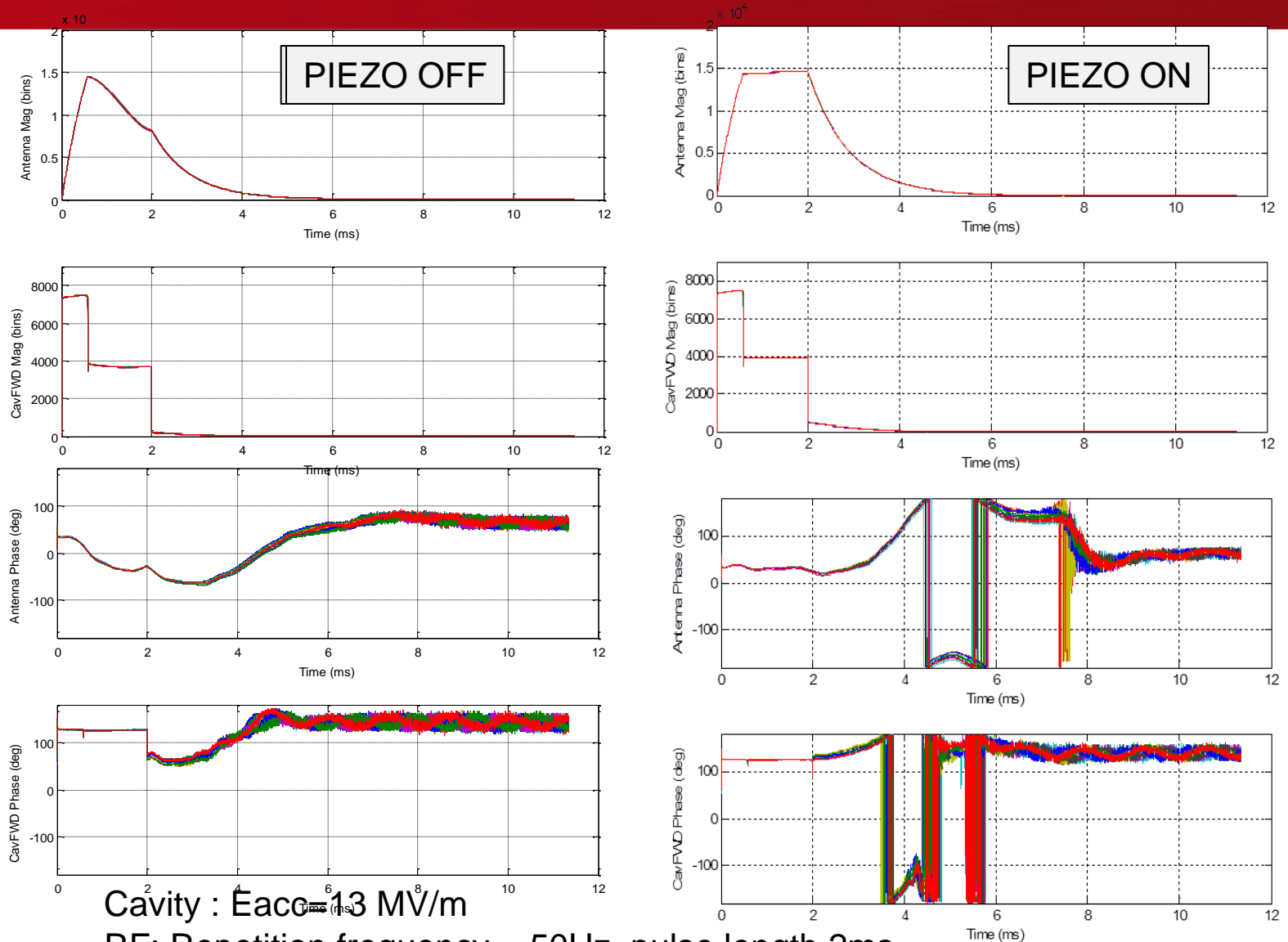
- Try to simplify the machining of the parts of a Saclay II type,
- Simplify assembly/disassembly
- Design a piezo frame which enables preload of piezo and make it independent of the cavity springback force
- Use a single piezo first

- does not take space on the beam line
- planetary gear box for reliability
- possible symmetric slow tuning +/- 2.5 mm

Testing on the CARE-HIPPI
 704 MHz $\beta = 0.47$ 5-cell cavity
 $K_L = -3.8 \text{ Hz}/(\text{MV}/\text{m})^2$



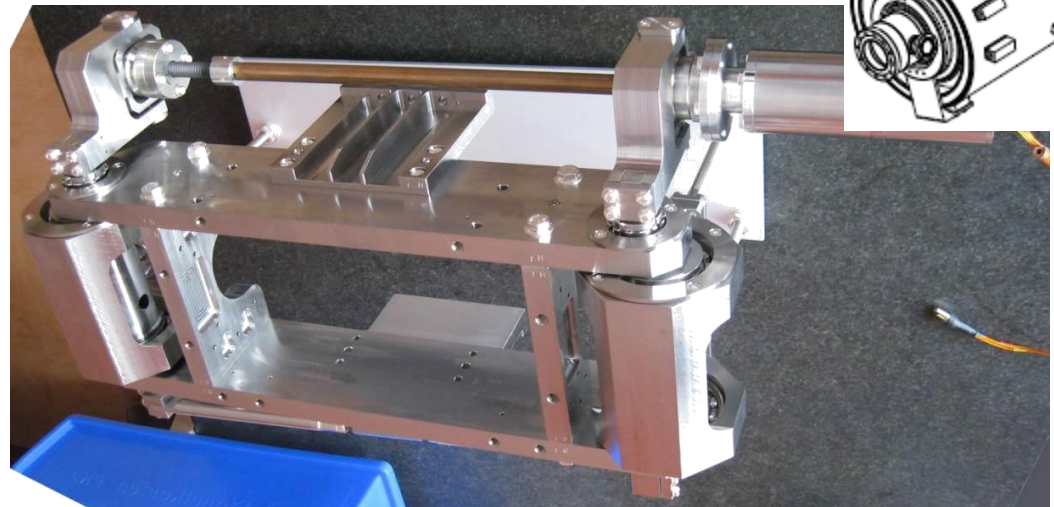
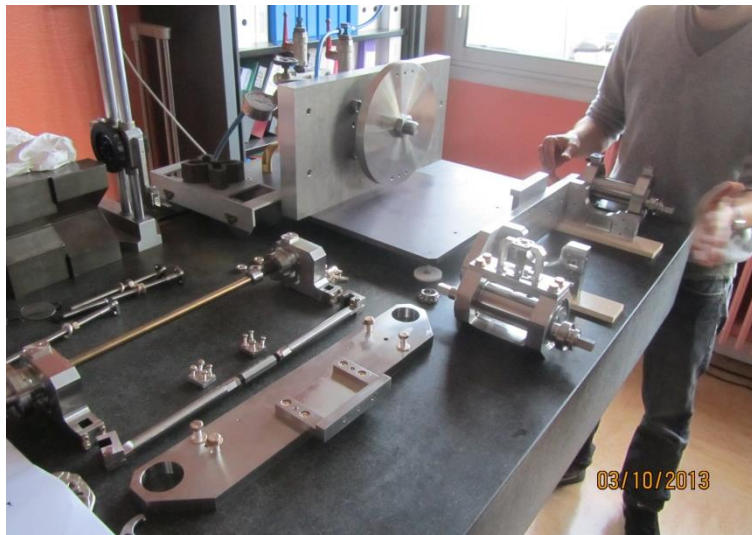
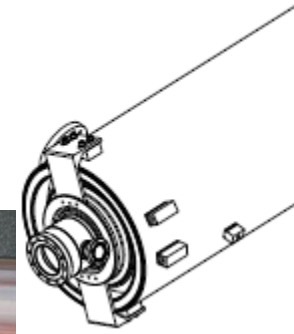
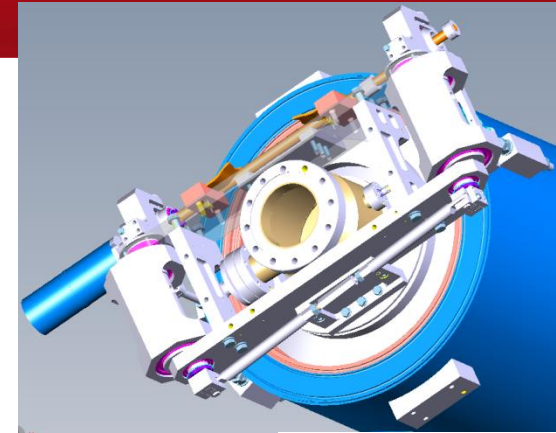
LFD COMPENSATION RESULTS



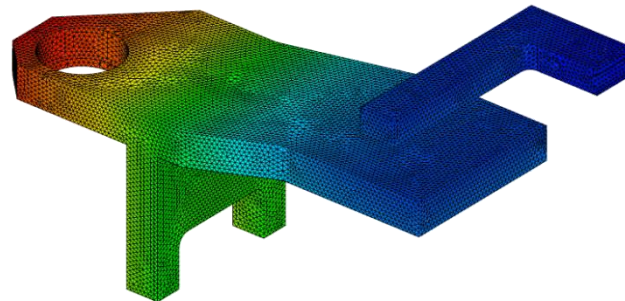
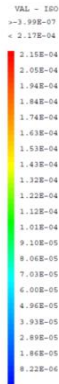
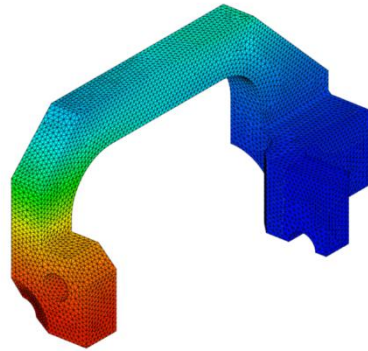
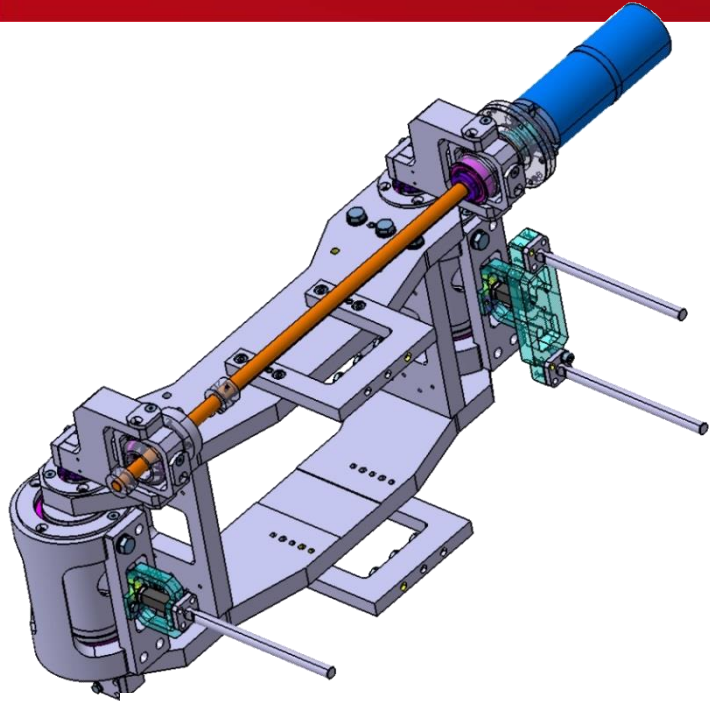
SPL tuner design is SACLAY-V of the previous type with minor modifications:

- Tuner installation on an already assembled cavity string requires:
 - compatibility with cavity clamping tools
 - Two stage assembly (pre-assembly can be done in advance, final assembly only on the cavity)
 - Attachment on beam pipe rather than on the cavity flange

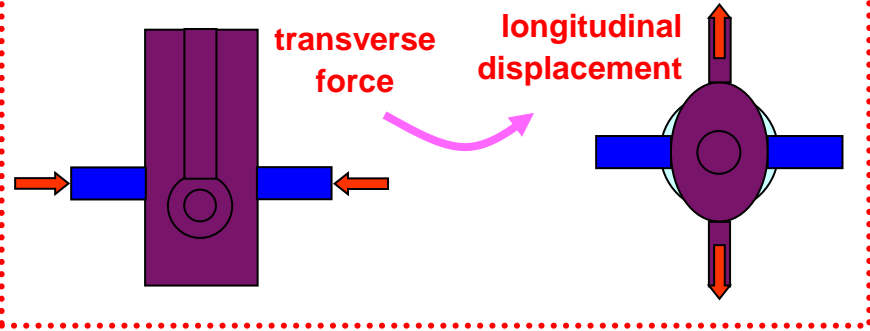
- More space for HOM dampers



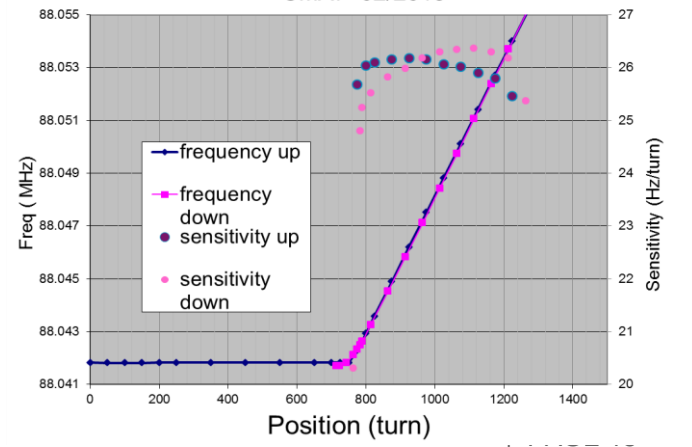
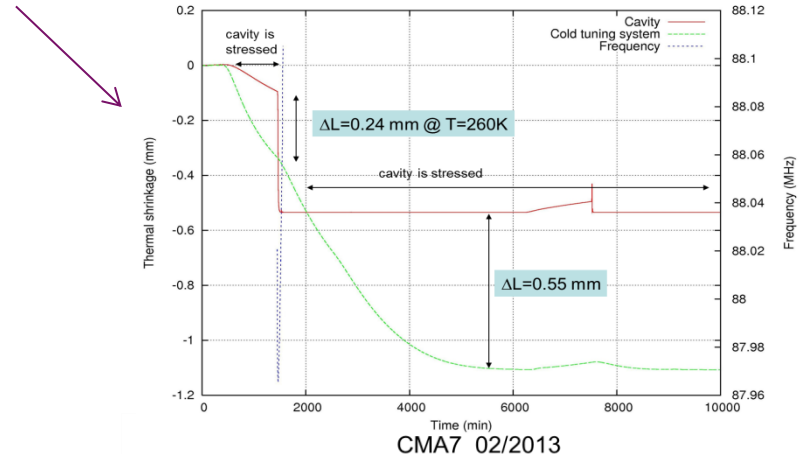
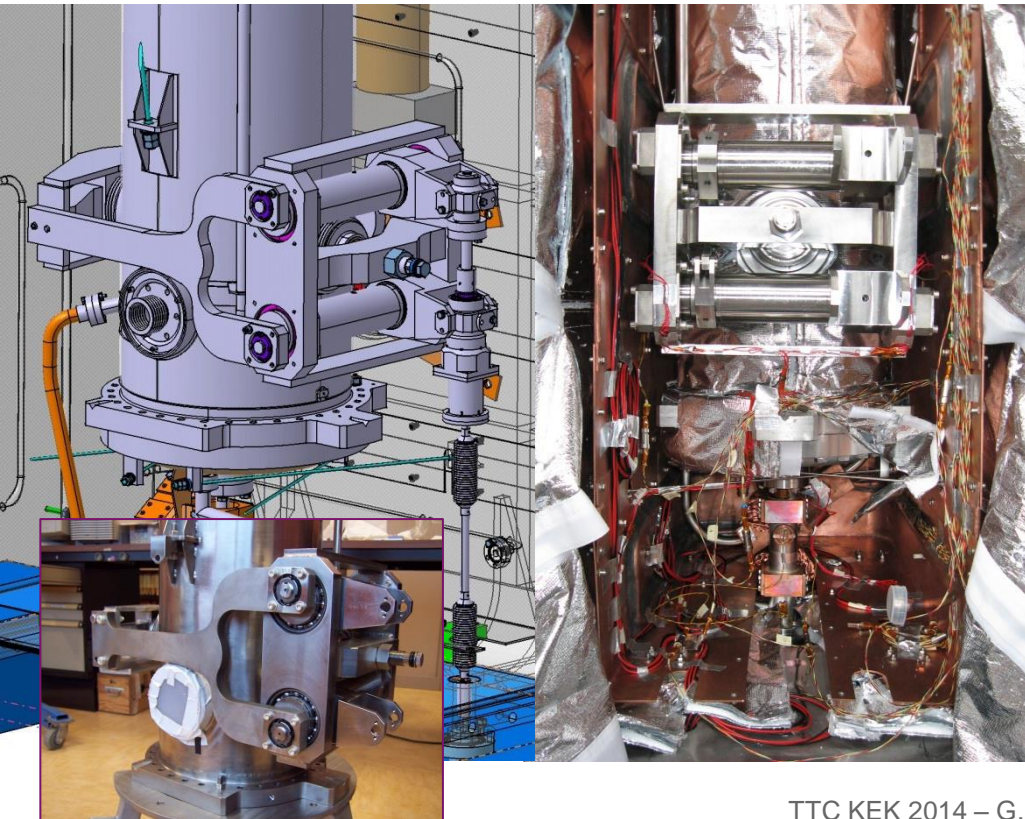
- Saclay V SPL type adapted for ESS cavities
- +/- 3 mm range
- using only positive stroke MB theor. range = 650 kHz, HB range = 590 kHz
- 1+1 piezo for redundancy
- Cold motor and planetary gearbox (1/100e)
- Piezo support has a stiffness 10 times higher than the cavity \Rightarrow piezo preload at 2K is independent of the cavity springback force



DEUTERON LINACS – SPIRAL2



- Transverse lever tuner
- Squishes the cavity
- Saves longitudinal space
- Motor is outside the vacuum vessel
- Disengagement system added after preseries cryomodule test in 2008: QWR experienced plastic deformation during cooldown





Main screw
Nut embedded in universal joint

Usual components in Saclay tuners

Stepper motor

Gear box

Arms
Eccentric shaft

form a lever arm

Stiff beams

$F=8\text{kN}$ on beam ports
 $F=250\text{N}$ on the main screw

TA6V Lever

Lever flexible area

Anchor points on the helium tank

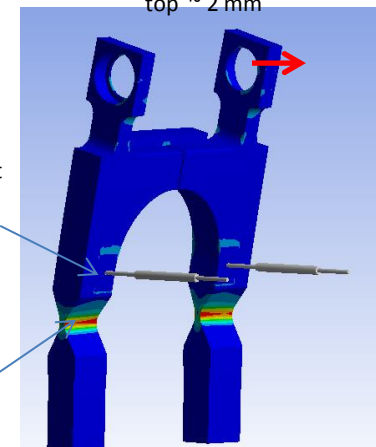
Cavity /tuner interface flange

Specific parts for HWR

Displacement of lever top $\sim 2\text{ mm}$

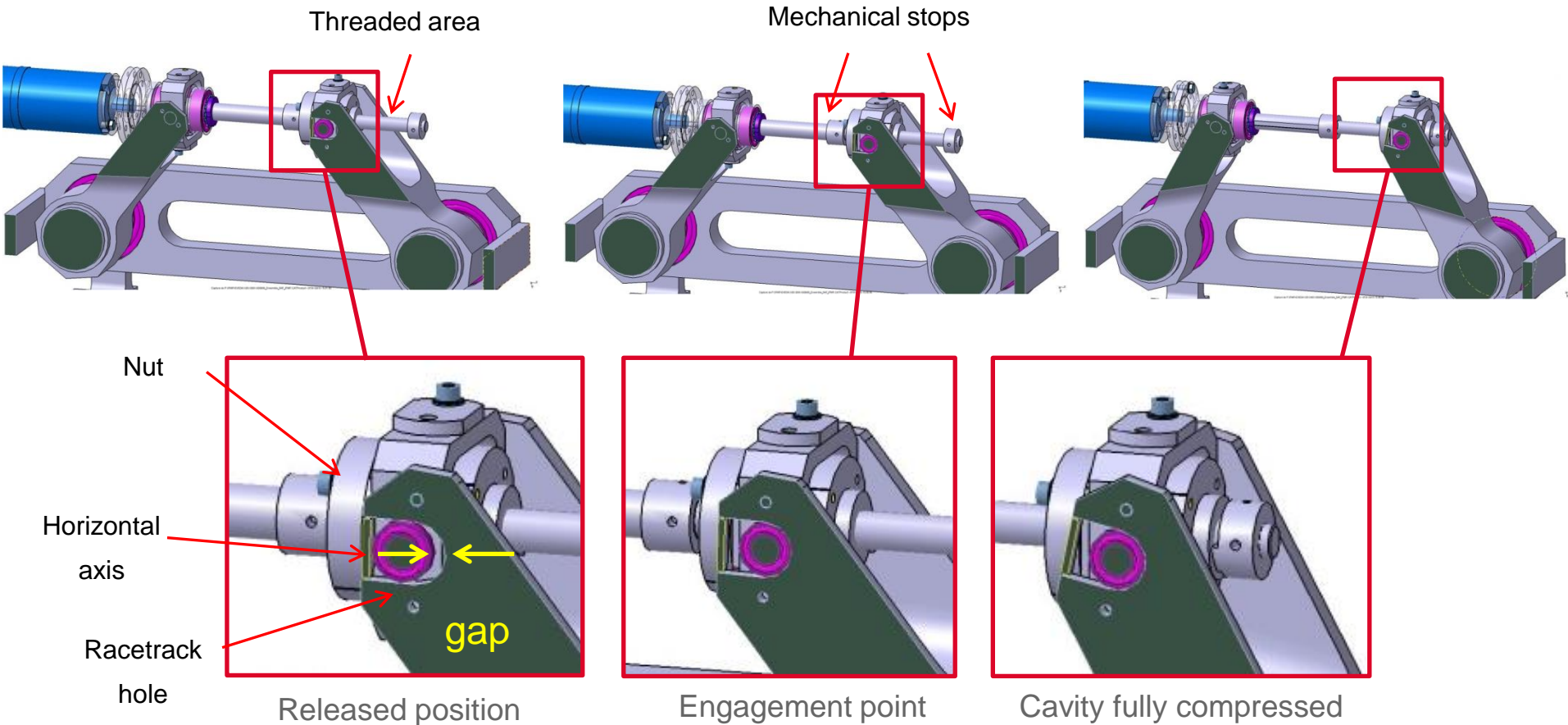
Displacement of the cavity flange $\sim 0.3\text{ mm}$

Maximum stress = 240 MPa



IFMIF LIPAC – DISENGAGEMENT SYSTEM

- The horizontal axis of the universal joint is sliding in a racetrack hole
- The mechanism is covered and secured by a cap (not seen in cut views)



Thank you for your attention

