

# Domintating noise sources in PVLAS

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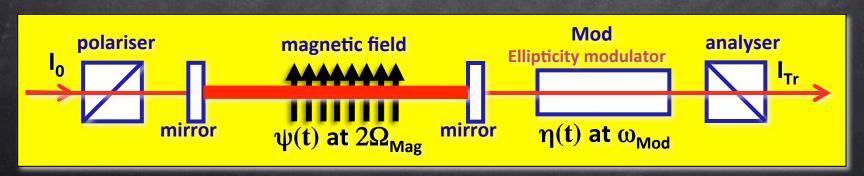
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#### PVLAS scheme



- A Fabry-Perot cavity increases the single pass ellipticity by a factor  $N=2\mathcal{F}/\pi$
- Heterodyne detection linearizes the ellipticity  $\psi$  to be measured
- Rotating magnetic fields modulate the searched effect





## Frequency components



Frequency	Fourier component	Intensity/ $I_{\rm out}$	Phase
dc	$I_{ m dc}$	$\sigma^2 + \alpha_{\rm dc}^2 + \eta_0^2/2$	97 <del></del>
$ u_{\mathrm{Mod}}$	$I_{ u_{\mathrm{Mod}}}$	$2\alpha_{\rm dc}\eta_0$	$ heta_{ ext{Mod}}$
$\nu_{\mathrm{Mod}} \pm 2\nu_{\mathrm{Mag}}$	$I_{ u_{ m Mod}\pm 2 u_{ m Mag}}$	$\eta_0 \frac{2\mathcal{F}}{\pi} \psi$	$\theta_{\mathrm{Mod}} \pm 2\theta_{\mathrm{Mag}}$
$2\nu_{\mathrm{Mod}}$	$I_{2 u_{ m Mod}}$	$\eta_0^2/2$	$2\theta_{\mathrm{Mod}}$

The signal amplitude can then be calculated from the two sidebands:

$$\Psi = \frac{1}{2} \left( \frac{I_{\nu_{\text{Mod}} + 2\nu_{\text{Mag}}}}{\sqrt{2I_{\text{out}}I_{2\nu_{\text{Mod}}}}} + \frac{I_{\nu_{\text{Mod}} - 2\nu_{\text{Mag}}}}{\sqrt{2I_{\text{out}}I_{2\nu_{\text{Mod}}}}} \right)$$

All sources of noises contributing to the spectral density of the photodiode signal at  $v_{\text{Mod}} \pm 2v_{\text{Mag}}$  will limit our sensitivity

## Sensitivity Goal



#### Main interest of PVLAS is the Euler-Heisenberg birefringence

• 
$$B = 2.5 \text{ T}$$

• 
$$F = 7.10^5$$
  $\Delta n = 2.5.10^{-23}$   $\psi = 5.10^{-11}$ 

• L = 1.6 m

If we assume a maximum integration time of 10<sup>6</sup> s (= 12 days)



The necessary ellipticity sensitivity is  $< 5 \cdot 10^{-8} \text{ 1/VHz}$ Birefringence sensitivity  $< 2.5 \cdot 10^{-20} \text{ 1/VHz}$ 

Peak shot noise limit = 
$$\sqrt{\frac{e}{I_0q}} \approx 5 \cdot 10^{-9} \; \frac{1}{\sqrt{\rm Hz}} \;\;$$
 for I $_{\rm 0}$  = 8 mW

 $(I_0$  = output intensity reaching the analyzer, q = 0.7 A/W)



### Actual Sensitivity



#### Main interest of PVLAS is the Euler-Heisenberg birefringence

• 
$$B = 2.5 \text{ T}$$

• 
$$F = 7.10^5$$
  $\Delta n = 2.5.10^{-23}$   $\psi = 5.10^{-11}$ 

• L = 1.6 m

If we assume a maximum integration time of 106 s (= 12 days)



The present ellipticity sensitivity is  $\approx 5 \cdot 10^{-7} \text{ 1/VHz}$ Birefringence sensitivity  $< 2.5 \cdot 10^{-19} \text{ 1/VHz}$ 

Peak shot noise limit = 
$$\sqrt{\frac{e}{I_0q}} \approx 5 \cdot 10^{-9} \; \frac{1}{\sqrt{\rm Hz}} \;\;$$
 for I $_{\rm 0}$  = 8 mW

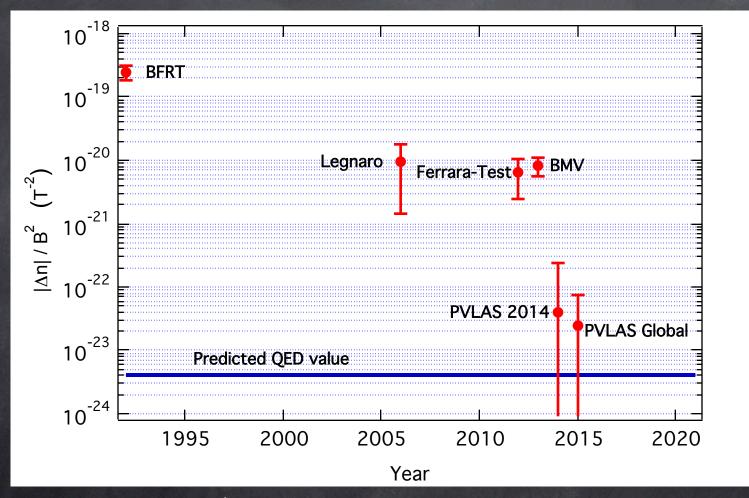
( $I_0$  = output intensity reaching the analyzer, q = 0.7 A/W)



#### Present limit



#### Error bars correspond to 1 $\sigma$



$$\Delta n_u = \frac{\Delta n}{B^2} = (-2.4 \pm 4.8) \times 10^{-23} \text{ T}^{-2}$$



### Shot noise



• The ultimate limit will be the rms shot noise  $i_{\rm shot}$  of the current  $i_{\rm DC}$  (q = photodiode efficiency  $\approx$  0.7 A/W,  $\Delta v$  = bandwidth).

$$i_{\rm shot} = \sqrt{2ei_{\rm DC}\Delta\nu} = \sqrt{2eI_0q\left(\sigma^2 + \frac{\eta_0^2}{2} + \alpha_{\rm DC}^2\right)\Delta\nu}$$

• With  $\eta_0 \gg \sigma^2$ ,  $\alpha_{\rm DC}$  the shot noise spectral sensitivity becomes ( $I_0$  = 8 mW)

$$s_{\rm shot} = \sqrt{\frac{e}{I_0 q}} \approx 5 \cdot 10^{-9} \frac{1}{\sqrt{\rm Hz}}$$



## If we were shot noise limited...



• The expected ellipticity for B = 2.5 T,  $F = 7.10^5 \text{ and}$ L = 1.6 m is

$$\psi_{\rm QED} = 5 \cdot 10^{-11}$$

 The necessary integration time to reach a signal to noise ratio = 1

$$T = \left(\frac{s_{\text{shot}}}{\psi_{\text{QED}}}\right)^2 = 10^4 \text{ s}$$



#### Other known noise sources



$$s_{\rm dark} = \frac{V_{\rm dark}}{G} \frac{1}{I_{\rm out} q \eta_0}$$

**Photodetector noise.** Reduce contribution by increasing power or improving detector

$$s_{\rm J} = \sqrt{\frac{4k_{\rm B}T}{G}} \frac{1}{I_{\rm out}q\eta_0}$$

**Johnson noise.** Reduce contribution by increasing power

$$s_{\text{RIN}} = \text{RIN}(\nu_{\text{Mod}}) \frac{\sqrt{(\sigma^2 + \eta_0^2/2)^2 + (\eta_0/2)^2}}{\eta_0}$$

Laer intensity noise. Reduce contribution by reducing  $\sigma^2$ , stabilize power, increase  $v_{\text{Mod}}$ 

+ all other uncontrolled sources of time varying birefringences  $\alpha(t)$ 

High finesse cavities are a source of 1/f birefringence noise

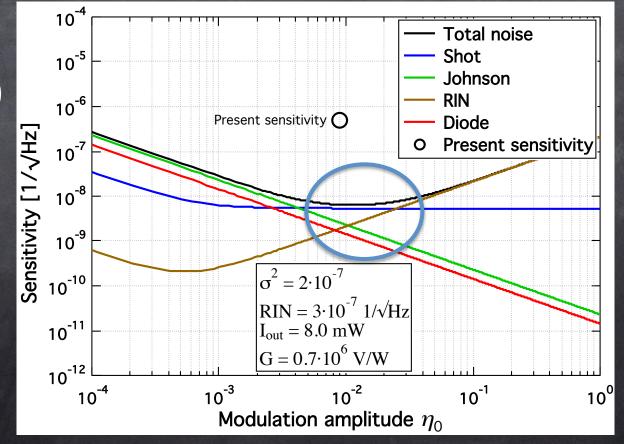


#### Calculated noise



• Contribution of the various noises as a function of the modulation amplitude  $\eta_0$  compared to the measured sensitivity.

*F* ≈ 700000





### Classification



- Noise in phase with the rotation of the magnets
  - Generate peaks
  - Peaks can be at various harmonics
  - Faraday effect at first harmonic
  - Integration is useless until these are eliminated

- Wideband Noise
  - Totally independent from magnets
  - Reduces by integrating in time





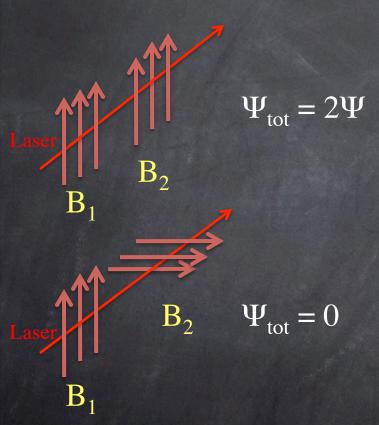
#### IN PHASE NOISE



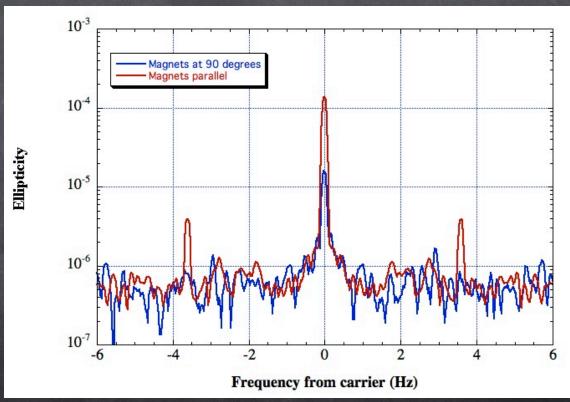
## Two magnets



Two magnets system to check that signal is due to magnetic birefringence



#### Measurement with 1.3 mbar of air

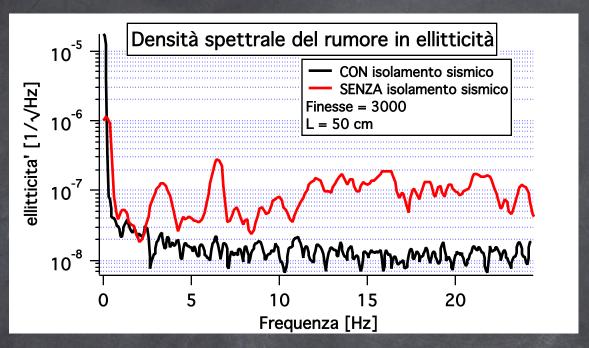


For a very weak signal this represents a crucial test



#### Vibrations



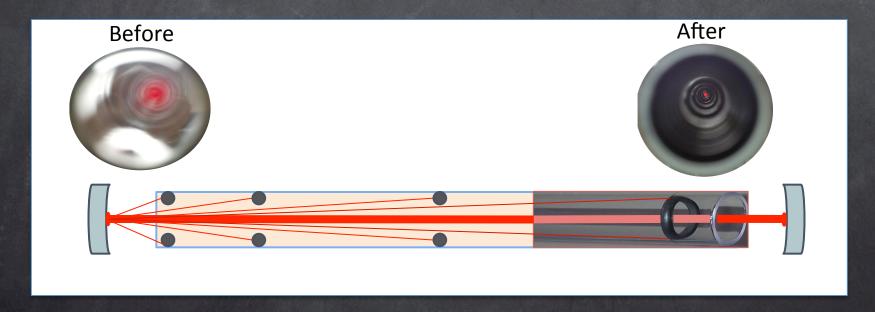


- If rotating magnets shake the optical bench peaks would appear
  - Vibrated bench to determine effect in ellipticity.
  - In phase vibration of the bench with magnets in rotation generate a very small acceleration signal. Not a limiting factor.

## Diffused light in tube



Baffles were mounted in properly spaced positions so that the light scattered from the mirror cannot see the internal surface of the glass tube.



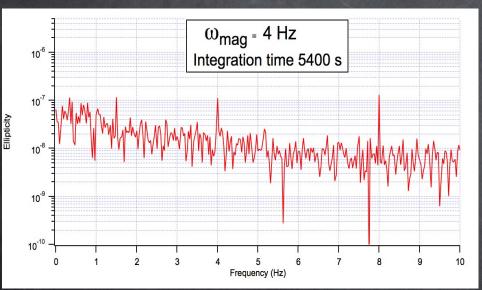
- Not optimal due to rounded edges of the o'rings
- Plan to replace them with baffles with knife-edges
- Black cermamic tube?

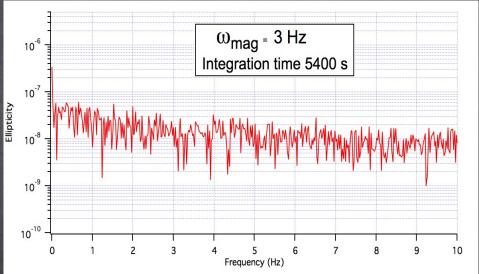


## Diffused light in tube



- Glass tube without baffles: spurious peaks were present at  $\omega_{mag}$  and  $2\omega_{mag}$
- The peaks depended on the position of the tube in the magnet
- Glass tube with baffles: spurious peaks are no longer present at  $\omega_{mag}$  and  $2\omega_{mag}$





#### Unfortunately, no improvement in sensitivity



## Faraday



- Faraday effect generates rotations, not ellipticities
  - Variations of the field component parallel to propagation
  - Present in both the gas (calibration) and on the mirrors
  - Linear in the field intensity -> first harmonic (odd harmonics)
  - In principle, not a problem. But ...

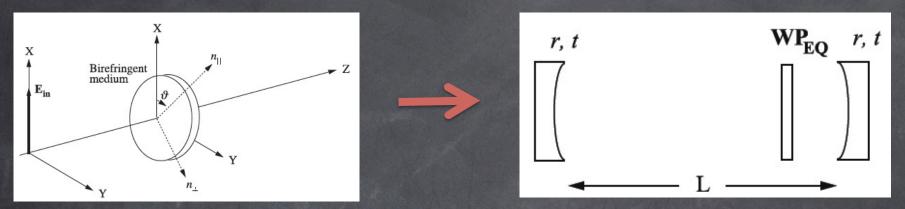
Cavity birefringence mixes ellipticities and rotations



## Mirror birefringence



Fabry Perot cavity mirrors have intrinsic static birefringence

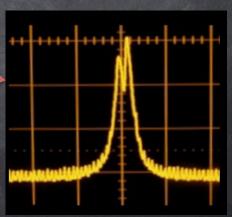


The resulting cavity behaves like a waveplate. This results in:

- cavity mode splitting
- increased 1/f noise (?)



- Cavity mirrors must be rotated to reduce total birefringence
- Polarization must be aligned with one of the equivalent waveplate axes.

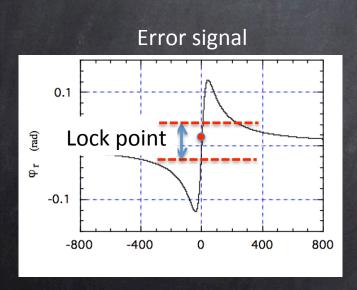


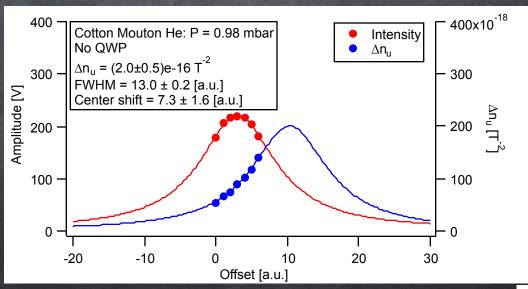
## Cavity birefringence



- With He gas at various pressures we measured the ellipticity as a function of feedback offset  $\delta$
- The imaginary part of E(t) will beat with the ellipticity of the modulator

$$E(t) = E_0 \left(\frac{2\mathcal{F}}{\pi}\right) i\psi \sin 2\theta \left(1 + i\left(\frac{\alpha_{\rm EQ}}{2} - \delta\right) \frac{2\mathcal{F}}{\pi}\right) \left(\frac{1}{1 + \left(\frac{2\mathcal{F}}{\pi}\right)^2 \sin^2\left(\frac{\alpha_{\rm EQ}}{2} - \delta\right)}\right)$$





Example with P = 0.98 mbar He



## Mirror birefringence

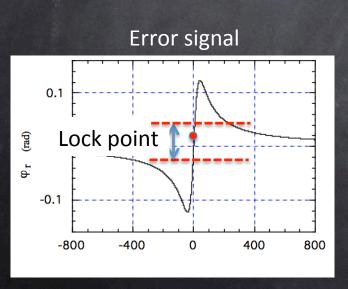


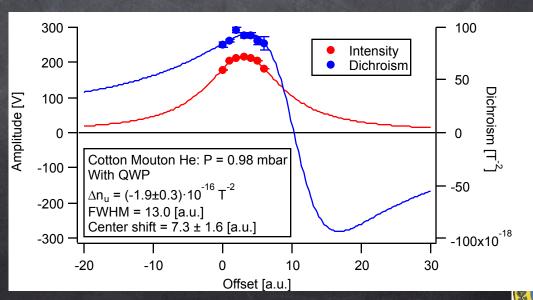
The laser is locked with its polarization along one of the cavity's axis.

- the perpendicular polarization acquires an extra phase due to the cavity birefringence
  - there is also a rotation (real component) [Appl. Phys. B 83, 571-577 (2006)]

$$E(t) = E_0 \left(\frac{2\mathcal{F}}{\pi}\right) i\psi \sin 2\theta \left(1 - i\left(\frac{\alpha_{\rm EQ}}{2} - \delta\right) \frac{2\mathcal{F}}{\pi}\right) \left(\frac{1}{1 + \left(\frac{2\mathcal{F}}{\pi}\right)^2 \sin^2\left(\frac{\alpha_{\rm EQ}}{2} - \delta\right)}\right)$$

With a QWP and the ellipticity modulator one can measure the induced rotation.





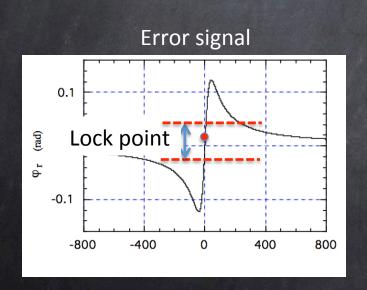
## Mirror birefringence

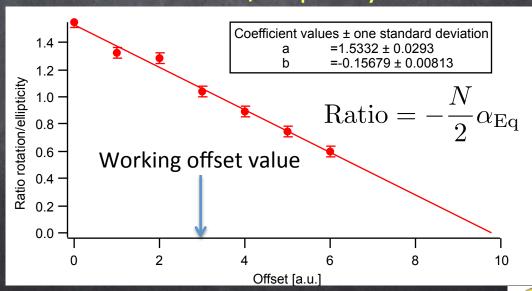


Vice versa if there were a rotation  $\varepsilon$  induced in the cavity it will partially convert to an ellipticity and beat with the modulator alone

$$E(t) = E_0 \left(\frac{2\mathcal{F}}{\pi}\right) \underbrace{\epsilon \sin 2\theta \left(1 - i\left(\frac{\alpha_{\rm EQ}}{2} - \delta\right) \frac{2\mathcal{F}}{\pi}\right)}_{\bullet} \left(\frac{1}{1 + \left(\frac{2\mathcal{F}}{\pi}\right)^2 \sin^2\left(\frac{\alpha_{\rm EQ}}{2} - \delta\right)}\right)$$

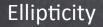
#### Rotation/ellipticity

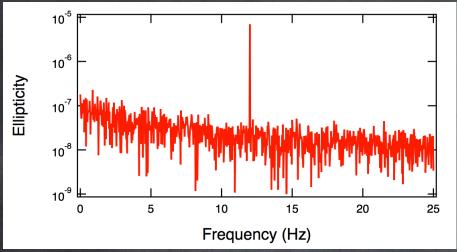




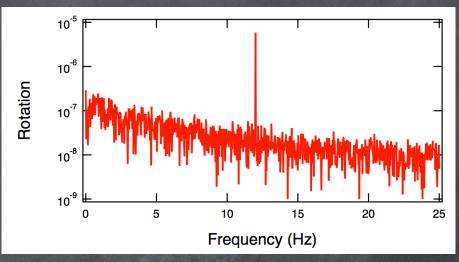








QWP inserted: Rotation



230 µbar Ar.  $v_B = 6$  Hz, 640 s integration

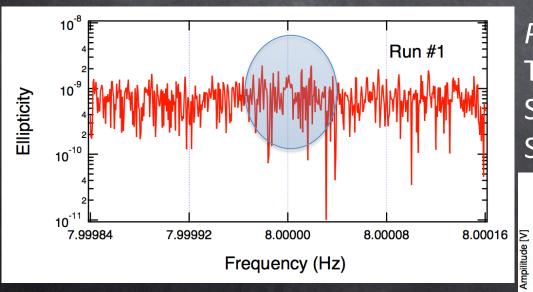
#### In Vacuum

- .... a Faraday rotation will be seen as an ellipticity. In vacuum, we only see a contribution at the first harmonic: signal  $\approx 10^{-8}$ .
- The two magnets give different values and phase in the signal due to slightly different longitudinal component of the field on the mirrors

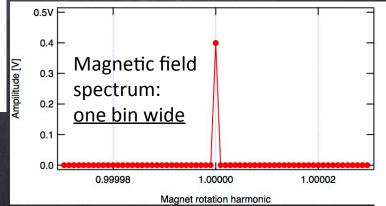
## In phase noise



- After some effort, we think we have systematic peaks under control.
   Centering of the glass tube inside the magnet is critical.
- Long integration is possible.
- During some long runs, small drifts change the measurement conditions and small structures appeared around  $2v_B$  several bins wide in the Fourier spectrum.



 $P < 10^{-7}$  mbar.  $v_B = 4$  Hz T =  $10^6$  s intgration Signal width  $\Delta v = 10^{-6}$  Hz Structure  $> \approx 10^{-5}$  Hz







### WIDEBAND NOISE



#### Possible sources



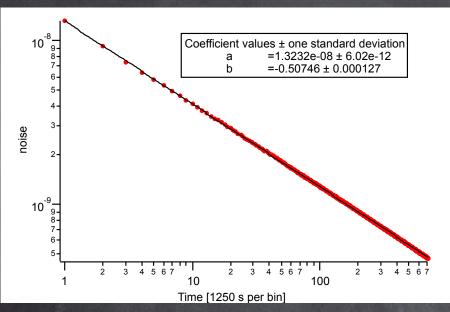
- Thermal effects
- Laser feedback
- Environmental noise
- Diffused light
- Gas
- Mirror birefringence



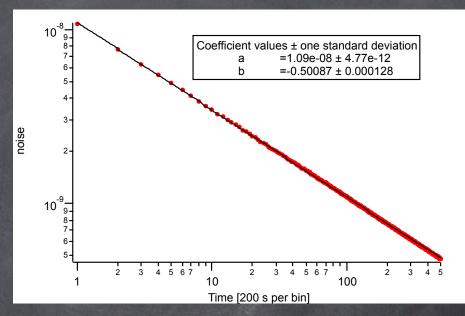
### Measured noise

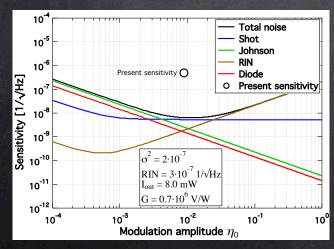






 $T = 10^6 \, s$ 





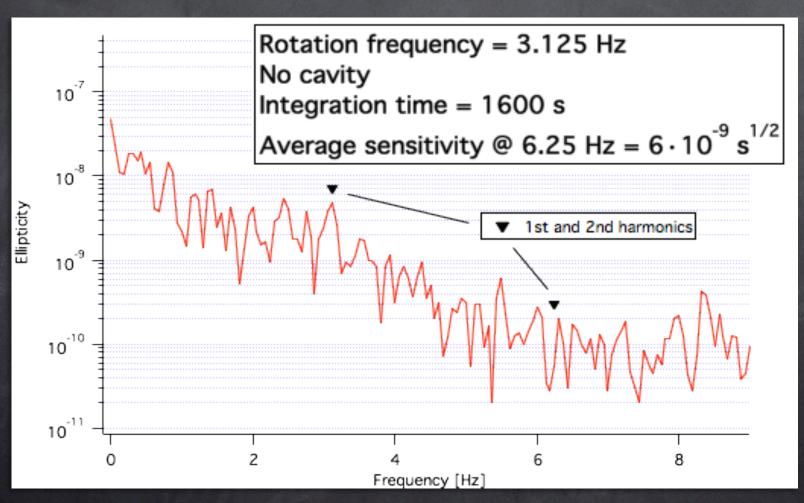
Integrated noise around  $2v_{\rm B}$  decreases as  $\sqrt{T}$ 



### Performance without cavity



**No cavity** – reached expected noise level with rotating magnets



No electronically induced signals in the readout system



## Thermal effects



- Noise at  $2v_B$  is independent of laser power
  - Stronger drifts in quasi static ellipticity if power is turned up
  - Effect at much lower frequencies than  $2v_R$  (6 Hz 12.5 Hz)
  - After an 'unlock' of the laser there is an ellipticity settling time of several minutes. Does not affect noise a  $2v_B$ .
  - The settling and drifts also depend on how well the polarization is aligned with the cavity birefringence.
  - The contribution of the static ellipticity of the PEM is not neglectable.



#### Environmental noise



- Possible contribution from conditioning system
  - All electronics has been taken outside of the clean room
  - Temperature stability is better than 0.1 degrees
  - Took two relatively long runs with and without conditioning system => NO DIFFERENCE in sensitivity



### Feedback



- Redesigned feedback circuit after 2014
  - Automatic locking
  - Lower noise integrated OpAmps
  - Lower offsets

No improvement in the wideband noise

- Tried several different locking frequencies
  - Working frequency = 503 kHz: below crystal resonance
  - Tried different frequencies without any improvement in the noise



### Feedback 2



- Locking set point can be modulated
  - Modulation generates ellipticity signal at  $v_{\text{Mod}}$  and  $2v_{\text{Mod}}$ .
  - Conversion Ellipticity => frequency: ≈ 10<sup>-6</sup> per Hz
  - Output noise from mixer generates noise in ellipticity: ≈ 10<sup>-9</sup>

Cannot account for observed wideband noise.



## Diffused light



- Installation of baffles and absorbing glass
  - Baffles reduced peaks but had no effect on sensitivity
  - Diaphragm at center of cavity: 5 mm diameter. No effect.
  - Absorbing glass in large vacuum chambers. No effect.

- Changed input polarizer
  - New polarizer with fewer surfaces (Glan-Thompson)
  - Noise improved by factor ≈ 4!
  - May be due to alignment ?

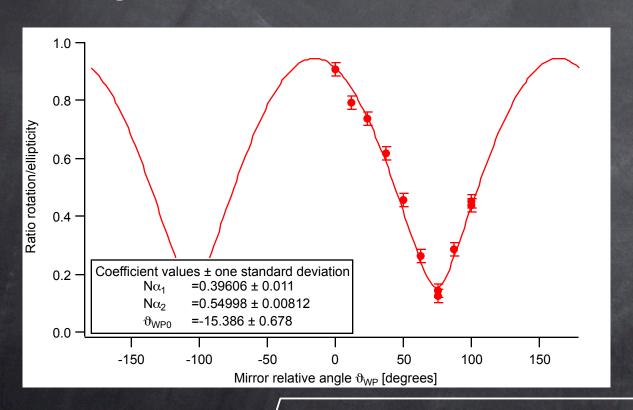
Not really clear..... More testing soon



## Mirror Birefringence



- Both mirrors have birefringence with  $N\alpha/2 \approx 0.5$ 
  - Aligned slow axis of one mirror with fast axis of the other



- Unfortunately the alignment drifts slowly with time!
- To be conservative, we considered the worst value.

$$N\alpha_{\rm EQ} = N\sqrt{(\alpha_1 - \alpha_2)^2 + 4\alpha_1\alpha_2\cos^2\theta_{\rm WP}}$$



## Cooling mirrors



 We are planning to design new chambers for the mirrors which will allow cooling of the mirrors to LN<sub>2</sub>.



## Thank you



### Cotton-Mouton effect



A gas at a pressure p in the presence of a transverse magnetic field B becomes birefringent.

 $\Delta n_u$  indicates the birefringence for unit field at atmospheric pressure

$$\Delta n = n_{\parallel} - n_{\perp} = \Delta n_u \left( \frac{B[T]}{1T} \right)^2 \left( \frac{P}{P_{\text{atm}}} \right)$$

Total ellipticity

$$\psi_{\rm gas} = \frac{\pi L_{\rm eff}}{\lambda} \Delta n_u B^2 p \sin 2\theta$$

Gas	$\Delta n_{\rm u}$ ( T ~ 293 K)	
Nitrogen	$-(2.47\pm0.04) \times 10^{-13}$	
Oxygen	$-(2.52\pm0.04) \times 10^{-12}$	
Carbon Oxide	$-(1.83\pm0.05) \times 10^{-13}$	
Helium	(2.2±0.1) x 10 <sup>-16</sup>	

To avoid spurious effects the residual gas must be analysed:

Ex.  $p(O_2) < 10^{-8}$  mbar



## Key ingredients



Experimental study of the quantum vacuum with:

- magnetic field perturbation
- linearly polarised light beam as a probe
- changes in the polarisation state are the expected signals

$$\psi = \frac{\pi L_{\text{eff}}}{\lambda} \Delta n(B^2) \sin 2\theta(t)$$

- high magnetic field rotating high field permanent magnet
- ullet long optical path very-high finesse Fabry-Perot resonator:  $N=2{\cal F}/\pi$
- ellipsometer with heterodyne detection for best sensitivity periodic change of field amplitude/direction for signal modulation

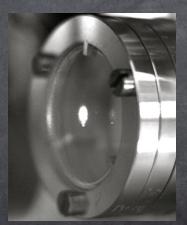


## Problems and how to proceed with the process of the proces

#### Sensitivity far from expected

- Diffused light in the chambers due to optical elements and from a few dust speckles on the mirrors
- Substituted input polarizer (fewer surfaces) and noise improved by factor 3 .... Clue?



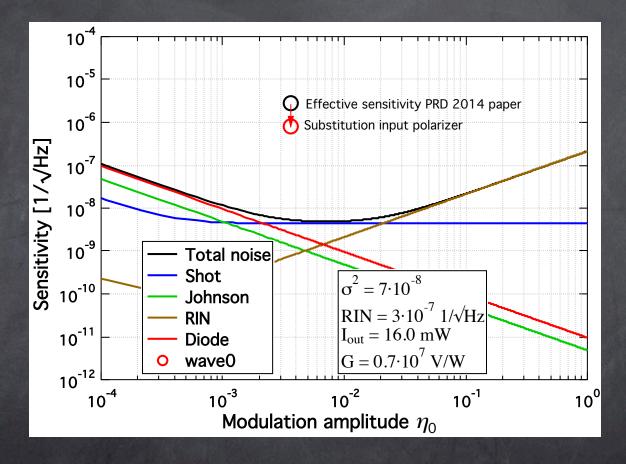


- Ordered wobble-sticks to try to design a cleaning method
- Ordered absorbing glass to cover inner walls of chambers



#### Future





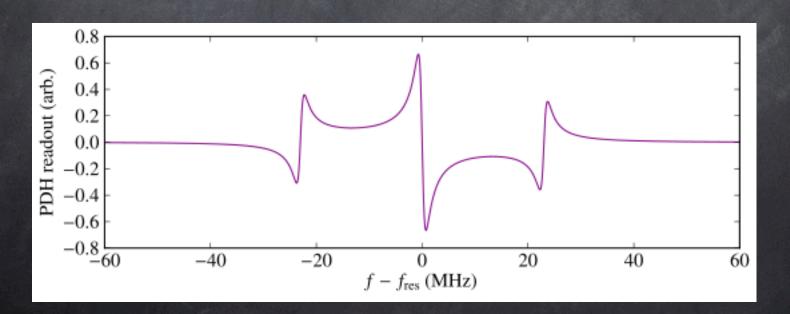
- Starting new data taking with new sensitivity
- QED is still out of reach ....



## Laser locking principle



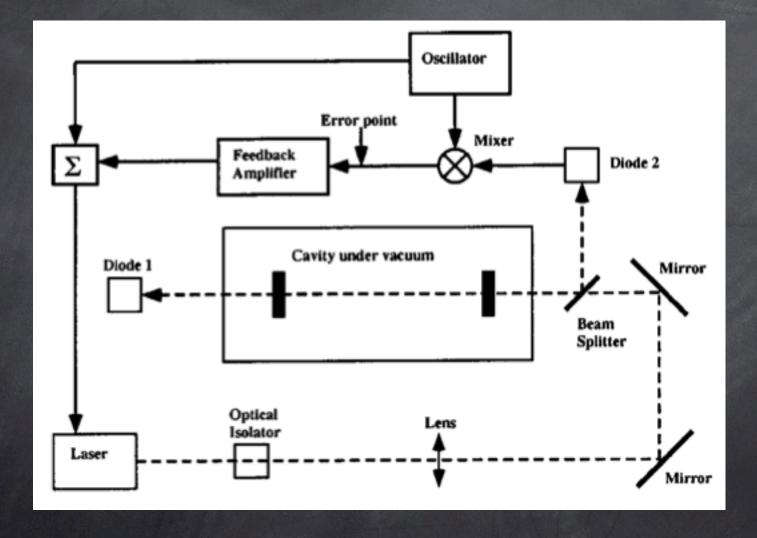
- In practice the laser is modulated at a frequency greater than the feedback bandwidth
- The reflected light is detected and demodulated at the modulation frequency
- An error signal is obtained. The central part is linear





## Locking scheme

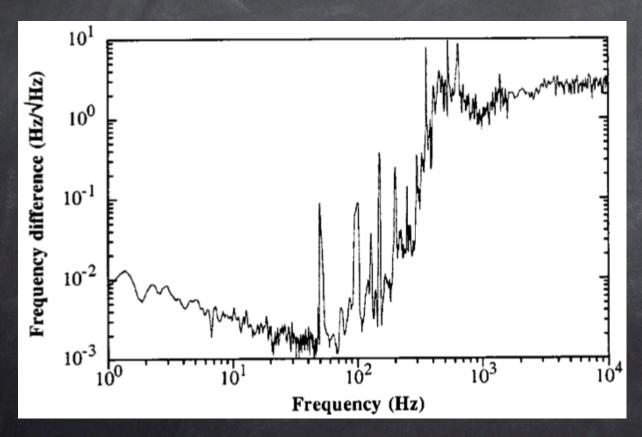




## Locking scheme



Noise spectral density of the error signal during lock. This indicates the frequency **difference** between the cavity and the laser.



Cavity finesse = 45000 Cavity width = 3800 Hz



#### Noise considerations



Indicating with  $R_{\nu_{
m Mod}+2\nu_{
m Mag}}$  the noise spectral density at the signal frequencies and assuming

$$R_{\nu_{\text{Mod}}+2\nu_{\text{Mag}}} = R_{\nu_{\text{Mod}}-2\nu_{\text{Mag}}}$$

The ellipticity sensitivity spectral density will be

$$s = \frac{R_{\nu_{\text{Mod}} + 2\nu_{\text{Mag}}}}{\sqrt{4I_{\text{out}}I_{2\nu_{\text{Mod}}}}}$$

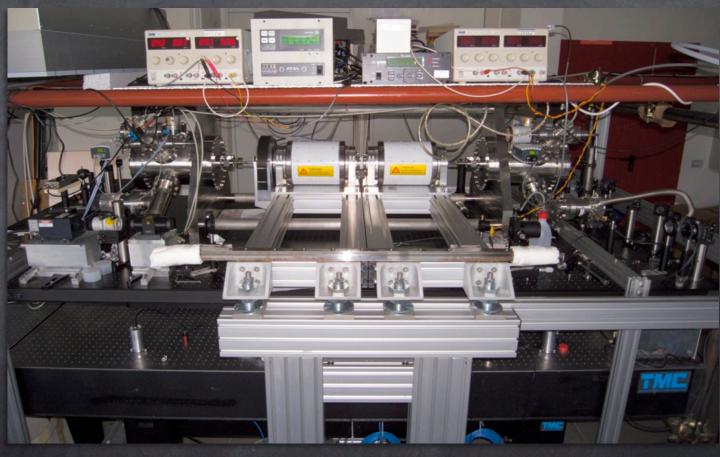


### Ferrara test setup



- Ellipsometer
   and optical
   cavity on single
   optical table
- Optical table with active suspension system
- Two magnets
- High rotation frequency for the magnetic source
- High frequency polarization modulator

In operation since 2010



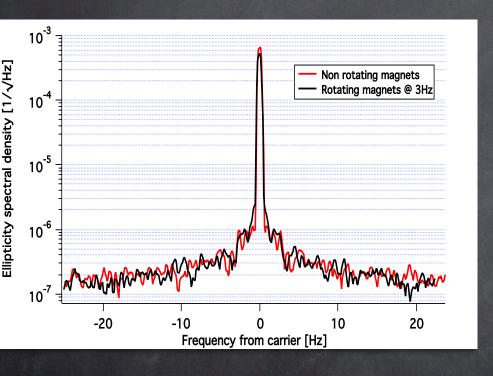
Main limitation: most of the components are magnetic

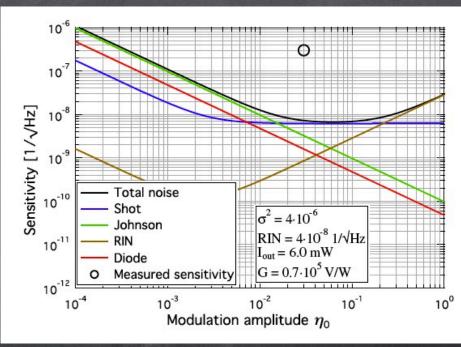


#### Performance - wideband noise



With high-finesse cavity: F > 400000Extra wideband noise. Sensitivity worsened – still under study



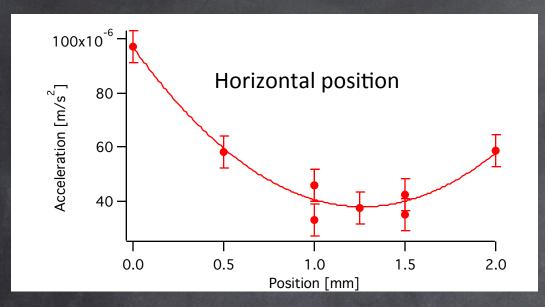


 $s_{total}$  (6 Hz) ~ 3  $10^{-7}$  1/VHz  $s_{total}$  (20 Hz) ~ 1.5  $10^{-7}$  1/VHz



#### Tube movement





- Placing a 3-axis accelerometer on the glass tube we were able to study its movement as a function of its position
- The glass tube was positioned where the movement was minimum.

