



The OSIRIS Pre-Detector

Paul Hackspacher, Michael Wurm Forschergruppe JUNO



September 18, 2017

From Daya Bay Liquid Scintillator Replacement Experiment: Danger of 222 Rn-contamination of LS



Possible issues in JUNO:

- Air leak in filling line?
- Failure of purification plants?
- Unforeseen problems?



- Joint use of on-site LS storage tank as radioactivity pre-detector
- Measure radioactive background during storage/filling/cycling





Online Scintillator Internal Radioactivity Investigation System



- 8 m height
- 100 20" wall PMTs, honeycomb arrangement
- 2 cm acrylic tank, $\emptyset = 3 \text{ m}$
- Water buffer, $\emptyset = 7 \text{ m}$
- 6 mm steel walls,
 60 cm rock cavern
- 5" steel slabs on top and bottom



PMT Distribution



PMT design based on JUNO simulation: ellipsoid + cylinder (mushroom) Material properties (composition, density, refractive indices, etc.) based on LENA simulation with updates from JUNO

$$\left. \begin{array}{l} A_{PMT} = 20.27 \text{ m}^2 \\ A_{Tank} = 152.38 \text{ m}^2 \end{array} \right\} r = 13.3\% \\ \text{PMT QE} \times \text{CE} = 35\% \end{array} \right\} \text{Photons detected: } \sim 4.66\% \\ \end{array}$$

Absolute light yield: $Y \approx 10,000 \gamma/\text{MeV}$ Photoelectron yield: $Y_{p.e.} \approx 466 \text{ p.e.}/\text{MeV}$

Conservative estimate: $Y_{p.e.} \simeq 300 \text{ p.e.}/\text{MeV}$ (considering absorption, etc.)

Energy resolution:
$$\frac{\Delta E}{E} = \frac{\Delta N}{N} \stackrel{\text{Poisson}}{=} \frac{1}{\sqrt{N}} = \frac{1}{\sqrt{Y_{p.e.} \cdot E}}$$

 $\Rightarrow \Delta E = \sqrt{\frac{E}{Y_{p.e.}}}$

Bi-Po-coincidence within Uranium chain, daughters of ²²²Rn:

$$\begin{array}{c} ^{214}\mathrm{Bi} \rightarrow ^{214}\mathrm{Po} \rightarrow ^{210}\mathrm{Pb} \\ \beta \mbox{ (99.979\%) } \alpha \\ \mbox{Q-Value: } 3.26\,\mbox{MeV} \quad E_{\alpha} = 7.69\,\mbox{MeV} \end{array}$$



Fig. 11 - Measured time difference between pairs of 214 Bi and 214 Po events; T(214 Po) = 236.6 µs.

CTF (arXiv:0705.0239[physics.ins-det])

$$au(^{214}{
m Po}) = 236.6\,\mu{
m s}$$

Select coincidence window: 710 μ s (three lifetimes τ)

Bq / kg	⁴⁰ K	²³² Th	²³⁸ U
PMT	8.96	3.71	3.76
Rock	220	123	142
Steel	$13.4 \cdot 10^{-3}$	$8 \cdot 10^{-3}$	$1.2 \cdot 10^{-3}$
Acrylic	$270 \cdot 10^{-6}$	$4 \cdot 10^{-6}$	$12\cdot 10^{-6}$

External Backgrounds

From DocDB 2140, 1377

Internal Backgrounds

⁴⁰ K	$1 \cdot 10^{-17} \mathrm{g/g}$
²³⁸ U	$1\cdot 10^{-16} \mathrm{g/g}$
²³² Th	$1\cdot 10^{-16} \mathrm{g/g}$
¹¹ C	1000 cts/d/kt
¹⁰ C	20 cts/d/kt

From solar neutrino requirements

How small can the signal get so that we can still identify it against the background?

Qualitative shape comparison:





Shielding





Event Rate Distribution



In order to distinguish signal from background: $N_{BiPo} \sim 2 \cdot \sqrt{N_{BG}}$

$$\Rightarrow R_{Bi} \gtrsim \frac{2 \cdot \sqrt{R_{BG}(\mathrm{Bi}) \cdot \Delta t_{Coinc} \cdot R_{BG}(\mathrm{Po})}}{\left(1 - \exp(-\frac{\Delta t_{Coinc}}{\tau})\right) \cdot \epsilon_{Bi} \cdot \epsilon_{Po}} \cdot \frac{1}{\sqrt{t_{Tank}}}$$

Background rates for various fiducial volumes:

Volume	Mass	Bi-Range	Po-Range	Accidentals
Full	48.6 t	1324 Bq	529 Bq	497 Bq
$ z \leq 3 \mathrm{m}$	36.5 t	104 Bq	26 Bq	1.9 Bq
$ z \leq 3 \mathrm{m}, r \leq 1 \mathrm{m}$	27.4 t	24 Bq	0.2 Bq	3 .4 mBq

After scaling with fiducial volume mass:

Sensitivity over Time



Sensitive up to $3.8 \cdot 10^{-8} \,\mathrm{Bq/kg} \stackrel{\circ}{=} 160 \,\mathrm{cts/d} \stackrel{\circ}{=} 6.8 \cdot 10^{-27} \,\mathrm{g/g}$ of $^{222} \mathrm{Rn}$

May 2007: Rn contamination in Borexino due to air leak during filling



Rn event rate in Borexino

Maximal event rate: $\sim 800 \, \text{cts/d}$

Component	Costs (EUR)	Comment
Steel tank	35,000	assuming a conventional tank
		welded underground
Acrylic vessel	27,000	
Steel slabs	7,500	material costs for 4 m diameter
MCP-PMTs	350,000	assuming 3,500 EUR per piece
- mounting, potting,	+x	
- cabling, electronics	+x	
Liquid Handling system	+x	
- overflow tank		

Total: \sim 500,000 EUR

Re-purpose of Daya Bay PMTs:

- Huge cost savings
- DYB PMTs better operated in oil \Rightarrow Change of buffer liquid?

Trigger rate?

- DYB FADC: 100 Hz
- TDC/ADC: 2 kHz
- Singles background (above 500 keV) in OSIRIS: 5.8 kHz

Tank size issue

- Room size: L=42 m, W=12 m, H=10 m
- Welding underground not allowed
- Tank too heavy for crane
- 1 m additional height for calibration system?





- Danger of Rn-contamination in Liquid Scintillator line (Air leak, purification failure, etc.)
- Joint use of LS tank as radioactivity monitor during filling/cycling
- Mounting of $\mathcal{O}(100)$ photomultipliers on tank inner walls
- Measuring Bi-Po-214-coincidence vs external gamma background
- Geant4-simulation shows sensitivtly up to $3.8\cdot 10^{-8}\,\mathrm{Bq/kg} \triangleq 160\,\textrm{cts/d} \triangleq 6.8\cdot 10^{-27}\,\mathrm{g/g}~\textrm{of}~^{222}\mathrm{Rn}$
- Costs estimated to $\mathcal{O}(500 \text{ kEUR})$

Outlook

- Task Force summoned in the last collaboration meeting
- Find realizable construction solution, iron out discrepancies
- Move simulation to GIT/SVN project
- Rewrite geometry to investigate new design feasibility

Looking for people to contribute in the simulation





