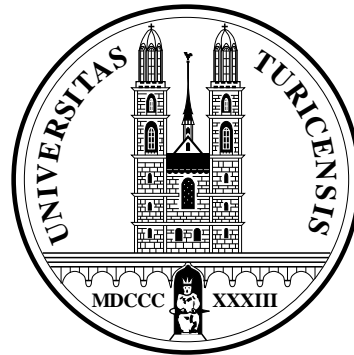


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# A numerical approach to the double real radiation part of $e^+e^- \rightarrow 3$ jets at NNLO

Gudrun Heinrich

Universität Zürich



# Motivation

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experiments at high energy colliders in past years:

precision measurements

led to stringent tests of the Standard Model and bounds on New Physics

only possible in combination with

"precision calculations"

what to expect from "Old Physics" must be well under control  $\Rightarrow$  precise knowledge of parameters like  $\alpha_s$ ,  $\sin^2 \theta_W$  important

- at the LHC:  $n$ -jet cross section  $\sim \alpha_s^n$
- future International Linear Collider will reach precision at the per mille level

# Jet production in $e^+e^-$ annihilation

---

measurements of  $e^+e^- \rightarrow$  jet rates & shape observables

- allow precision tests of the SM over wide range of energies
- offer possibility for determination of strong coupling constant  $\alpha_s$  with unseen precision

$\alpha_s$  world average:

$$\alpha_s(M_Z) = 0.1182 \pm 0.0027 \text{ (stat. and sys.)} \quad [\text{S. Bethke 04}]$$

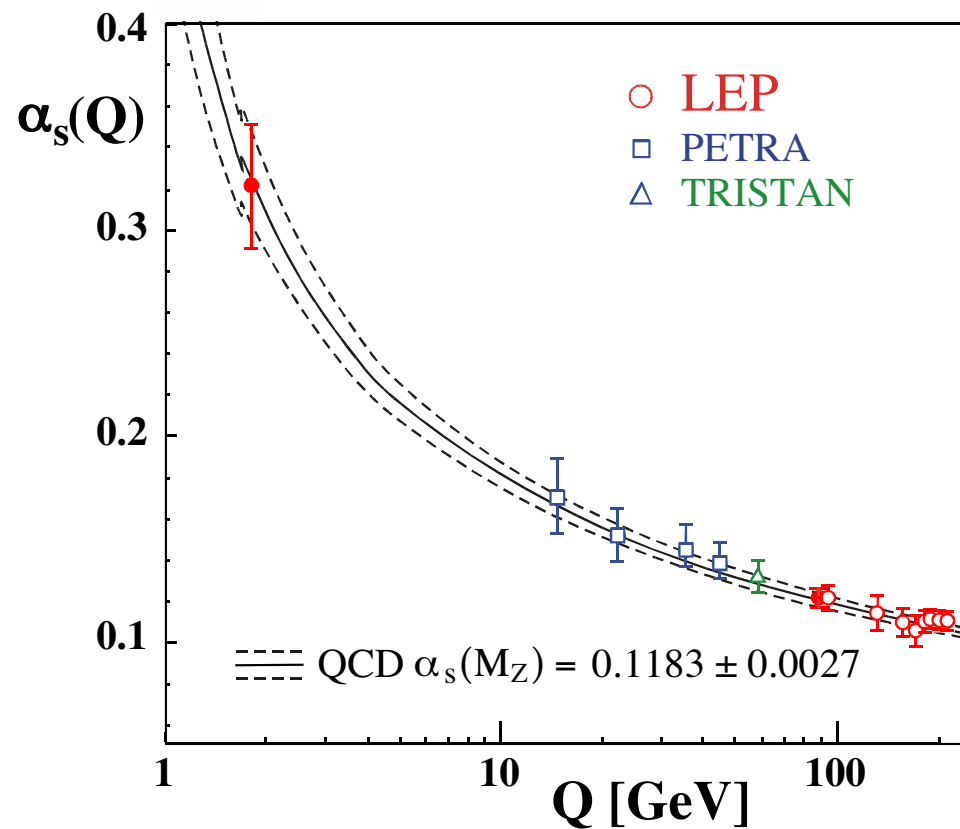
determination based **only** on data where

**NNLO** QCD theory predictions exist!

(DIS,  $\Gamma(Z \rightarrow \text{had})$ ,  $\tau$ ,  $\Upsilon$  – decays)

# $\alpha_s$ determination

LEP data for jets and shape observables very precise,  
but not used for world average: only NLO theory available!



[S. Bethke '04]

# $\alpha_s$ determination

---

error on  $\alpha_s(M_Z)$  from  $e^+e^-$  jet rates and event shape observables (NLO + NLL resum) :

theoretical:  $\mathcal{O}(5\%)$ , dominated by scale dependence !

experimental:  $\mathcal{O}(1.3\%)$  (statistical, hadronisation, ...)

[R. Jones, Ford, Salam, Stenzel, Wicke '04]

⇒ NNLO will improve the error considerably !

mandatory to match experimental precision at the ILC

NLO calculation:

Ellis, Ross, Terrano '81, Fabricius, Schmitt, Kramer, Schierholz '81,  
Kramer, Lampe '89, Kunstz, Nason, Marchesini, Webber '89

resummation:

Catani et al. '92-'98, Dokshitzer et al. '98, Banfi et al. '02, Gardi et al. '01-'03

# NNLO calculations

---

## problems in NNLO calculations:

- enormous complexity of expressions
- analytic integrations very difficult
- direct numerical evaluation hampered by singularities
- massless particles  $\Rightarrow$  **soft and collinear (IR) singularities**  
( $1/\epsilon^n$  poles in dim.reg.)
- IR singularities are entangled in a complicated way  
 $\Rightarrow$  need to be isolated and subtracted
  - from loop integrals ( $\rightarrow$  **analytic integration**)
  - from integrals over soft/collinear phase space regions ( $\rightarrow$  **subtraction terms**)

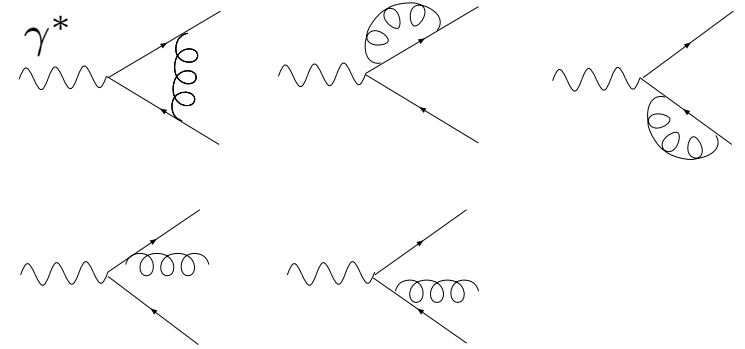
# subtraction of infrared poles: NLO

virtual:  $d\sigma^V = P_2/\epsilon^2 + P_1/\epsilon + P_0$

real: integration of subtraction terms

$d\sigma^S$  over singular regions of phase space

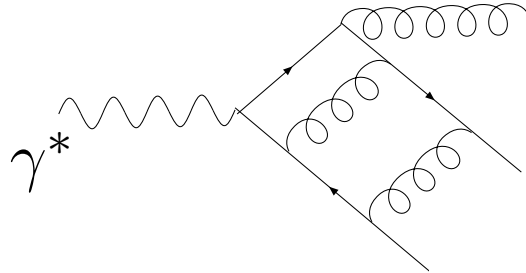
$$\Rightarrow \int_{\text{sing}} d\sigma^S = -P_2/\epsilon^2 - P_1/\epsilon + Q_0$$



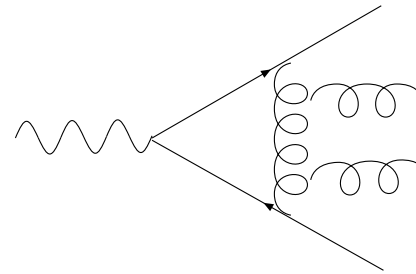
$$\sigma^{NLO} = \underbrace{\int_{m+1} \left[ d\sigma^R - d\sigma^S \right]_{\epsilon=0}}_{\text{numerically}} + \underbrace{\int_m \left[ \underbrace{d\sigma^V}_{\text{analytically}} + \underbrace{\int_1 d\sigma^S}_{\text{analytically}} \right]_{\epsilon=0}}_{\text{numerically}}$$

# partonic ingredients for $e^+e^- \rightarrow 3$ jets at NNLO

- 2-loop virtual

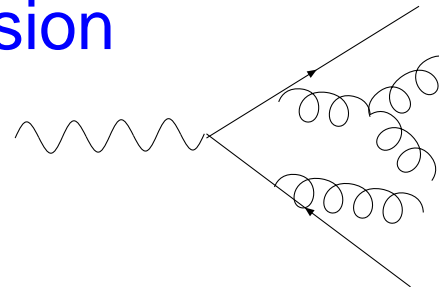


- one-loop plus single unresolved real emission



- double unresolved real emission

**bottleneck:** 5 partons in final state,  
up to 2 soft or collinear



**difficulty:**

isolation of infrared poles  
from phase space integrals



# subtraction of infrared poles: NNLO

*m*-jet production schematically:

$$\begin{aligned} d\sigma_{NNLO} = & \underbrace{\int_{d\Phi_{m+2}} \left( d\sigma_{NNLO}^R - d\sigma_{NNLO}^S \right)}_{\text{finite}} + \int_{d\Phi_{m+2}} d\sigma_{NNLO}^S \\ & + \underbrace{\int_{d\Phi_{m+1}} \left( d\sigma_{NNLO}^{V,1} - d\sigma_{NNLO}^{VS,1} \right)}_{\text{finite}} + \int_{d\Phi_{m+1}} d\sigma_{NNLO}^{VS,1} \\ & + \int_{d\Phi_m} d\sigma_{NNLO}^{V,2} \end{aligned}$$

$$\int_{d\Phi_{m+2}} d\sigma_{NNLO}^S + \int_{d\Phi_{m+1}} d\sigma_{NNLO}^{VS,1} + \int_{d\Phi_m} d\sigma_{NNLO}^{V,2} = \text{finite}$$

# subtraction of infrared poles: NNLO

---

two conceptually different approaches:

- "conventional" approach:

manual construction of a **subtraction scheme** and **analytic** integration over subtraction terms in

$D = 4 - 2\epsilon$  dimensions

[A. Gehrmann-De Ridder, T. Gehrmann, N. Glover], [Kilgore], [Weinzierl],  
[Del Duca, Somogyi, Trocsanyi], [Frixione, Grazzini]

- **sector decomposition**: automated isolation of IR poles in parameter space and **numerical** integration of pole coefficients

[Binoth, GH], [Anastasiou, Melnikov, Petriello]

# sector decomposition

---

- no manual construction of subtraction terms
- isolation of poles in  $1/\epsilon$  by **automated procedure** acting in parameter space
- pole coefficients will be complicated functions  
⇒ integrate **numerically**

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- development as a powerful tool for differential NNLO calculations [Anastasiou, Melnikov, Petriello:  $e^+e^- \rightarrow 2$  jets,  $H$  production,  $\mu$  decay,  $W$  production '04-06]

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- $e^+e^- \rightarrow 3$  jets at NNLO: very complicated singularity structure due to high number of massless particles

# basics of sector decomposition

---

integral of matrix element squared with some measurement function  $\mathcal{J}$ :

typically contains "overlapping" structures like

$$\begin{aligned} \int d\Phi^{(D)} |\text{ME}|^2 \mathcal{J} &\sim \int ds_{13} ds_{23} s_{13}^{-1-\epsilon} \frac{\mathcal{J}(s_{13}, s_{23})}{s_{13} + s_{23}} \\ &\sim \int_0^1 dx dy x^{-1-\epsilon} \frac{\mathcal{J}(x, y)}{x + y} \end{aligned}$$

singularities for  $x, y \rightarrow 0$  need to be factorised

**sector decomposition** is an algorithmic way to factorise this type of entangled singularities

# sector decomposition

---

$$I = \int_0^1 dx dy x^{-1-\epsilon} (x+y)^{-1} \mathcal{J}(x, y) \left[ \underbrace{\Theta(x-y)}_{(1)} + \underbrace{\Theta(y-x)}_{(2)} \right]$$

subst. (1)  $y = xt$       (2)  $x = yt$

$$I = \int_0^1 dx x^{-1-\epsilon} \int_0^1 dt (1+t)^{-1} \mathcal{J}(x, xt) \\ + \int_0^1 dy y^{-1-\epsilon} \int_0^1 dt t^{-1-\epsilon} (1+t)^{-1} \mathcal{J}(yt, y)$$

⇒ singularities **factorised**, **number of integrals doubled**



# general algorithm

---

- map parameter integrals to **unit hypercube** (manual)
- map singularities to be located at the **origin** of parameter space (manual/automated)

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result:

$$I = \int_0^1 dx_1 x_1^{b_1 - \kappa_1 \epsilon} \dots \int_0^1 dx_n x_n^{b_n - \kappa_n \epsilon} F(x_1, \dots, x_n)$$
$$\lim_{x_i \rightarrow 0} F(x_1, \dots, x_n) = \text{const}$$

# general algorithm

---

- perform subtractions and expansion in  $\epsilon$  (fully automated)

use identities like

$$\int_0^1 dx \int_0^1 dy x^{-1-\kappa\epsilon} f(x, y) =$$
$$-\frac{1}{\kappa\epsilon} \int_0^1 dx \delta(x) \int_0^1 dy f(x, y) + \int_0^1 dx \int_0^1 dy x^{-\kappa\epsilon} \frac{f(x, y) - f(0, y)}{x}$$

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note: if  $f(x, y) = \Theta(x - a) g(y) \Rightarrow$  pole term zero

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- result after  $\epsilon$ -expansion: **Laurent series in  $\epsilon$**

$$I = \sum_{k=\text{maxpole}}^{-n} C_k(y_i) / \epsilon^k + \mathcal{O}(\epsilon^{n+1}) \quad (y_i \text{ scaled invariants } s_{ij})$$

- poles are isolated  $\Rightarrow$  integrate finite coefficient functions  $C_k(y_i)$  **numerically** over the phase space

# application to $1 \rightarrow 5$ parton phase space

---

use scaled invariants  $y_1 = s_{12}/q^2, \dots, y_{10} = s_{45}/q^2$

$$\int d\Phi_{1 \rightarrow 5}^D = C_{\Gamma}^{(5)} \int \prod_{j=1}^{10} dy_j \delta\left(1 - \sum_{i=1}^{10} y_i\right) (-\Delta_5)^{\frac{D}{2}-3} \Theta(-\Delta_5)$$



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$$\begin{aligned} \Delta_5 = & y_{10}^2 y_1 y_2 y_3 + y_9^2 y_1 y_4 y_5 + y_8^2 y_2 y_4 y_6 + y_7^2 y_3 y_5 y_6 \\ & + y_6^2 y_1 y_7 y_8 + y_5^2 y_2 y_7 y_9 + y_4^2 y_3 y_8 y_9 + y_3^2 y_4 y_7 y_{10} \\ & + y_2^2 y_5 y_8 y_{10} + y_1^2 y_6 y_9 y_{10} \\ & + y_{10} [y_2 y_3 y_5 y_7 + y_1 y_3 y_6 y_7 + y_2 y_3 y_4 y_8 \\ & + y_1 y_2 y_6 y_8 + y_1 y_3 y_4 y_9 + y_1 y_2 y_5 y_9] \\ & + y_9 [y_4 y_5 (y_3 y_7 + y_2 y_8) + y_1 y_6 (y_5 y_7 + y_4 y_8)] \\ & + y_6 y_7 y_8 (y_3 y_4 + y_2 y_5) \end{aligned}$$

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- perform variable transformations to map integrations to unit hypercube (solve constraint  $\Delta_5 = 0$ )

can be done once and for all, but **costly in number of iterations** for certain denominators

**better:**

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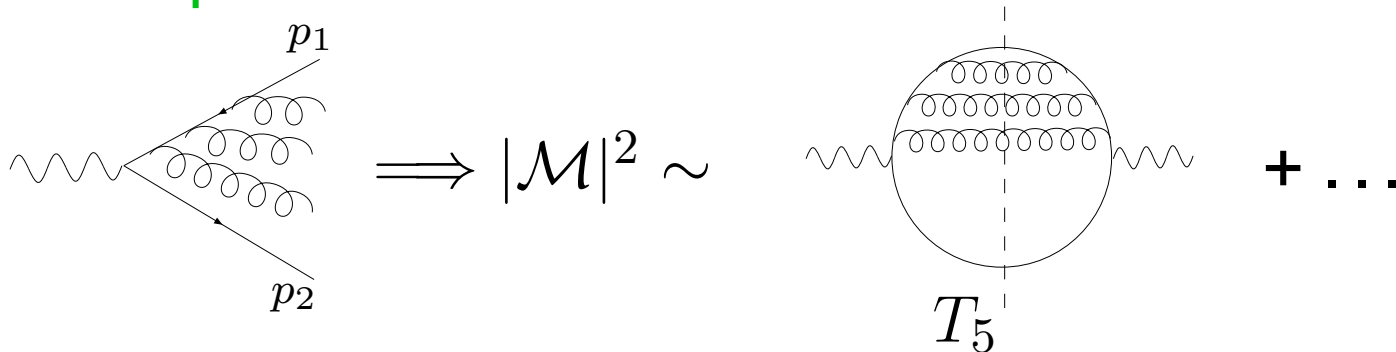
can be done once and for all, but **costly in number of iterations** for certain denominators

**better:**

- use different parametrisations, optimized for certain denominator structures ("**topologies**")  
(minimise square-root terms in denominators, maximize natural factorisations)

# example from $e^+e^- \rightarrow 3$ jets

example:



convenient phase space parametrisation:

$$s_{1345}/q^2 = t_1, s_{134}/q^2 = t_1 t_2, s_{13}/q^2 = t_1 t_2 t_3, \dots$$

$$s_{24}/q^2 = y_5^- + (y_5^+ - y_5^-) t_5, y_5^\pm \text{ solution of } \Delta_5 = 0,$$

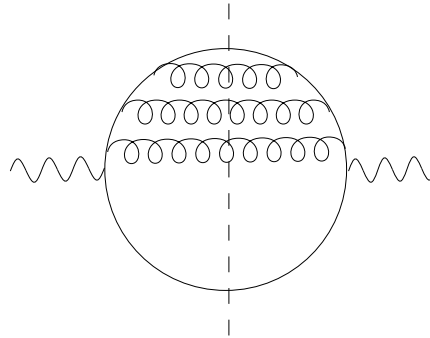
$s_{25}, s_{45}$  also contain square-roots

$$\int d\Phi_{1 \rightarrow 5}^D = \mathcal{K}_\Gamma^{(5)}(q^2)^{2D-5} \int_0^1 \prod_{j=1}^9 dt_j t_1^{2-3\epsilon} [t_5(1-t_5)]^{-1-\epsilon} [t_8(1-t_8)t_9(1-t_9)]^{-\frac{1}{2}-\epsilon}$$

$$[(1-t_1)t_2(1-t_2)(1-t_3)]^{1-2\epsilon} [t_3 t_4(1-t_4)t_6(1-t_6)t_7(1-t_7)]^{-\epsilon}$$

# example from $e^+e^- \rightarrow 3$ jets

result for example graph  $T_5$ :



$$\begin{aligned} T_5 = & C_F^3 \left( \frac{\alpha_s}{4\pi} \right)^3 T_2 \left\{ - \frac{0.166618 \pm 0.000086}{\epsilon^3} \right. \\ & - \frac{1}{\epsilon^2} \left[ (1.49928 \pm 0.00148) - (0.499853 \pm 0.000258) \log \left( \frac{Q^2}{\mu^2} \right) \right] \\ & - \frac{1}{\epsilon} \left[ (5.59588 \pm 0.0064) - (4.49783 \pm 0.0044) \log \left( \frac{Q^2}{\mu^2} \right) \right. \\ & \left. \left. + (0.749779 \pm 0.00039) \log^2 \left( \frac{Q^2}{\mu^2} \right) \right] + \text{finite} \right\} \end{aligned}$$

# check by Kinoshita-Lee-Nauenberg theorem

$$T_5 + z_1 T_4 + z_2 T_3 + z_3 T_2 = \text{finite}$$

renormalisation constants:

$$z_1 = C_F \frac{\alpha_s}{4\pi} \frac{1}{\epsilon}, \quad z_2 = C_F^2 \left( \frac{\alpha_s}{4\pi} \right)^2 \left( \frac{1}{2\epsilon^2} - \frac{1}{4\epsilon} \right), \quad z_3 = C_F^3 \left( \frac{\alpha_s}{4\pi} \right)^3 \left( \frac{1}{6\epsilon^3} - \frac{1}{4\epsilon^2} + \frac{1}{6\epsilon} \right)$$

e.g.  $z_3$  from

$$I_3 - I_3^{s_1} - \left[ I_3^{s_2} - I_3^{s_2 s_1} \right]$$

— [overall divergence of expressions above]

# check pole cancellations

---

$$z_1 T_4 + z_2 T_3 + z_3 T_2 =$$

$$C_F^3 \left(\frac{\alpha_s}{4\pi}\right)^3 T_2 \left\{ \frac{1}{6\epsilon^3} + \frac{1}{2\epsilon^2} \left[ 3 - \log\left(\frac{Q^2}{\mu^2}\right) \right] \right. \\ \left. + \frac{1}{\epsilon} \left[ 5.60813 - \frac{9}{2} \log\left(\frac{Q^2}{\mu^2}\right) + \frac{3}{4} \log^2\left(\frac{Q^2}{\mu^2}\right) \right] + \text{finite} \right\}$$

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# differential results

---

- in order to compare to experimental data, we need to produce **distributions** which are **differential in certain observables**



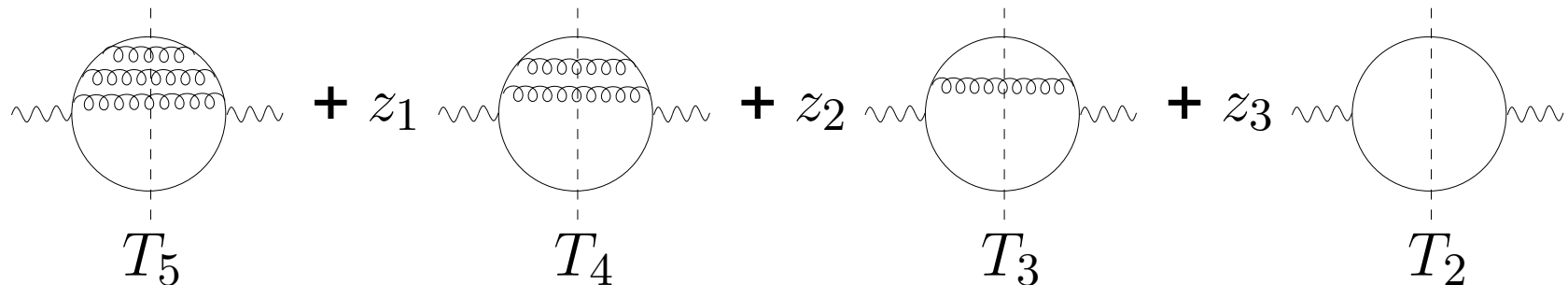
# differential results

---

- in order to compare to experimental data, we need to produce **distributions** which are **differential in certain observables**
- **no problem:** before numerical integration, pole coefficients and finite parts are **functions of invariants**  
 $s_{12}, \dots, s_{45}$ 
  - ⇒ 4-momenta of all final state particles **can be reconstructed**
  - ⇒ program has architecture of **partonic event generator**
  - ⇒ flexibility to include **experimental cuts**, jet algorithms, definition of shape observables, etc. **at the Monte Carlo level**

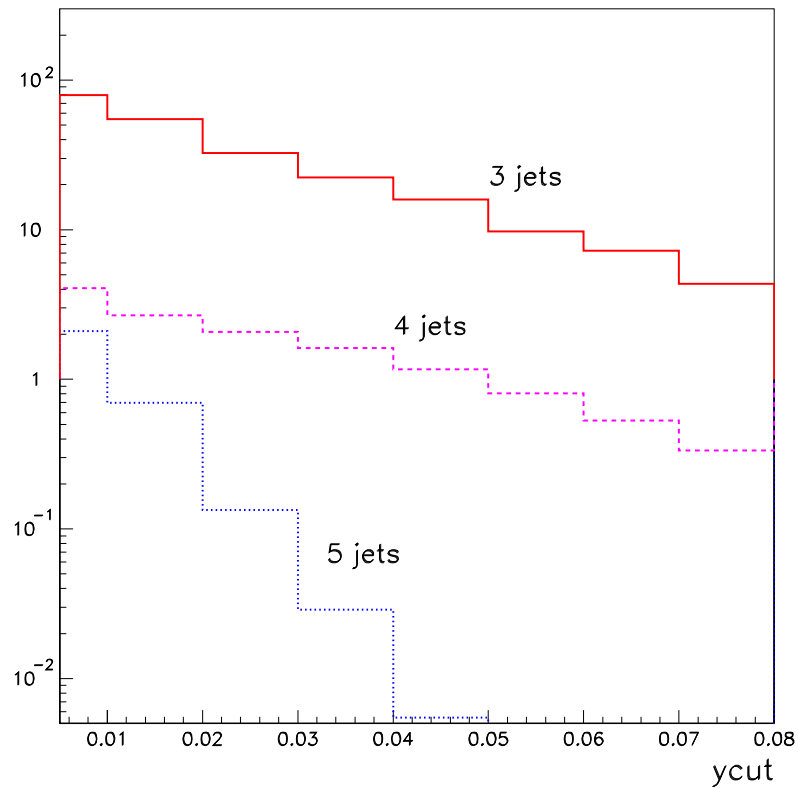
# example

## 3,4,5-jet rates for "ladder" contribution



- virtual contributions calculated analytically  
(only renormalisation factors for ladder graph)
- phase space integrations for 3,4,5-parton final states by Monte Carlo program based on output of sector decomposition for  $T_4$  and  $T_5$

# example: jet rates for ladder graph

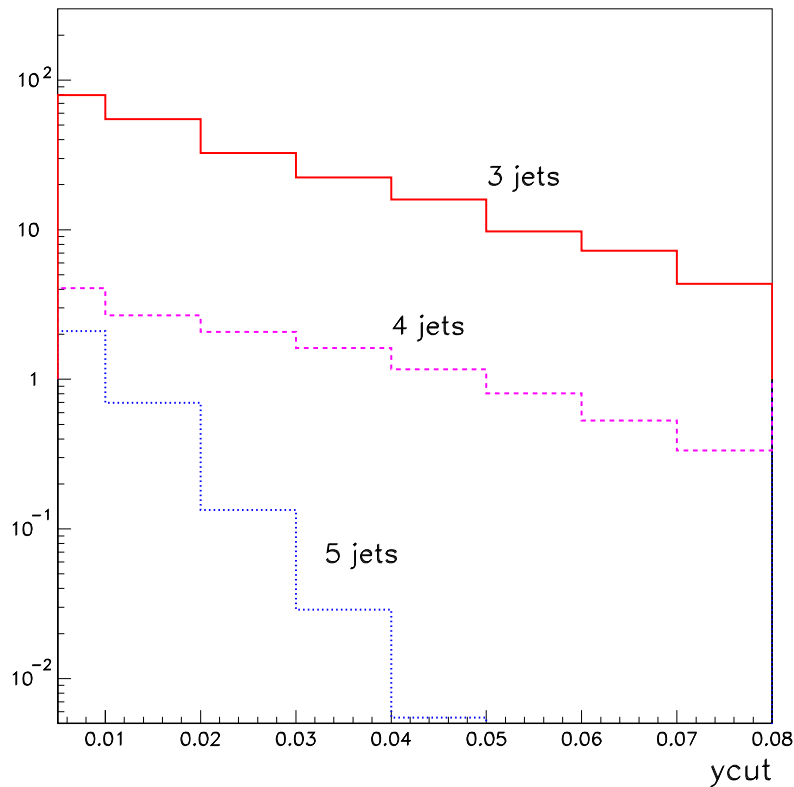


$y^{\text{cut}}$ : minimal separation between jets  
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# example: jet rates for ladder graph

note:

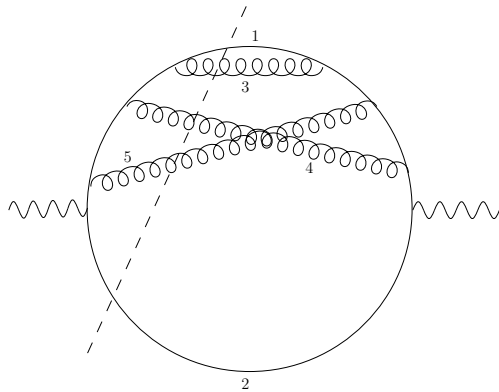
- ladder graph only, not a physical observable, but architecture of program as a partonic event generator same for remaining parts
- CPU time  $\mathcal{O}(10 \text{ min})$  for 1% precision (2.8 GHz Pentium IV)



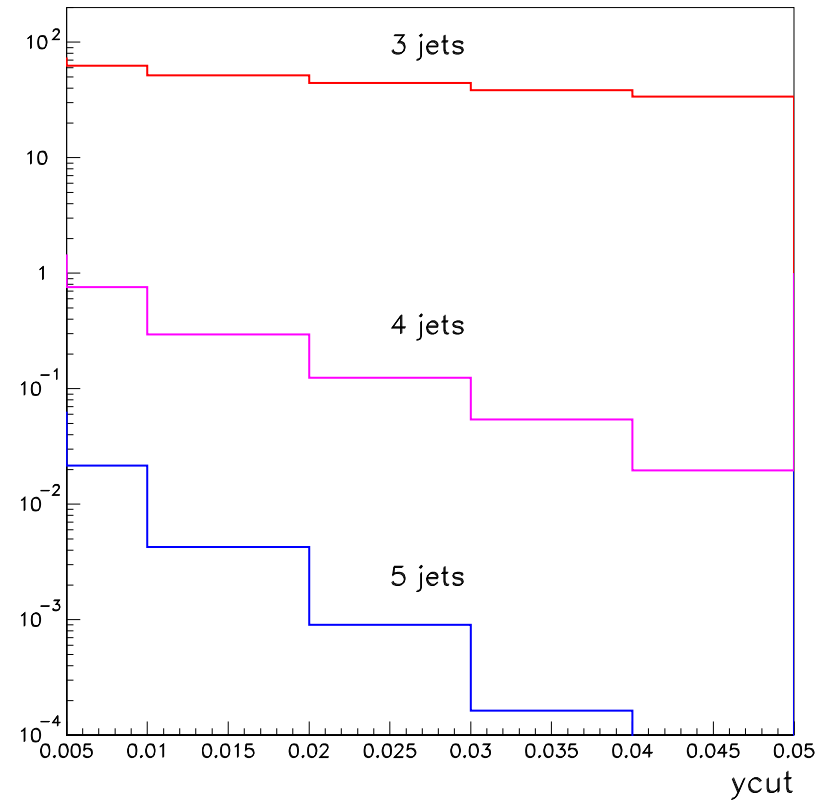
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# a non-planar topology

more complex because square-root term in denominator unavoidable

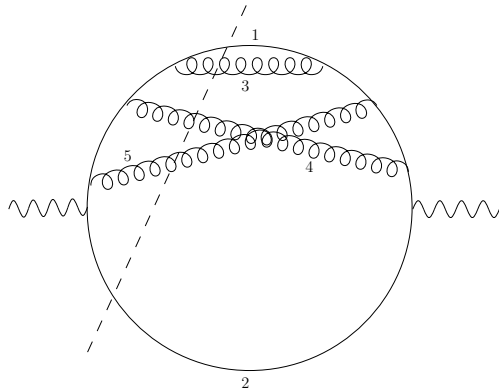


magnitude of jet rates for non-planar topology  
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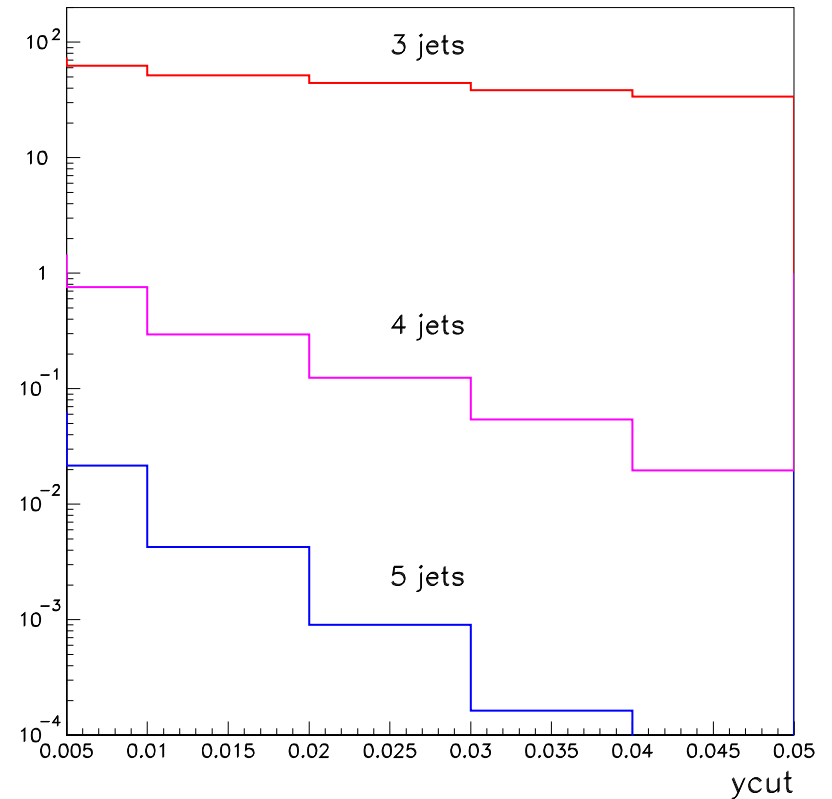
more complex because square-root term in denominator unavoidable



note:

- virtual corrections not yet included
- CPU time  $\mathcal{O}(2\text{ h})$  for 1% precision
- other topologies can be calculated in parallel
- $\mathcal{O}(100)$  topologies
- $\mathcal{O}(10)$  PS parametrisations

magnitude of jet rates for non-planar topology  
(5-parton channel only)



# roadmap

---

- include all topologies of  $e^+e^- \rightarrow q\bar{q}ggg, q\bar{q}Q\bar{Q}g$  squared matrix elements

limit size of expressions produced by iterated sector decomposition by using convenient phase space parametrisations and information on physical limits

- combine with one-loop + single real and two-loop virtual corrections
  - one-loop + single real: use a combination of analytic integration and sector decomposition
  - two-loop virtual: use analytic expressions to save CPU time

[Garland, Gehrmann, Glover, Koukoutsakis, Remiddi '01],

[Moch, Uwer, Weinzierl '02]

# Summary: comparison of the two approaches

---

## analytic subtraction

- ⊕ moderate number of subtraction terms
- ⊕ maximal (analytical) control over pole parts
- ⊕ insights into infrared structure of QCD
- ⊖ different for each colour structure
- ⊖ **analytical** integration of subtraction terms may become impossible for processes involving **several mass scales**

## sector decomposition

- ⊖ produces large expressions
- ⊖ numerical cancellation of pole coefficients
- ⊕ high level of automatisisation
- ⊕ basic algorithm same for all colour structures of a given process
- ⊕ subtraction terms are integrated **numerically**  $\Rightarrow$  no need to have simple subtraction terms  $\Rightarrow$  **application to other processes easier**



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the two methods are complementary

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- ⊖ **analytical** integration of subtraction terms may become impossible for processes involving **several mass scales**

## sector decomposition

- ⊖ produces large expressions
- ⊖ numerical cancellation of pole coefficients
- ⊕ high level of automatisisation
- ⊕ basic algorithm same for all colour structures of a given process
- ⊕ subtraction terms are integrated **numerically**  $\Rightarrow$  no need to have simple subtraction terms  $\Rightarrow$  **application to other processes easier**

the sector decomposition approach has been/will be a useful tool for NNLO calculations where analytical methods reach their limits

# backup

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for Monte Carlo program: remap to energies and angles

$$E_1 = \frac{q^2 - s_{2345}}{2q}, \quad E_2 = \frac{q^2 - s_{1345}}{2q},$$

$$E_3 = \frac{q^2 - s_{1245}}{2q}, \quad E_4 = \frac{q^2 - s_{1235}}{2q}$$

$$\cos \theta_1 = -1 + 2 (s_{1345}s_{2345} - s_{345}) / (1 - s_{1345}) / (1 - s_{2345})$$

$$\cos \theta_2 = -1 + 2 (s_{1245}s_{2345} - s_{245}) / (1 - s_{1245}) / (1 - s_{2345})$$

$$\cos \theta_3 = -1 + 2 (s_{1235}s_{2345} - s_{235}) / (1 - s_{1235}) / (1 - s_{2345})$$

⋮