

Double-Real-Virtual and Double-Virtual-Real Corrections to the Three-Loop Thrust Soft Function

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① Introduction

- Thrust observable
- Resummation
- Soft function

② Linear reduction of parametric integrals

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Definition

Thrust Brandt et al., PL (1964), Farhi, PRL (1977)

$$T = 1 - \tau = \text{Max}_{\hat{\mathbf{n}}} \frac{\sum_i |\hat{\mathbf{n}} \cdot \vec{k}_i|}{\sum_i |\vec{k}_i|}, \quad (1)$$

where $\vec{k}_i$ are the momenta of the final-state particles or jets, and the maximum is obtained for the Thrust axis $\hat{\mathbf{n}}$.

- One of the fundamental tools to test the theory of strong interactions (such as the asymptotic freedom of QCD)
- Can be measured very accurately
- Infrared safe, theoretically clean, and feasible to high perturbative order computations
- Suitable for the determination of the strong coupling $\alpha_s(M_Z)$ with a high precision

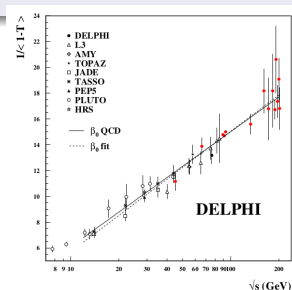


Figure: $\frac{1}{\langle 1-T \rangle}$ as a function of the cms energy. Kluth (2006)

Near the dijet limit ($\tau \rightarrow 0$), fixed-order perturbative calculation breaks down due to the presence the large logarithms.

$$\frac{d\sigma}{d\tau} = \sum_{n=0}^{\infty} \sum_{k=1}^{2n+1} \alpha_s^n C_k^{(n)} \frac{1}{\mu} \mathcal{L}_{2n-k} \left(\frac{\tau}{\mu} \right), \quad (2)$$

where the logarithms

$$\mathcal{L}_{2n-k}(\tau) = \left(\frac{\ln^{2n-k} \tau}{\tau} \right)_+,$$

$$\mathcal{L}_{-1}(\tau) = \delta(\tau).$$

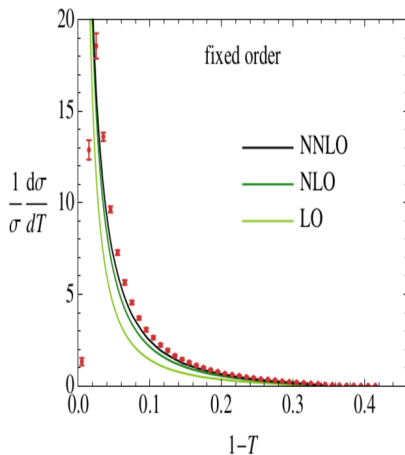


Figure: Fixed-order distribution Becher & Schwartz (2008)

Soft-collinear effective theory (SCET) provides a systematic method to resum large logarithms. Near the dijet region, the thrust distribution is factorized in SCET: [Becher & Schwartz, JHEP \(2008\)](#)

$$\frac{1}{\sigma_0} \frac{d\sigma_{sing.}}{d\tau} = H(\mu) \int \prod_{i=n,\bar{n},s} d\tau_i \mathcal{J}_n(\tau_n, \mu) \mathcal{J}_{\bar{n}}(\tau_{\bar{n}}, \mu) S(\tau_s) \delta(\tau - \tau_n - \tau_{\bar{n}} - \tau_s, \mu),$$

where σ_0 is the leading order cross section for $e^+e^- \rightarrow q\bar{q}$. We assume that q is along the light-like direction $n = (1, 0, 0, 1)$ while $\bar{q}$ along $\bar{n} = (1, 0, 0, -1)$. H is the hard function, $\mathcal{J}$ is the inclusive jet function, and S is the soft function defined as the vacuum expectation of Wilson lines.

The logarithmic terms can be resummed to all orders through the standard resummation techniques.

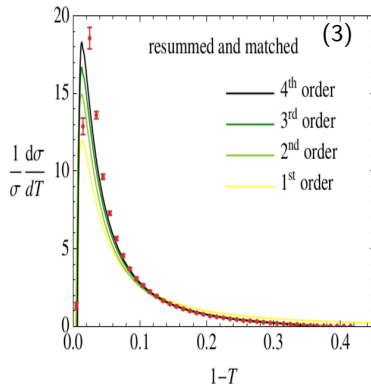


Figure: Resummed distribution [Becher & Schwartz \(2008\)](#)

Definition

Soft function

$$S(\tau) = \frac{1}{N_c} \sum_X \text{Tr} \left\{ \langle \Omega | Y_{\bar{n}}^\dagger Y_n | X \rangle \langle X | Y_n^\dagger Y_{\bar{n}} | \Omega \rangle \right\} \delta \left(\tau - \sum_k \min \{ k \cdot n, k \cdot \bar{n} \} \right), \quad (4)$$

where Y_n and $Y_{\bar{n}}$ are the soft Wilson lines, $|\Omega\rangle$ is the vacuum, and the summation is taken over all the final hadronic states of soft scales.

Known results:

- two-loop
Monni et al. JHEP(2011),
Kelley et al. PRD(2011),
Boughezal et al. PRD(2015)
- three-loop
triple-real:
Baranowski et al. PRD(2022)
double-real-virtual &
double-virtual-real:

Logarithmic Order	fixed-order matching	Anomalous Dimension γ_i	Γ_{cusp}
LL	1	-	1-loop
NLL	1	1-loop	2-loop
NLL'	α_s	1-loop	2-loop
NNLL	α_s	2-loop	3-loop
NNLL'	α_s^2	2-loop	3-loop
N ³ LL	α_s^2	3-loop	4-loop
N ³ LL'	α_s^3	3-loop	4-loop
N ⁴ LL	α_s^3	4-loop	5-loop

Chen et al. arXiv:2206.12323

Table: The definitions for the logarithmic accuracy of the resummation calculation.

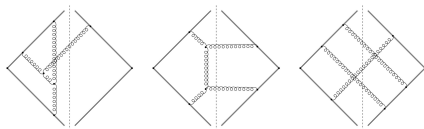


Figure: Representative diagrams for three-loop thrust soft function.

Double-real-virtual (RRV) contribution:

$$S_{RRV}^{(3)}(\tau; \epsilon) = \int d\Phi_2 \Theta(\tau; k_1, k_2) \int \frac{d^D l}{(2\pi)^D} \omega_{RRV}^{(3)}(l, k_1, k_2; n, \bar{n}), \quad (5)$$

where $d\Phi_n$ denotes the n -body phase-space integration measure, $\omega_{RRV}^{(3)}$ is the squared amplitude, and

$$\Theta(\tau; k_1, k_2) = \int d\tau_1 d\tau_2 \delta(\tau - \tau_1 - \tau_2) \Theta_{\tau_1}(k_1) \Theta_{\tau_2}(k_2),$$

with

$$\Theta_{\tau}(k) \equiv \theta(k^+ - k^-) \delta(\tau - k^-) + \theta(k^- - k^+) \delta(\tau - k^+).$$

Difficulty: Traditional integration-by-parts (IBP) method and differential-equation (DE) technique break down due to the presence of Heaviside theta functions.

Solution: Integrals with theta functions can be reduced by constructing and solving linear relations in the parametric representation. Chen JHEP(2020), EPJC(2020, 2021)

$$\begin{aligned} \frac{1}{D_i^{\lambda_i+1}} &\Longleftrightarrow \frac{e^{-\frac{\lambda_i+1}{2}i\pi}}{\Gamma(\lambda_i+1)} \int_0^\infty dx_i e^{ix_i D_i} x_i^{\lambda_i} \\ \theta(D_i) &\Longleftrightarrow -\frac{i}{2\pi} \int_{-\infty}^\infty dx_i \frac{e^{ix D_i}}{x_i + i0^+} \end{aligned}$$

We generalize theta function and define

$$w_\lambda(u) \equiv e^{-\frac{\lambda+1}{2}i\pi} \int_{-\infty}^\infty dx \frac{1}{x^{\lambda+1}} e^{ixu}. \quad (6)$$

Obviously, $w_0(u) = 2\pi\theta(u)$, $w_{-1}(u) = 2\pi\delta(u)$, and $w_{-2}(u) = 2\pi\delta'(u)$.

We consider the parametrization of a general scalar integral:

$$J(\lambda_1, \lambda_2, \dots, \lambda_n) = \int [dl_1][dl_2] \cdots [dl_L] \frac{w_{\lambda_1}(D_1) w_{\lambda_2}(D_2) \cdots w_{\lambda_m}(D_m)}{D_{m+1}^{\lambda_{m+1}+1} D_{m+2}^{\lambda_{m+2}+1} \cdots D_n^{\lambda_n+1}}, \quad (7)$$

where L is the number of loops, l_i are the loop momenta, D_i are the denominators of propagators, and we denote the integration measure as $[dl_i] \equiv \frac{1}{\Gamma(1+\epsilon)} \frac{d^d l_i}{\pi^{d/2}}$ with d the space-time dimension.

$$J = s_g^{-\frac{L}{2}} e^{i\pi\lambda_f} I(\lambda_0, \lambda_1, \dots, \lambda_n) = s_g^{-\frac{L}{2}} e^{i\pi\lambda_f} \int d\Pi^{(n+1)} \mathcal{I}^{(-n-1)}, \quad \text{with} \quad (8)$$

$$\mathcal{I}^{(-n-1)} = \frac{\Gamma(-\lambda_0)}{\Gamma(1+\epsilon)^L \prod_{i=m+1}^{n+1} \Gamma(\lambda_i + 1)} \mathcal{F}^{\lambda_0} \prod_{i=1}^{n+1} x_i^{\lambda_i}. \quad (9)$$

Here s_g the determinant of the d -dimensional space-time metric, $\lambda_0 = -d/2$, and $\lambda_f = \frac{1}{2}Ld - \frac{1}{2}m - \sum_{i=m+1}^n (\lambda_i + 1)$. The integration measure

$$d\Pi^{(n+1)} \equiv \prod_{i=1}^{n+1} dx_i \delta(1 - f(x)), \quad (10)$$

with the positive definite function $f(x)$ satisfying $f(\alpha x) = \alpha f(x)$. The polynomial $\mathcal{F}$ is related to the Symanzik polynomials U and F through

$$\mathcal{F}(x) \equiv F(x) + U(x)x_{n+1}, \quad \text{with} \quad (11)$$

$$U(x) \equiv \det A, \quad \text{and} \quad F(x) \equiv U(x) \left(\sum_{i,j=1}^L (A^{-1})_{ij} B_i \cdot B_j - C \right). \quad (12)$$

Here A , B , and C are linear in x and are determined from $\sum_{i=1}^n x_i D_i \equiv \sum_{i,j=1}^L A_{ij} l_i \cdot l_j + 2 \sum_{i=1}^L B_i \cdot l_i + C$.

By virtue of the homogeneity of the integrands of the parametric integrals, it can be proven that

$$0 = \int d\Pi^{(n+1)} \frac{\partial}{\partial x_i} \mathcal{I}^{(-n-1)}, \quad i = 1, 2, \dots, m, \quad (13a)$$

$$0 = \int d\Pi^{(n+1)} \frac{\partial}{\partial x_i} \mathcal{I}^{(-n-1)} + \delta_{\lambda_i 0} \int d\Pi^{(n)} \mathcal{I}^{(-n)} \Big|_{x_i=0}, \quad i = m+1, m+2, \dots, n+1. \quad (13b)$$

A parametric integral can be understood as a function of the indices λ_i . We define the operators $\mathcal{R}_i$, $\mathcal{D}_i$, and $\mathcal{A}_i$, such that.

$$\hat{\mathcal{R}}_i I(\lambda_0, \dots, \lambda_i, \dots) = (\lambda_i + 1) I(\lambda_0, \dots, \lambda_i + 1, \dots),$$

$$\hat{\mathcal{D}}_i I(\lambda_0, \dots, \lambda_i, \dots) = I(\lambda_0, \dots, \lambda_i - 1, \dots),$$

$$\hat{\mathcal{A}}_i I(\lambda_0, \dots, \lambda_i, \dots) = \lambda_i I(\lambda_0, \dots, \lambda_i, \dots).$$

And we define

$$\hat{x}_i = \mathcal{D}_i, \quad i = 1, 2, \dots, m,$$

$$\hat{x}_i = \mathcal{R}_i, \quad i = m+1, m+2, \dots, m,$$

$$z_i = -\mathcal{R}_i, \quad i = 1, 2, \dots, m,$$

$$z_i = \mathcal{D}_i, \quad i = m+1, m+2, \dots, n,$$

$$\hat{a}_i = -\mathcal{A}_i - 1, \quad i = 1, 2, \dots, m,$$

$$\hat{a}_i = \mathcal{A}_i, \quad i = m+1, m+2, \dots, n.$$

We further introduce the operators $\hat{x}_{n+1}$ and $\hat{z}_{n+1}$ formally defined by $\hat{z}_{n+1}I = I$ and $\hat{x}_{n+1}^i I = (\hat{a}_{n+1} + 1)(\hat{a}_{n+1} + 2) \dots (\hat{a}_{n+1} + i)I$, with $\hat{a}_{n+1} \equiv -(L+1)\mathcal{A}_0 - \sum_{i=1}^n (\hat{a}_i + 1)$. The eq. (13) can be written in the following form:

$$\left(\mathcal{D}_0 \frac{\partial \mathcal{F}(\hat{x})}{\partial \hat{x}_i} - \hat{z}_i \right) I = 0, \quad i = 1, 2, \dots, n+1. \quad (14)$$

Let y be a kinematical variable, and we assume that the polynomial $U(x)$ is free of y , then the parametric integrals satisfy the differential equation

$$\frac{\partial}{\partial y} I = -\mathcal{D}_0 \frac{\partial \mathcal{F}}{\partial y} I. \quad (15)$$

We introduce the dimensionless variables by re-scaling the momenta as $\tau_i \rightarrow \hat{\tau}_i \tau$, $k_i \rightarrow \hat{k}_i \tau$ and $l \rightarrow \hat{l} \tau$, to factorize out the τ dependence from the rest of the integral and find

$$S_{RRV}^{(3)}(\tau; \epsilon) = \tau^{-1-6\epsilon} \int d\hat{\Phi}_2 \frac{d^D \hat{l}}{(2\pi)^D} \omega_{RRV}^{(3)}(\hat{l}, \hat{k}_1, \hat{k}_2; n, \bar{n}) \Theta(1; \hat{k}_1, \hat{k}_2),$$

Thus we see that the τ -dependence of the soft function is trivial. An extra scale can be introduced by inserting into the master integrals a trivial integral of the form $\int dy \delta(K - y)$, with K a linear combination of Lorentz scalars of the loop momenta. That is

$$J_i \equiv \int [dk_1][dk_2][dl] \mathcal{J} = \int dy \int [dk_1][dk_2][dl] \delta(K - y) \mathcal{J} \equiv \int \frac{dy}{2\pi} J'_i(y),$$

$$\text{Integrals free of theta functions:} \quad K = k_1 \cdot k_2, \quad y = \frac{1}{2}(1 - x)^2,$$

$$\text{Integrals containing theta functions:} \quad K = k_1^{+/-} + k_2^{+/-}, \quad y = \frac{1}{x}.$$

Integrals J_i can be obtained from $J'_i(y)$ by integrating out y . For integrals with $K = k_1 \cdot k_2 - y$, the integration is straightforward. For integrals with $K = k_1^{+/-} + k_2^{+/-}$, $J_i(y)$ is singular at $y = \infty$ ($x = 0$). The integration can be carried out by subtracting the singular part of $J(y)$ (denoted by $\text{Sing}\{J(y)\}$) and integrating the singular part in d dimensions. That is,

$$\begin{aligned} J_i &= \int_0^\infty \frac{dy}{2\pi} J'_i(y) \\ &= \int_0^\infty \frac{dy}{2\pi} \text{Ser}\{J'_i(y) - \text{Sing}\{J'(y)\}\} + \int_0^\infty \frac{dy}{2\pi} \text{Sing}\{J'(y)\}. \end{aligned} \tag{16}$$

Here we use Ser to denote the series expansion of a function with respect to ϵ .

We decompose the two-gluon-virtual contribution according to the colour structures by

$$\hat{S}_{\text{RRV,gg}}^{(3)} = (4\pi)^6 \cos(\pi\epsilon) \alpha_s^3 C_A C_F \times \left(N_f \hat{S}_{\text{RRV,gg},a}^{(3)} + C_A \hat{S}_{\text{RRV,gg},b}^{(3)} + C_F \hat{S}_{\text{RRV,gg},c}^{(3)} \right). \quad (17)$$

Here

$$\begin{aligned} \hat{S}_{\text{RRV,gg},a}^{(3)} = & \frac{1}{54\epsilon^3} + \frac{31}{162\epsilon^2} + \frac{1}{\epsilon} \left(\frac{95}{81} - \frac{1}{9}\zeta_2 \right) + \frac{17}{27}\zeta_2 - \frac{41}{27}\zeta_3 + \frac{3778}{729} \\ & + \epsilon \left[\frac{62}{27}\zeta_2 + \frac{43}{81}\zeta_3 - \frac{149}{18}\zeta_4 + \frac{39568}{2187} \right], \end{aligned} \quad (18)$$

$$\begin{aligned} \hat{S}_{\text{RRV,gg},b}^{(3)} = & -\frac{5}{3\epsilon^5} - \frac{523}{144\epsilon^4} + \frac{1}{\epsilon^3} \left(\frac{34}{3}\zeta_2 - \frac{2129}{216} \right) + \frac{1}{\epsilon^2} \left(\frac{409}{24}\zeta_2 + 42\zeta_3 - \frac{76}{3} \right) \\ & + \frac{1}{\epsilon} \left(-\frac{386}{3}\zeta_2 + \frac{14399}{72}\zeta_3 + \frac{478}{3}\zeta_4 - \frac{101329}{1944} \right) - \frac{596}{3}\zeta_3\zeta_2 \\ & + \frac{6277}{54}\zeta_2 - \frac{121919}{108}\zeta_3 + \frac{8889}{8}\zeta_4 + \frac{2360}{3}\zeta_5 - 4\log(2)\zeta_2 - \frac{649801}{5832} \\ & + 1244.294408\epsilon, \end{aligned} \quad (19)$$

and

$$\hat{S}_{\text{RRV,gg},c}^{(3)} = \frac{6}{\epsilon^5} - \frac{60}{\epsilon^3}\zeta_2 - \frac{300}{\epsilon^2}\zeta_3 - \frac{810}{\epsilon}\zeta_4 + 3000\zeta_2\zeta_3 - 8100\zeta_5 + \epsilon [7500\zeta_3^2 - 19635\zeta_6]. \quad (20)$$

Similarly, for the two-ghost-virtual contribution, we have

$$\hat{S}_{\text{RRV,gh.gh.}}^{(3)} = (4\pi)^6 \alpha_s^3 C_A C_F \left(N_f \hat{S}_{\text{RRV,gh.gh.},a}^{(3)} + C_A \hat{S}_{\text{RRV,gh.gh.},b}^{(3)} \right), \quad (21)$$

with

$$\begin{aligned} \hat{S}_{\text{RRV,gh.gh.},a}^{(3)} = & -\frac{1}{108\epsilon^3} - \frac{13}{324\epsilon^2} + \frac{1}{\epsilon} \left(\frac{1}{18}\zeta_2 - \frac{10}{81} \right) - \frac{17}{54}\zeta_2 + \frac{41}{54}\zeta_3 - \frac{566}{729} \\ & + \epsilon \left[\frac{26}{27}\zeta_2 - \frac{457}{162}\zeta_3 + \frac{149}{36}\zeta_4 - \frac{14575}{4374} \right], \end{aligned} \quad (22)$$

and

$$\begin{aligned}
 \hat{S}_{\text{RRV,gh.gh.,}b}^{(3)} = & -\frac{5}{288\epsilon^4} - \frac{5}{144\epsilon^3} + \frac{1}{\epsilon^2} \left(\frac{5}{144}\zeta_2 - \frac{2}{81} \right) + \frac{1}{\epsilon} \left(-\frac{5}{27}\zeta_2 + \frac{11}{48}\zeta_3 - \frac{167}{3888} \right) \\
 & - \frac{55}{324}\zeta_2 - \frac{289}{216}\zeta_3 - \frac{1}{16}\zeta_4 + 2\log(2)\zeta_2 + \frac{35}{48} \\
 & + \epsilon \left[\frac{6583\zeta_2}{972} - \frac{655}{144}\zeta_2\zeta_3 - \frac{529}{162}\zeta_3 + \frac{2543}{144}\zeta_4 + \frac{425}{96}\zeta_5 + 4\log^2(2)\zeta_2 \right. \\
 & \left. - \frac{59}{6}\log(2)\zeta_2 - 24\text{Li}_4\left(\frac{1}{2}\right) + \frac{20513}{34992} - \log^4(2) \right].
 \end{aligned} \tag{23}$$

The double-virtual-real contribution reads

$$S_{V^2R}^{(3)}(\tau) = \frac{\alpha_{s,r}^3}{8\pi^3} \frac{1}{\mu} \left(\frac{\tau}{\mu} \right)^{-1-6\epsilon} \left(C_F C_A N_f S_{V^2R, C_F C_A n_f}^{(3)} + C_F C_A^2 S_{V^2R, C_F C_A^2}^{(3)} \right), \tag{24}$$

with

$$\begin{aligned}
S_{V^2 R, C_F C_A n_f}^{(3)} = & \frac{1}{9\epsilon^4} + \frac{5}{27\epsilon^3} + \frac{1}{\epsilon^2} \left(\frac{19}{81} - \frac{23}{18} \zeta_2 \right) + \frac{1}{\epsilon} \left(\frac{65}{243} - \frac{115}{54} \zeta_2 - \frac{7}{3} \zeta_3 \right) \\
& + \frac{211}{729} - \frac{545}{162} \zeta_2 - \frac{35}{9} \zeta_3 - \frac{13}{48} \zeta_4 \\
& + \left(\frac{665}{2187} - \frac{2359\zeta_2}{486} - \frac{223\zeta_3}{27} - \frac{65\zeta_4}{144} - \frac{341\zeta_5}{15} + \frac{161\zeta_3\zeta_2}{6} \right) \epsilon,
\end{aligned} \tag{25}$$

and

$$\begin{aligned}
S_{V^2 R, C_F C_A^2}^{(3)} = & -\frac{1}{3\epsilon^5} - \frac{11}{18\epsilon^4} - \frac{1}{\epsilon^3} \left(\frac{67}{54} + \frac{23}{6} \zeta_2 \right) - \frac{1}{\epsilon^2} \left(\frac{193}{81} - \frac{253}{36} \zeta_2 - 2\zeta_3 \right) \\
& + \frac{1}{\epsilon} \left(-\frac{1142}{243} + \frac{1541}{108} \zeta_2 + \frac{77}{6} \zeta_3 + \frac{409}{48} \zeta_4 \right) \\
& - \frac{6820}{729} + \frac{4547}{162} \zeta_2 + \frac{469}{18} \zeta_3 + \frac{143\zeta_4}{96} + \frac{52}{3} \zeta_2 \zeta_3 - \frac{122}{15} \zeta_5, \\
& + \left(-\frac{40856}{2187} + \frac{13403\zeta_2}{243} + \frac{1441\zeta_3}{27} + \frac{871\zeta_4}{288} + \frac{3751\zeta_5}{30} - \frac{1771\zeta_2\zeta_3}{12} \right. \\
& \left. - \frac{637\zeta_6}{1152} - \frac{31}{2} \zeta_3^2 \right) \epsilon,
\end{aligned} \tag{26}$$

- Some master integrals are numerically checked by using the sector decomposition method.
- The leading pole (ϵ^{-5}) of the $C_F C_A^2$ term is validated by the strongly ordered limit calculation.
- The $C_F C_A^2 \epsilon^{-5}$ term is canceled upon summing the RRR, RRV, and VVR contributions.
- The $C_F^2 C_A$ term agrees with the nonabelian exponentiation theorem.
- Some diagrams (such as the vacuum polarization diagrams) are checked through direct calculations.

- We analytically calculate the RRV and VVR contribution to the thrust soft function.
- The application of our method to the calculation of the RRR contribution is straightforward. This is the only missing piece of the complete $N^3\text{LO}$ thrust soft function, which is the key ingredient for the $N^3\text{LL}'$ resummation of the thrust observable in the dijet configuration.
- Our results can be used for the 0-jettiness in Drell-Yan/ ggH process as well as the 1-jettiness observable in DIS through analytic continuation. The results are also indispensable components to fulfill the $N^3\text{LO}$ calculation using the N -jettiness subtraction scheme.
- The calculation demonstrates the feasibility of our reduction method to future jet and substructure precision calculations.

The End

Thanks for your attention !



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