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High-D Consortium Meeting



Avalanche multiplication in a SiPM



When a photon hits a pixel, the generated charge carriers (e-h pairs) trigger an avalanche multiplication in the p-n junction by impact ionization.



- Gain >10⁵ is reached applying a reverse bias voltage above the breakdown level (V_{bd})
- I_{SIPM} increase when increasing applied V;
- I_{siPM} ranges from nA to mA (6 orders of magnitude).



- Higher temperature \rightarrow shorter mean free path of the charge carriers \rightarrow the critical E field necessary to keep a the avalanche increases, therefore V_{bd} increases as well.
- Photo-current $(I_{photo} = I_{SiPM} I_{dark})$ at constant bias voltage, V_{bias} , and constant photon rate, decreases with temperature:

$$I_{photo} \propto PDE(T) \cdot Gain(T)$$

 Explained, among other effects, by the temperature dependence of breakdown voltage, V_{bd}:

$$Gain \propto \frac{1}{q_0} C_{pix} (V_{bias} - V_{bd}(T))$$





- To **detect charged particles** the **SiPM is coupled to a scintillator** (plastic or inorganic). The minimum signal depends on the application: either single photon or minimum ionizing energy from a charged particle.
- **SiPMs operating on harsh radiation environment** or high ambient light show **high dark count rates**. The single photon resolution is not possible in this case.



MIP response before (black) and after (blue) irradiation:





- A ~40% reduction in the MIP response in a plastic scintillator with SiPM irradiated to ϕ_{eq} =10¹³ cm⁻² and operated at 2 V above breakdown (2 OV).
- Is unclear if these results are consequence of radiation damage in the SiPM or of the self-heating effect .





Dark current increase \rightarrow Self- heating effect

- What is self-heating effect?
 - Increase in dark current, up to 6 order of magnitude, leads to large power dissipation (heat) and therefore produce an increase on SiPM temperature.
- Why is this effect important?
 - If the heat is not cooled down fast enough, the increase on temperature changes the SiPM performance.
- How do we want to perform the studies?
 - Operate a non-irradiated SiPM, under LED illumination, to produce the same power (P = V_{bias}*I_{SiPM}) as expected for an irradiated SiPM.



- P~ 50 mW induced by I_{dark} (Irrad. at φ = 1e13 cm⁻² at V_{ex} = 2
 V, V_{bd} = 36.7 V @ -30 °C)
- P~ 50 mW induced by high I_{LED} (non-irrad. I_{LED}~0.5 mA at V_{ex} = 10 V, V_{hd} = 27.5 V @ 25 °C)

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- Determine ΔT_{SIPM} from an induced ΔI_{SIPM} with a predefined cycle:
 - I_{SIPM} increased either by increasing light intensity at constant V_{bias} or by changing V_{bias} under constant light illumination.
 - 2nd interval (B) is the comparison stage between the cycles:
 - ▶ Regardless prior conditions → Same power induced applying same V_{bias} and I_{LED}





Measurement setup with a SiPM

• SiPM KETEK non-irradiated (MP15V09 D2.8)

• d_{si}= 700 µm

- V_{bd} = 27.6 V @25°C, C_{pix} = 18 fF, τ = 14 ns
- Pixel size = 15 μm, 27000 pixels
- SiPM glued on alumina (Al₂O₃) substrate:
 - d_{Al2O3}= 600 μm
- Cooling system: temperature-controlled chuck
- POM (1.5 and 3.0 mm) between the alumina/PCB and cold chuck to emulate degraded thermal contact.
- 3 T sensors (PT-100): at 3.1 mm (T_{sensor1}) and 7.6 mm (T_{sensor2}) from the SiPM center, T_{sensor3} on the chuck.
- Illumination: LED (470 nm)



Alumina

POM Temperature controlled chuck Tsensor3



Ketek and MPPCs (HPK)

• Samples used:

	S 6	MPPC S14160-9766		
	Ketek	НРК		
# pixels	27367	8480		
Pixel size [µm]	15	15		
Active area [mm ²]	6.2	1.4 x 1.4		
Substrate	Alumina	PCB		
V _{bd} (@ 25°C)	27.6 V	38.2 V		
dV _{bd} /dT [mV/K]	22.4	33.3		
S _{photo}	0.46% (10.4 OV)	0.58% (7.8 OV)		





Method for self-heating studies with I_{photo}

- Express the temperature (T) dependence of I_{photo} as: $\frac{dI_{photo}}{dT} = \frac{dI_{photo}}{dV} \cdot \frac{dV_{bd}}{dT}$
- A relative change in I_{photo} is related to a change in T by the **sensitivity**: $S_{photo}(V_{bias}, T_{chuck}) = \frac{1}{I_{photo}} \cdot \frac{dI_{photo}}{dV} \cdot \frac{dV_{bd}}{dT} = \frac{1}{K}$
 - Calibration data is measured at known and stable T_{chuck}:

• Calibration data at several LED currents leads to the same sensitivity curve:



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- Instead of the usual I(V) measurements, this **method require to measure current vs time, I(t).**
- Determine ΔT_{SIPM} from an induced **power** (I and V steps):
- Example of constant illumination and V step from below to 10 V above V_{bd} with the SiPM on top of:



I_{SIPM} normalized to the first data point after the switch



• SiPM with good thermal contact $\rightarrow \tau \sim 1$ s

• SiPM with bad thermal contact $\rightarrow \tau \sim 10$ s

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ΔT_{SIPM} for I and V steps: good and degraded thermal contact



Same steady state current for I and V steps in the interval of interest.



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- Good thermal contact (SiPM+Alumina on top of the chuck surface):
 - Increase up to 0.5 K
- Degraded thermal contact (POM layers between the chuck surface):
 - SiPM+Alumina ~5 K for thicker POM layer.
 - For the SiPM+PCB ~15 K for thicker POM layer.
- $Ketek(Al_2O_3)$ on chuck 14 $Ketek(Al_2O_3) POM(1.5mm)$ Ketek(Al₂O₃) POM(3.0mm) 12 HPK(PCB) on chuck HPK(PCB) POM(1.5mm) 10 ΔΤ_{SiPM} [K] HPK(PCB) POM(3.0mm) 8 6 4 2 0 20 40 60 80 100 120 Power [mW] **Expected P for**

irradiated SiPM

- For a SiPM soldered on a PCB:
 - 50 mW \rightarrow T_{SIPM}~ 5 K -



- Good thermal contact (SiPM+Alumina on top of the chuck surface):
 - Shift on V_{bd} up to 15 mV
- SiPM+PCB on top of the chuck surface:
 - Shift on V_{bd} up to 300 mV
- Degraded thermal contact (SiPM+Alumina+POM layers between the chuck surface):
 - Shift on V_{bd} up to 120 mV
- Degraded thermal contact (SiPM+PCB+ POM layers between the chuck surface):
 - Shift on V_{bd} up to 500 mV





- Developed method to determine the heating of SiPMs from its current, as a function of:
 - Induced power, thermal contact and SiPM packages.
- The method has been used to determine the temperature increase of a SiPM with P ~ 50 mW, expected for instance in SiPM (MPPC HPK) irradiated to ϕ_{eq} ~10¹³ cm⁻² operated ~ 2V (OV)
- Heating causes a decrease in I_{photo} (increase in I_{dark}) and a shift on V_{bd} :
 - For good thermal contact: $\Delta T_{siPM} \sim 0.5$ K, $\Delta V_{bd} = 15$ mV
 - For degraded thermal contact (SiPM mounted on PCB): $\Delta T_{siPM} \sim 5 \text{ K}$, $\Delta V_{bd} = 180 \text{ mV}$. However, this shift on V_{bd} does not explain the significant MIP response reduction observed in previous studies.
 - Next steps:
 - Apply the method for irradiated samples.
 - Compare the results with thermal simulations.



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Thanks for your attention! Let's go for lunch!!!

Backup slides



- If the shift of 40 mV is not compensated, operating ~ U_{ex} = 2 V \rightarrow reduction of gain by 2 % + • reduction of PDE by 2 %
- Reduction of signal about 4 % •
- Increasing U_{bias} is a possible solution, **but**:





What is a SiPM

- <u>Single-Photon Avalanche Diode (SPAD)</u> = photo-diode reverse biased, operating above the breakdown voltage level, $V_{bd} \rightarrow$ Geiger mode (avalanche multiplication) \rightarrow Gain > 10⁵
- <u>Silicon Photo-Multiplier (SiPM)</u> = array of SPADs connected in parallel. The single SPADs in a SiPM \rightarrow pixels.









Customised SiPM (HPK) designed for CMS



SiPM response to low light intensity



I_{SIPM} as a function of time for I_{LED} steps, using KETEK S3 sample. At 25 °C. Normalizing the time to the first data point after the switch. For the cases with the SiPM on direct contact with the chuck (A), with a 1.5 mm (B) and 3.0 mm thick (C) POM layer between the SiPM and the chuck.

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	$\Delta T(0,0)$	$\Delta T(0.14,0))$	$\langle \Delta T \rangle$	R_{th}	ΔW	$ au_h$	$ au_c$
	[K]	[K]	[K]	[K/W]	[J]	[s]	[s]
Si	0.18	0.086	0.15	0.44	4.8×10^{-4}	5.0×10^{-3}	1.1×10^{-3}
$Si + Al_2O_3$	0.60	0.39	0.51	1.46	7.6×10^{-3}	32×10^{-2}	8.5×10^{-3}
+ 1.3 mm PVC	10.2	9.9	10.1	28.7	6.9	20	5.4
+ 3.15 mm PVC	19.0	18.6	18.8	53.7	15.1	44	31

Table 2: Simulated temperature change of the SiPM multiplication region and estimated heating- and cooling- time constants for a power of Pow = 350 mW dissipated in the multiplication region of the SiPM. Given are the temperature change of the multiplication region at the SiPM center, $\Delta T(0, 0)$, at the periphery, $\Delta T(0.14 \text{ cm}, 0)$, and the mean $\langle \Delta T \rangle$. $R_{th} = \langle \Delta T \rangle / Pow$ is the thermal resistance. ΔW is the energy deposited in all materials, and $\tau_h = R_{th} \cdot \Delta W / \langle T \rangle$ an estimate of the heating-time constant, and τ_c an estimate of the cooling-time constant.



WL FOLIE 404 11 Heat conducting foil, double-sided adhesive (0.127 mm thick), K= 0,37 W/m*K



Cold chuck Setup Sketch





MPPC samples soldered on flexprint









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- As a reference: HGCAL is using FR4 (glass epoxy laminate material) for the PCB and they use 0.3 W/m*K as thermal conductivity, POM-C (Polyoxymethylene) has the same thermal conductivity.
- PCB is only 1.3mm thick. Including the polyimide isolation layer (50µm thick) between PCB and heat sink (cooper), total thickness 1.6mm.





ΔT_{SIPM} for I_{LED} steps good thermal contact



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