



Elettra Sincrotrone Trieste

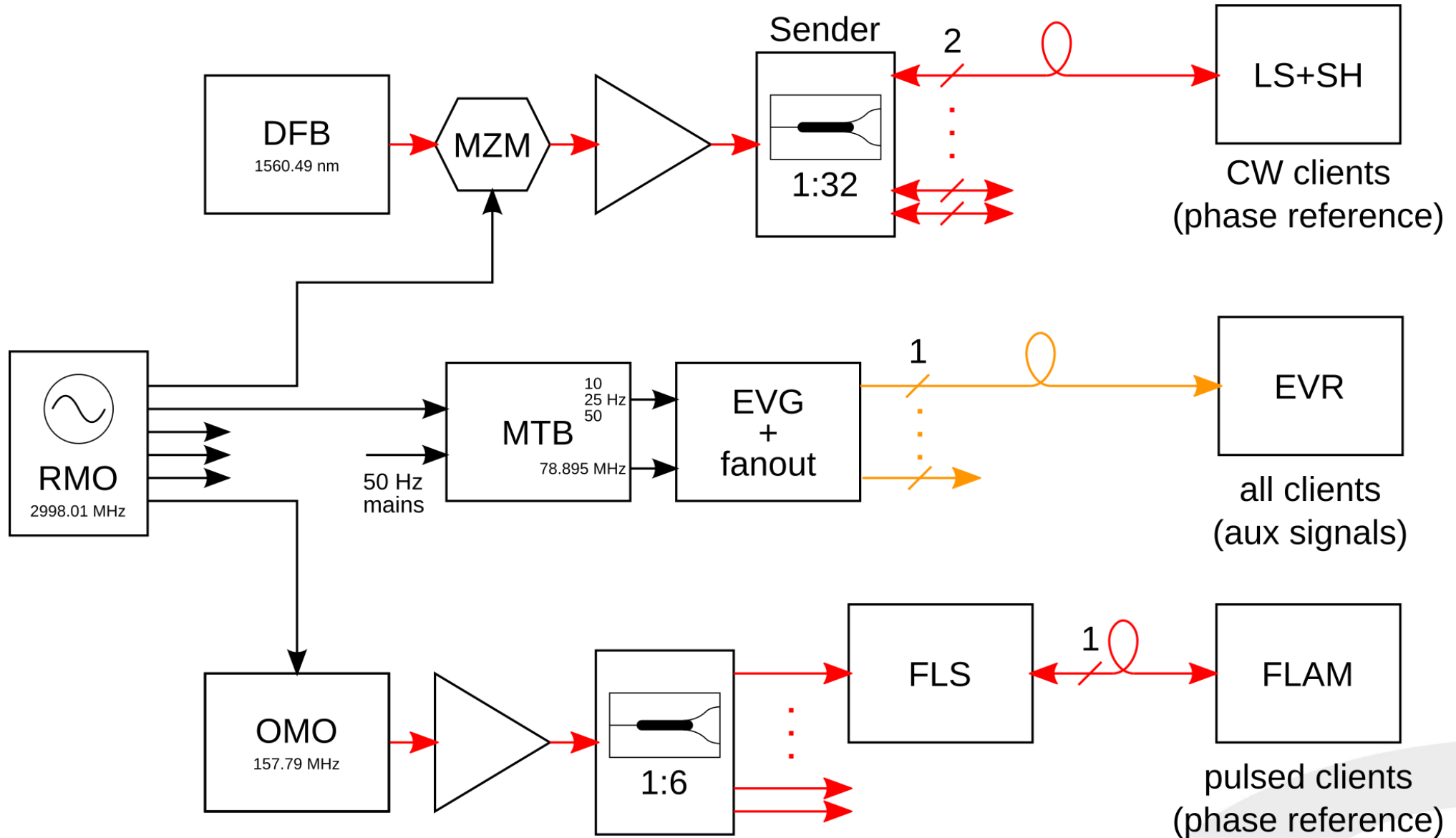
The FERMI Optical Timing system: operating experience and latest developments

F. Rossi, M. Predonzani, M. Ferianis

- system overview
- operating experience
- current and future activities

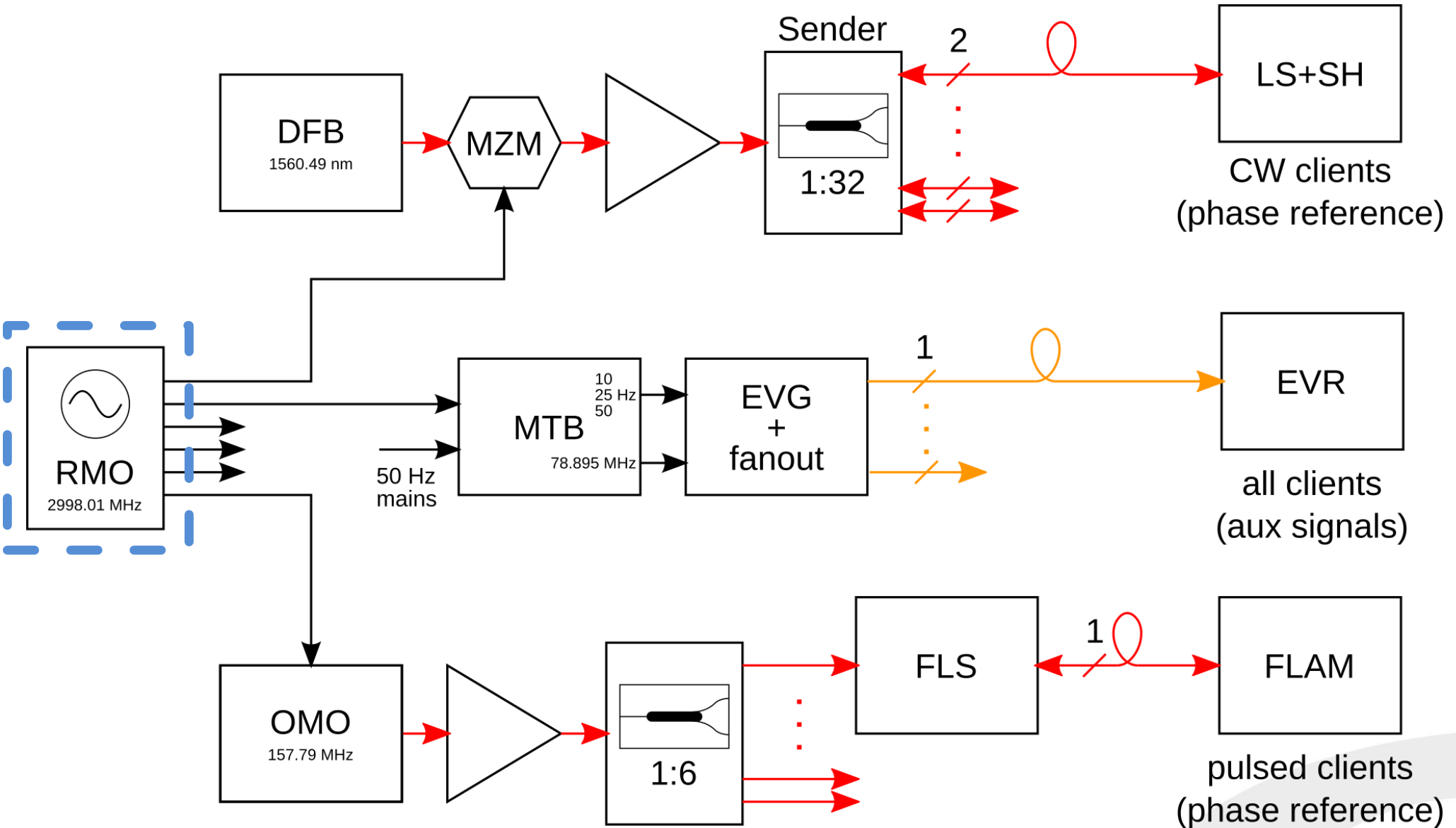


System overview



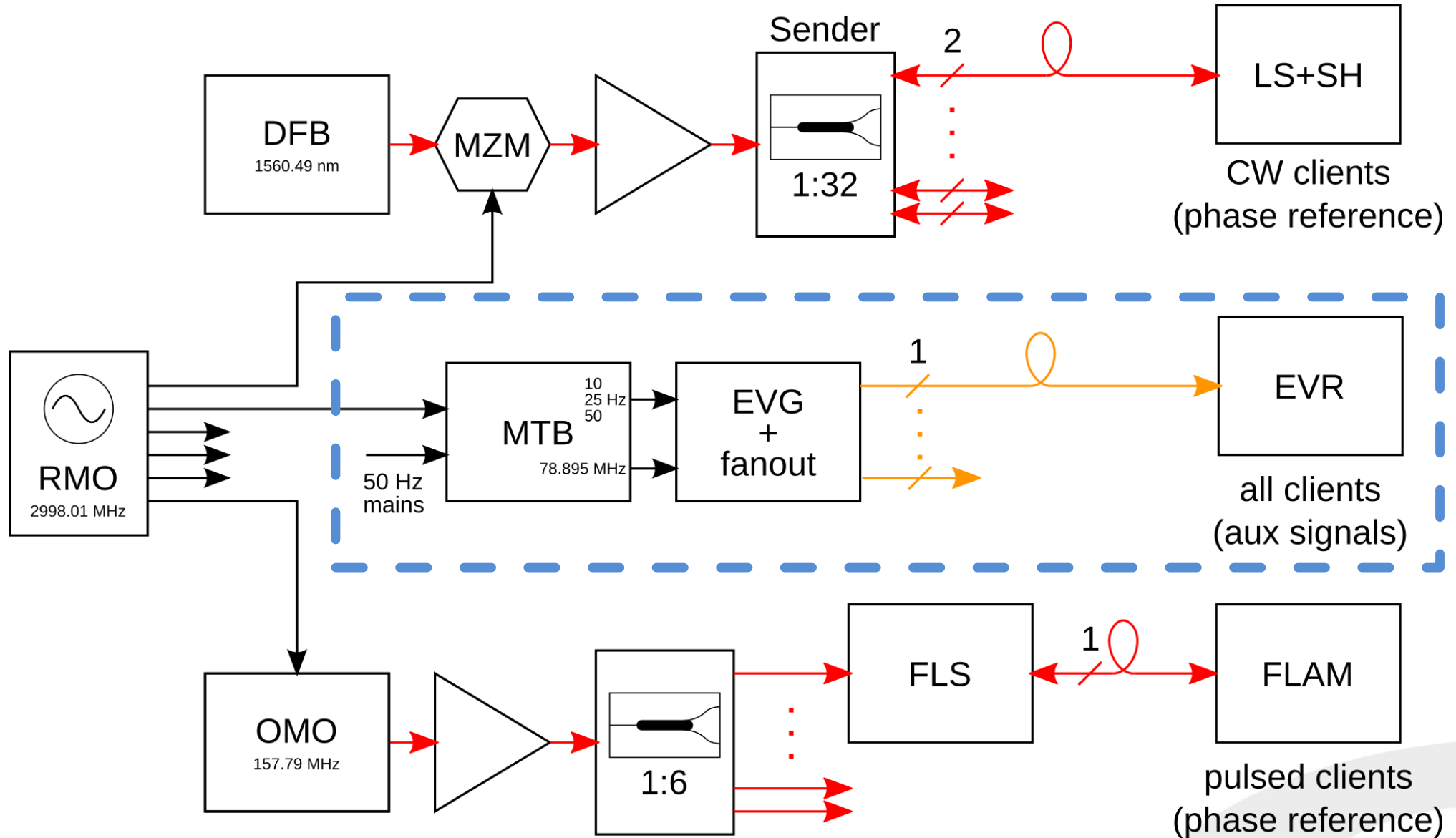


System overview



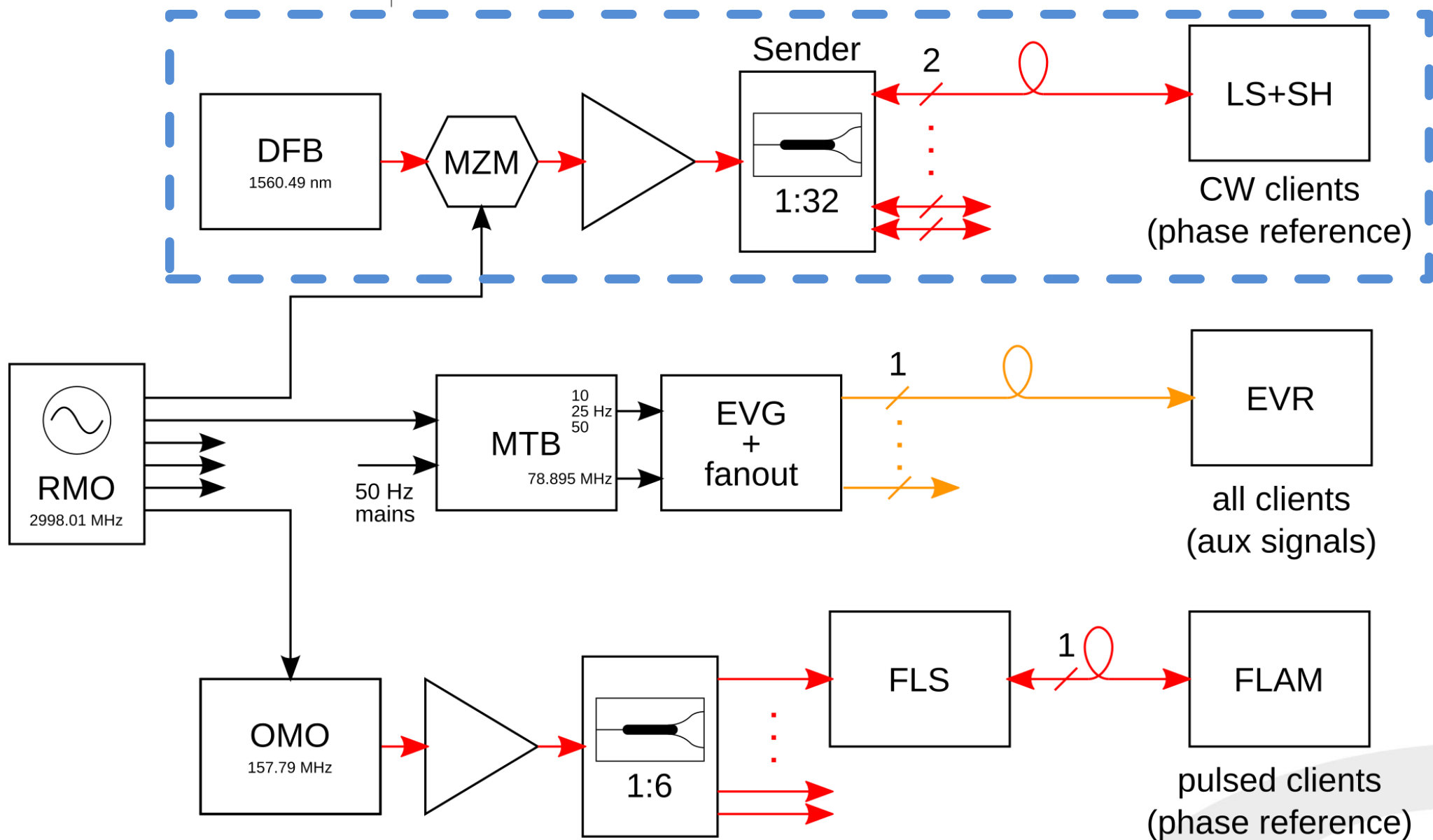


System overview



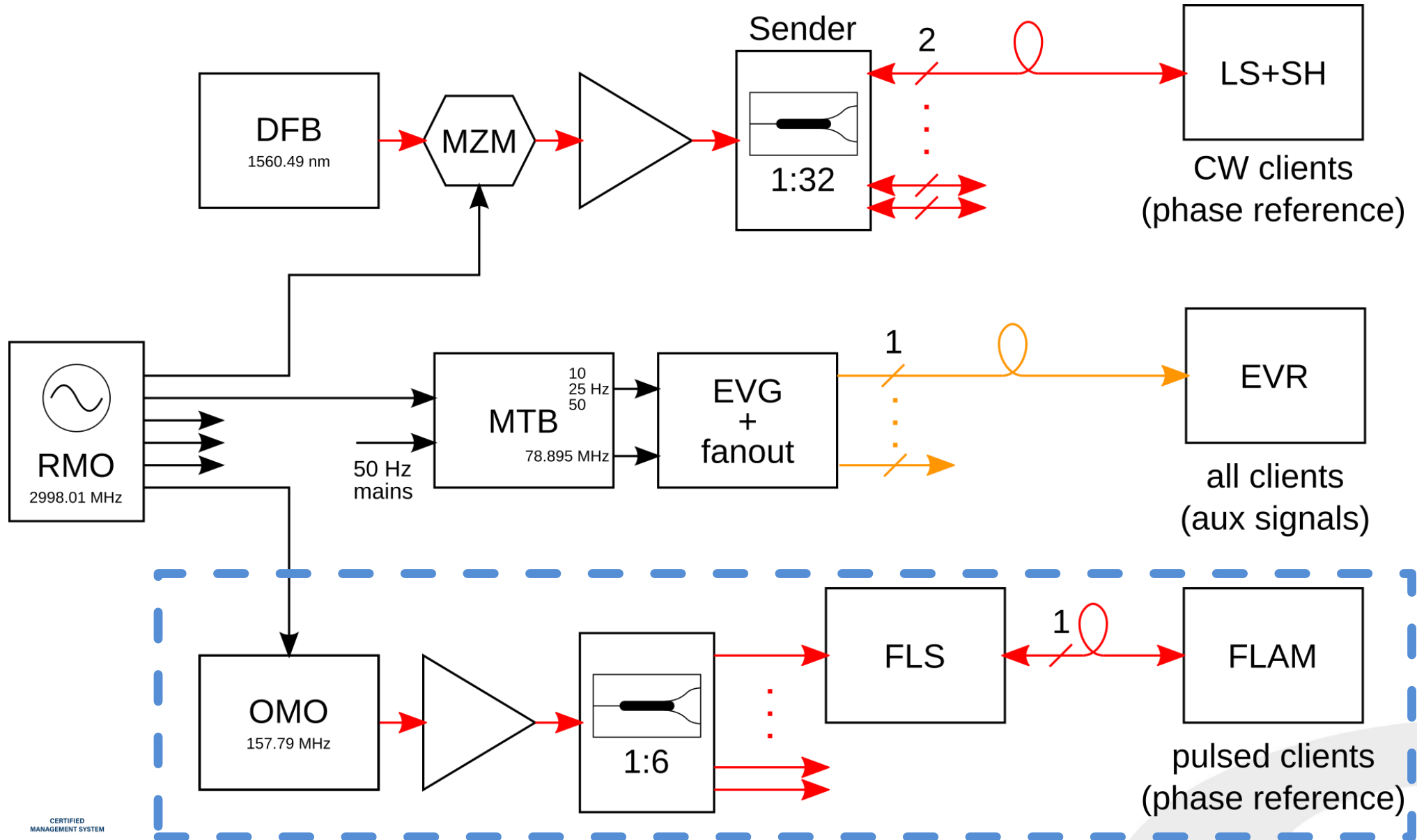


System overview





System overview



- **how critical is the start-up of the system?**
 - it requires at least a day starting from scratch (to reach an effective stabilization)
 - a procedure based on checklist is used to verify the system
 - the pulsed subsystem is more tricky due to the care needed to find and optimize (not deterministic process) the OMO mode-locking
 - we prefer to leave the laser always on (even during machine shutdown periods)
 - the CW subsystem is a turnkey solution
- **how much effort is needed to operate the system?**
 - up to now the fault rate has been quite low (a few events per year)
 - it is important to provide prompt support to control room
 - data analysis is quite important to find the source of a problem
 - system optimization as needed

■ which is our fault statistics?

Classification of the faults based on the impact on machine operations:

- **negligible** – all kind of blocking situations that can be solved quickly by generic operators (e.g. relocks, power cycling, etc)
- **medium** – all the faults that require some servicing by specialized people
- **severe** – servicing + long recovery time (in particular, the faults affecting the centre of the star topology)

On the basis of our experience, the most common faults belong to the first category.

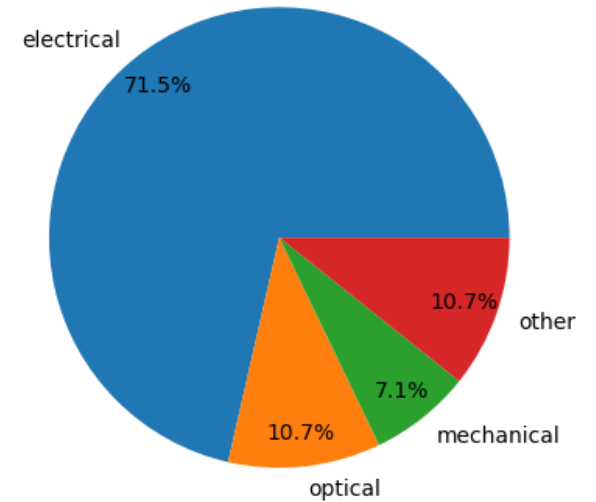
No faults due to radiations effects in the machine tunnels have been observed.

In 2009, one of the open issues was whether optical technologies for timing applications were reliable for 24/7 operations. An over ten-year experience confirms they are.

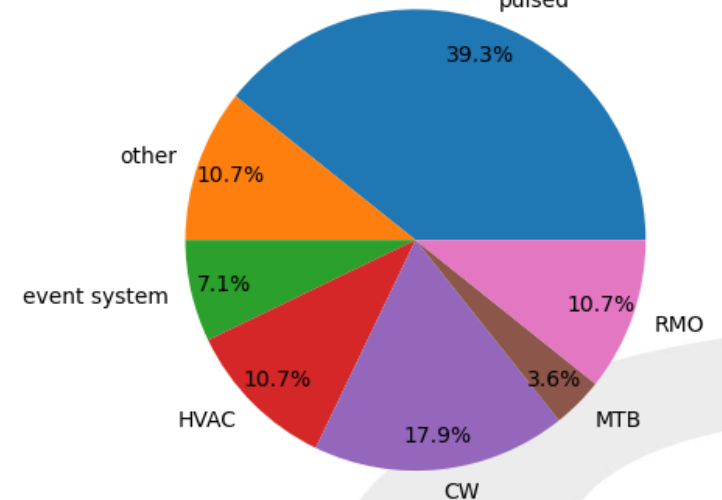
fault statistics requiring specialized service

Edit	Delete	RUN	Date of fault	Subsystem	Technology	Text
			50 Fri - 2023 Oct 27	pulsed	electrical	RE306 chiller found off, replaced with spare part
			50 Mon - 2023 Sep 11	other	electrical	electrical power outage, complete switch-off full system
			49 Mon - 2023 Jul 03	event system	electrical	replaced EVR module K11
			48 Mon - 2023 Mar 20	other	electrical	dead thermograph LT KG05.01
			48 Mon - 2023 Mar 20	event system	optical	replace two SFP modules (one in the central fanout)
			45 Wed - 2022 Jun 08	HVAC	mechanical	problems with the HVAC timing room due to 3-state valve
			44 Tue - 2021 May 04	BAM	mechanical	dead delay line BAM frontend
			40 Sun - 2020 Dec 06	HVAC	electrical	unstability of HVAC timing room
			36 Thu - 2019 Jun 13	pulsed	electrical	problems with power supply chiller RE306, replaced
			35 Thu - 2019 Mar 28	CW	electrical	fixed RF power supplies of K3 and K6 link stabilizers
			33 Mon - 2018 Apr 30	pulsed	mechanical	problem with pump of chiller RE306, replaced
			31 Fri - 2017 Nov 03	pulsed	optical	dead pump diode LFC SL
			31 Sun - 2017 Oct 29	pulsed	other	many unlock events OMO due to wrong configuration of the software
			31 Mon - 2017 Oct 23	other	electrical	replaced thermograph L4
			17 Sat - 2017 Sep 30	pulsed	electrical	fault power supply AC1550
			31 Thu - 2017 Sep 28	CW	electrical	fixed power supply link stabilizer K9
			29 Mon - 2017 Jan 23	pulsed	optical	burnt connector LFC amplifier EOS-link
			25 Tue - 2015 Nov 03	pulsed	other	recentering of FLS motor which reached end-of-travel
			17 Fri - 2013 Sep 13	CW	electrical	replaces synchhead on K9
			16 Tue - 2013 Jul 16	pulsed	electrical	power supply LFC PIL
			15 Thu - 2013 Mar 14	CW	electrical	replaced synchhead on K8 (RF amplifier)
			14 Sat - 2012 Dec 08	pulsed	other	OMO lost modeLocking
			13 Wed - 2012 Oct 17	pulsed	electrical	power supply LFC BC1
			12 Fri - 2012 Jul 27	HVAC	electrical	problems with temperature sensor used by the loop
			12 Fri - 2012 Jul 27	MTB	electrical	unstable 78 MHz reference
			12 Fri - 2012 Jun 15	RMO	electrical	unstable RMO due to jumps in the frequency (OCXOs)
			10 Fri - 2012 Mar 16	RMO	electrical	unstable RMO, no lockable to Rb
			10 Tue - 2012 Feb 07	CW	electrical	replaced link stabilizer K3
			7 Wed - 2011 May 25	RMO	electrical	replaced because of failure of internal multiplier

faults by technology

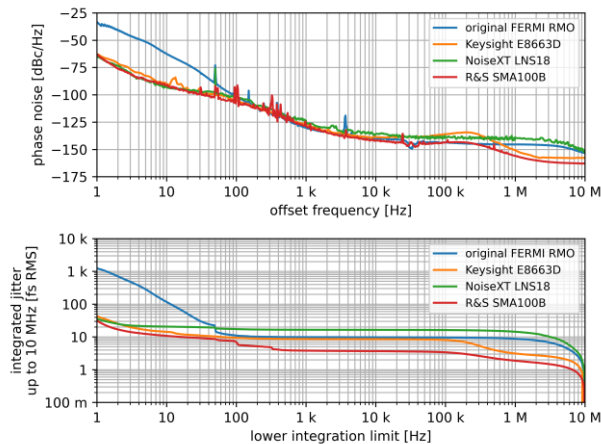


faults by subsystem



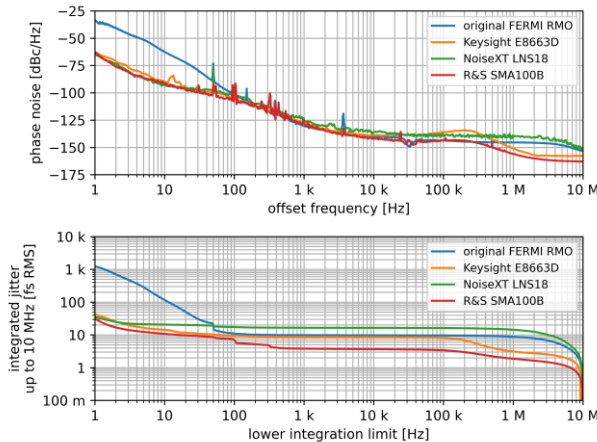
- which is our strategy to maximize the up-time?
 - an on-call 24/7 service is mandatory
 - a close integration of the hardware in the machine control system
 - remote control and system automation
 - data logging (important for failure analysis)
 - continuous monitoring of the system parameters (key to implement an alarm system)
 - to predict instabilities or future problems by automatic analysis of system parameters
 - to exploit the periodic slots scheduled for machine maintenance for the optimization/tuning of the system (if needed)
 - the OMO has a redundant pump diode, it can be activated on demand without removing the laser from the system (never used this possibility!)
 - to use as much as possible standard products

- which improvements were a real turning point?
 - Upgrade of our custom RMO to a commercial product (SMA100B)



- better phase noise
- reliability: no more faults related to RMO

- which improvements were a real turning point?
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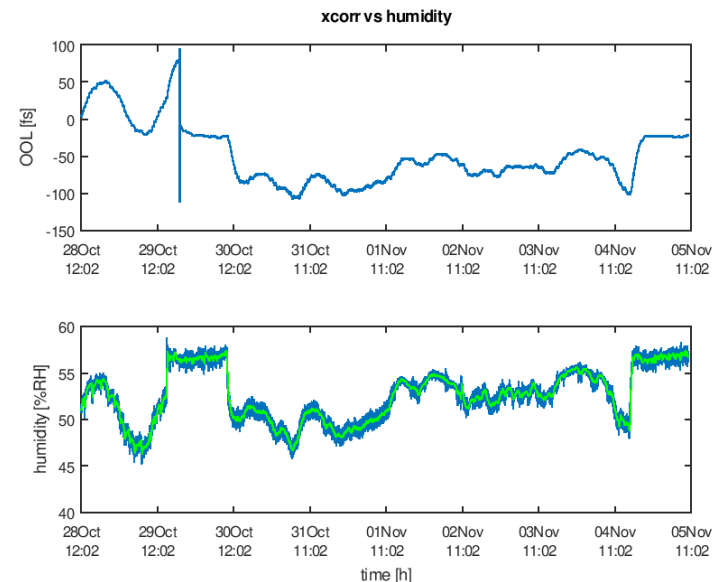


- better phase noise
- reliability: no more faults related to RMO

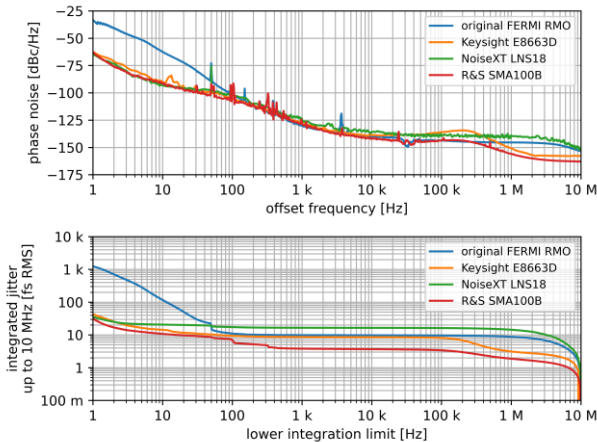
- Installation of an additional temporary machine to achieve a better control of the humidity in the timing room

Hopefully moving to a new integrated HVAC in 2024

- 0.25 degC p2p over 24 hours
- 2%RH p2p over 24 hours



- which improvements were a real turning point?
 - Upgrade of our custom RMO to a commercial product (SMA100B)

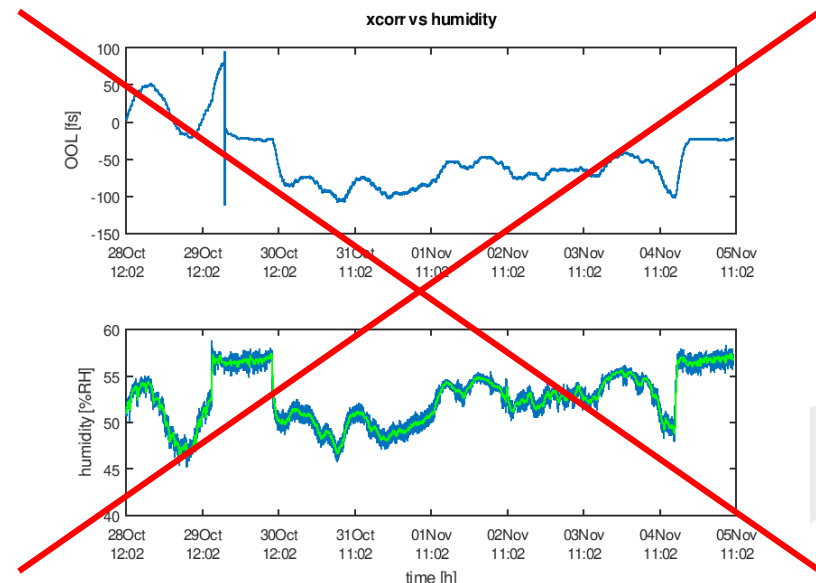


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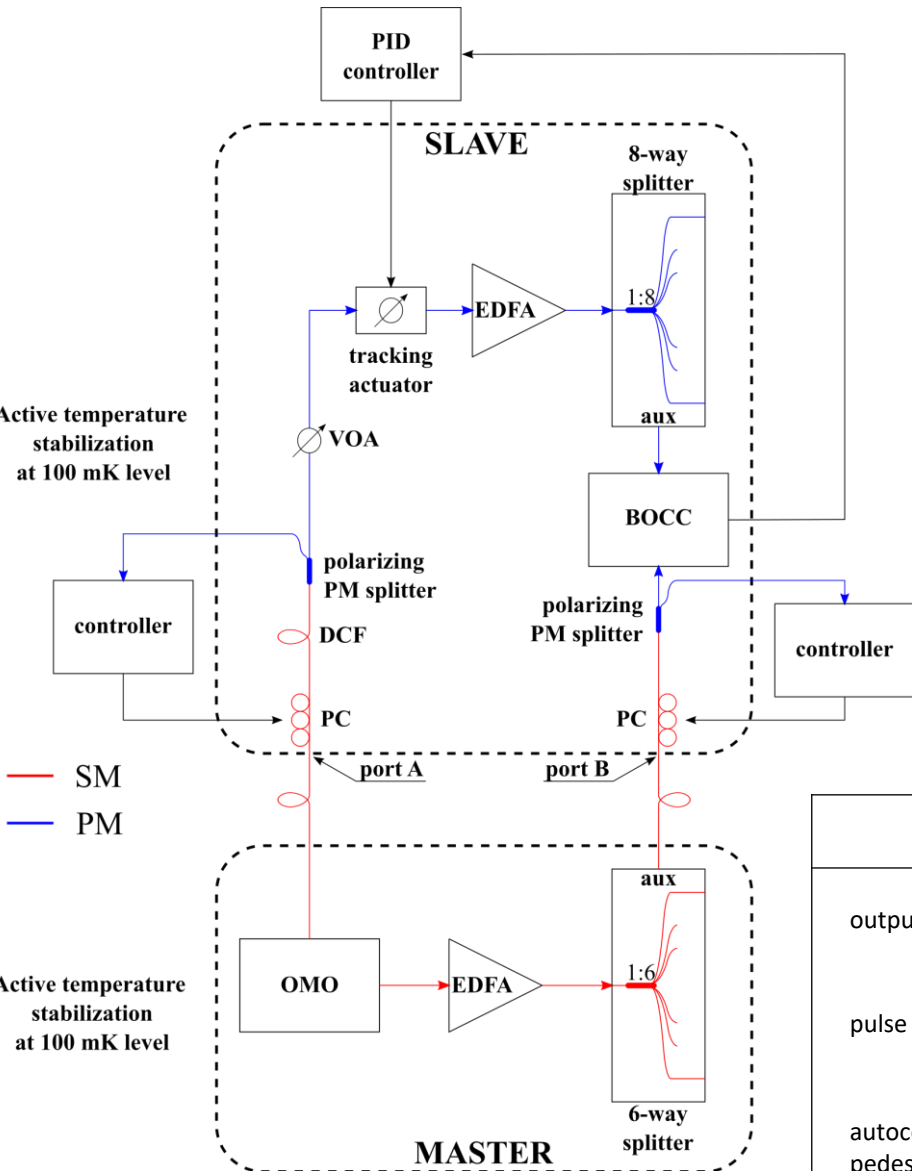
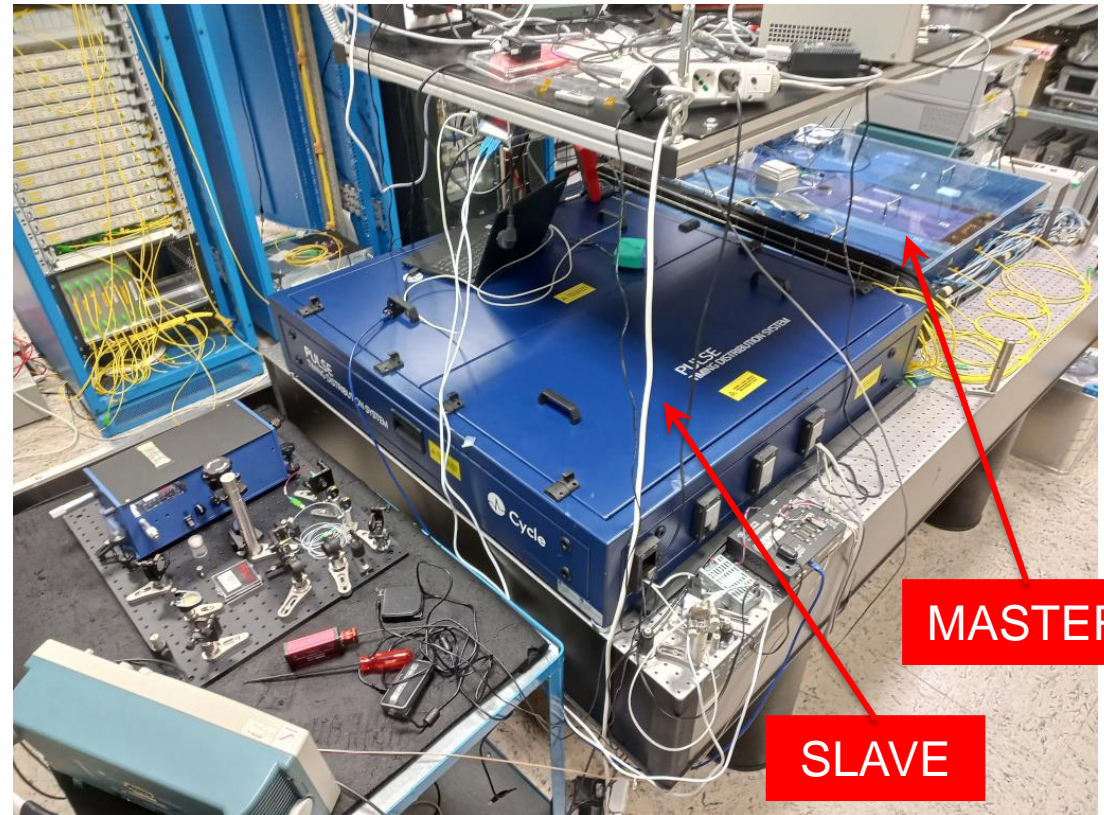
- 0.25 degC p2p over 24 hours
- 2%RH p2p over 24 hours



- which are the drawbacks of our system?
 - the pulsed system is not based on a polarization maintaining architecture
 - long-term stability < 1 fs RMS is hard to achieve
 - polarization drifts out of the links
 - this poses a limit for future FEL requirements with shorter pulses
 - how much is possible to improve the current architecture by squeezing the best performance out of it?
 - the OMO doesn't have a unique mode-locking condition
 - the recovery time in case of failure is not deterministic
 - the phase noise profile depends on the random combination of four waveplates
 - the CW distribution is “memory-less” due to the missing active stabilization of the link (in case of a power cycle the phase of the RF clients must be realigned, a software workaround is available)



Current and future activities



the most relevant specifications

output ports	8	amplitude noise	< 0.1 % RMS [10 Hz - 10 MHz]
pulse duration	< 200 fs FWHM	additive jitter	< 10 fs RMS [10 Hz - 10 MHz]
autocorrelation pedestal height	< 0.15%	splitter stability	< 25 fs p2p over 24-hour interval
average power	> 45 mW	tracker stability	< 25 fs p2p over 24-hour interval

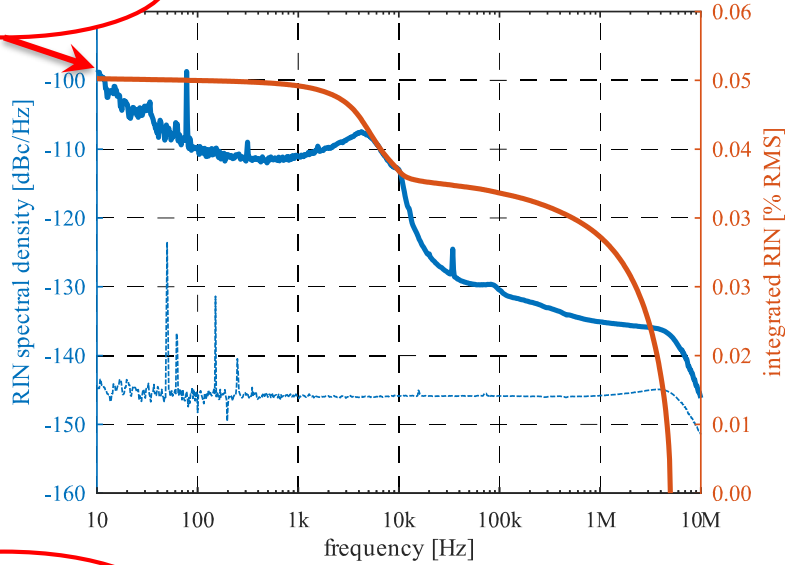


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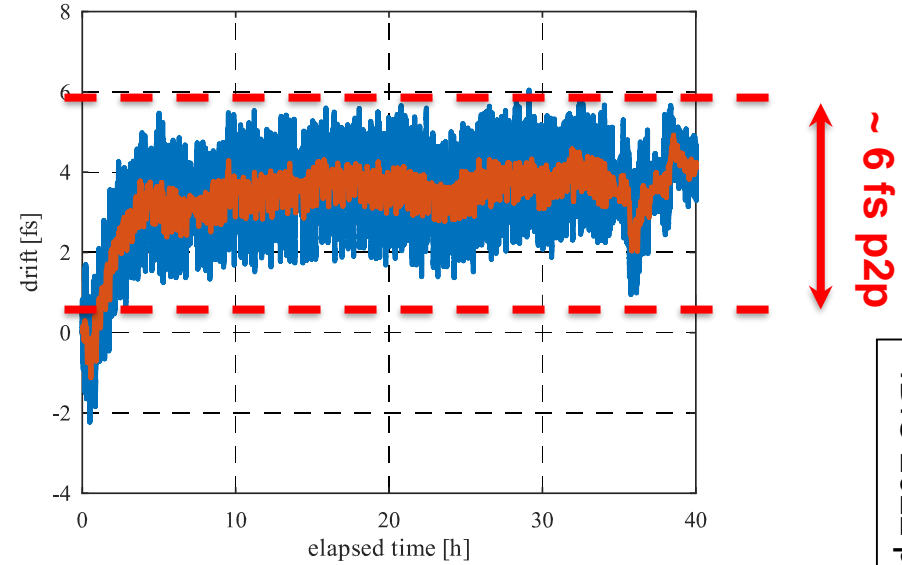
Current and future activities

0.052 % RMS

amplitude noise

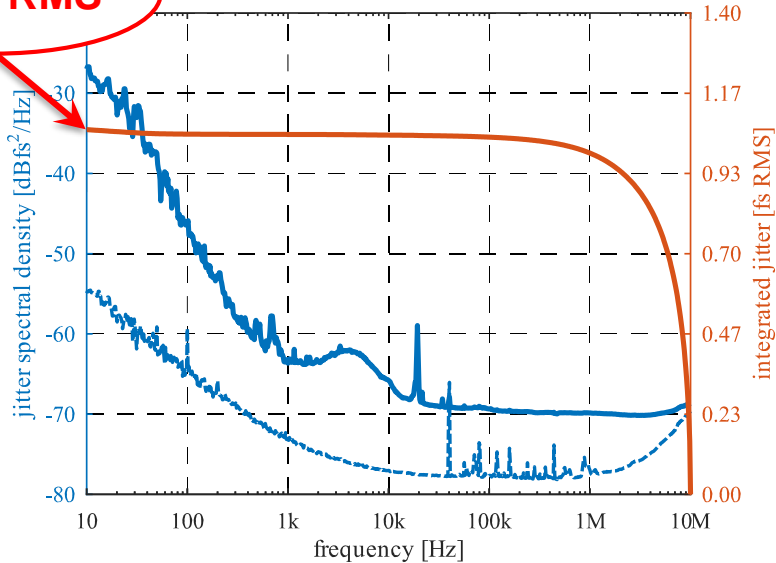


splitter stability

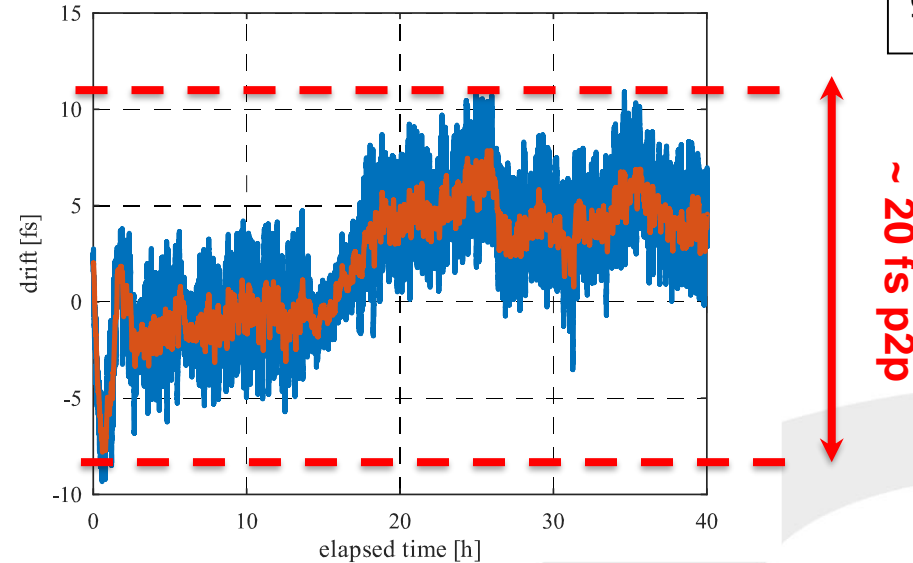


1.1 fs RMS

additive jitter

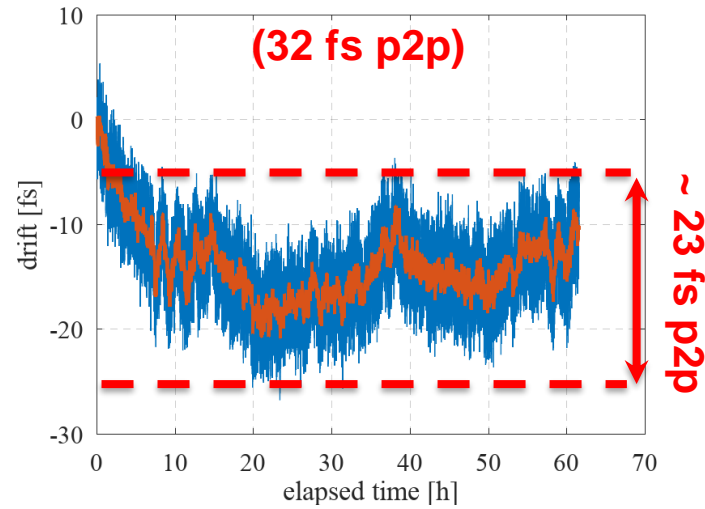
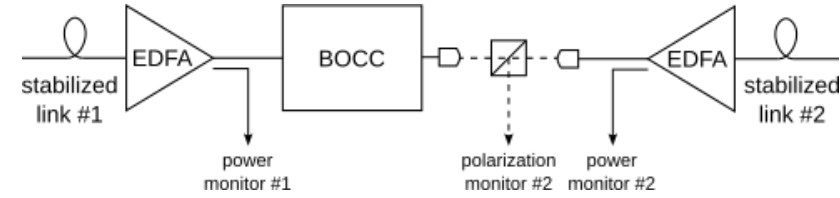


tracker stability



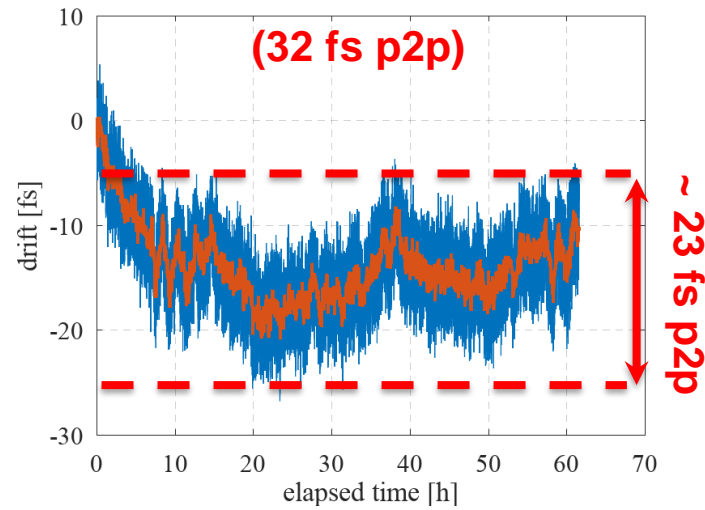
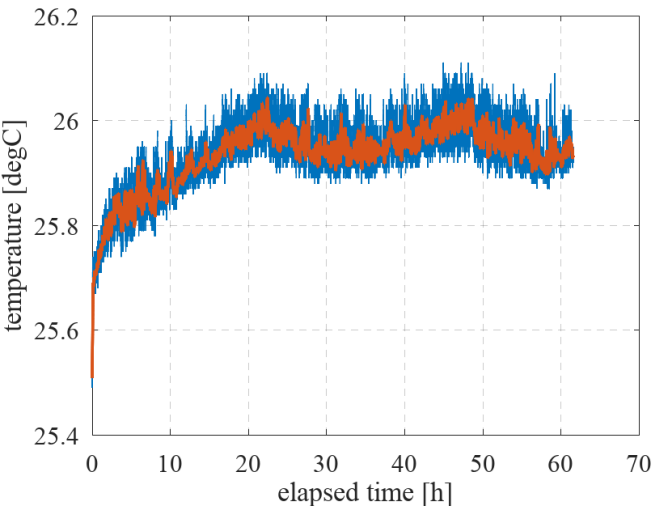
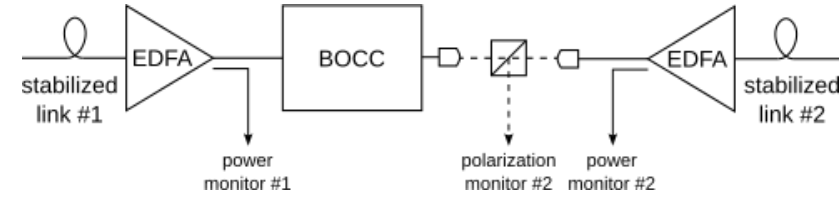
Current and future activities

OOL drift measurement (preliminary)



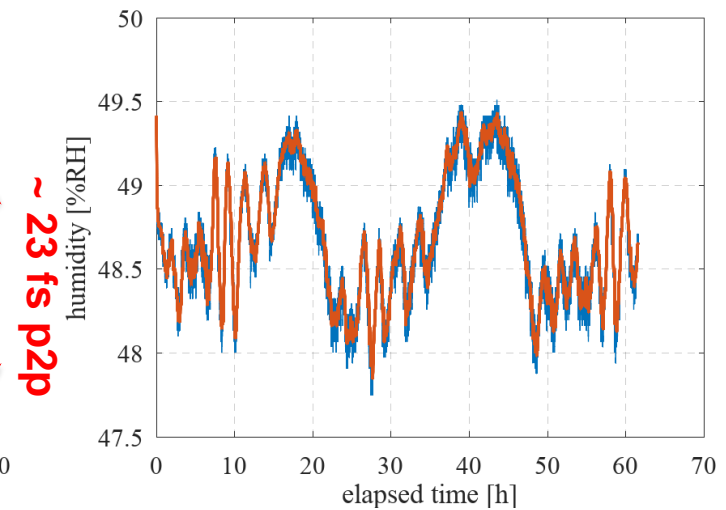
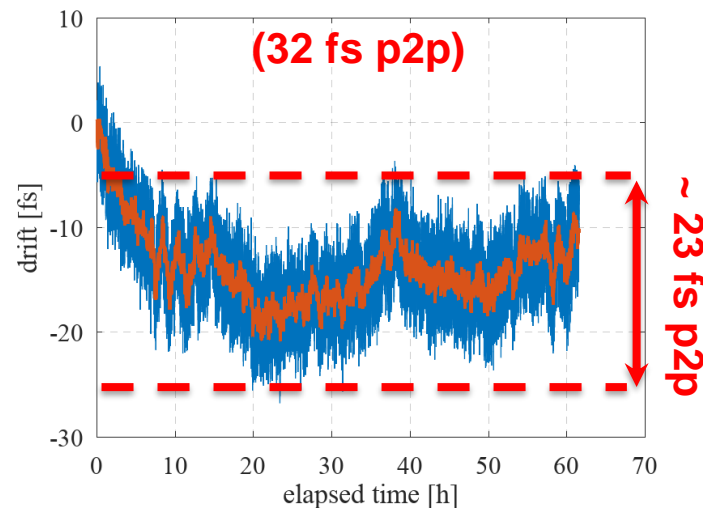
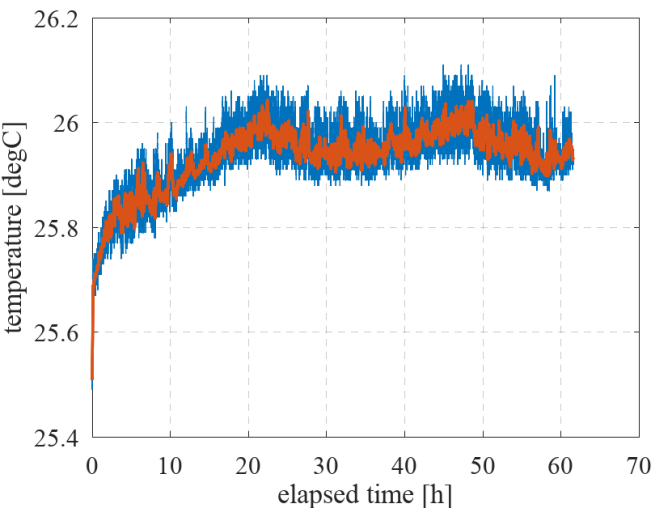
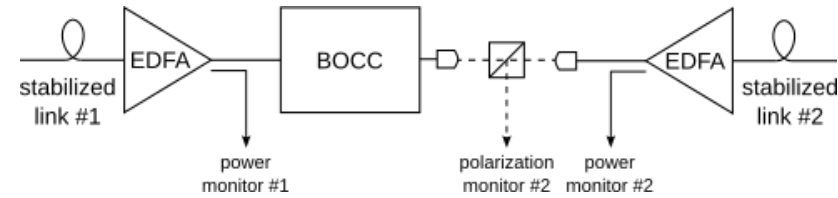
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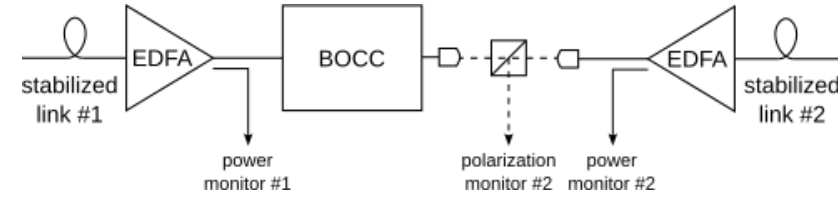


Current and future activities

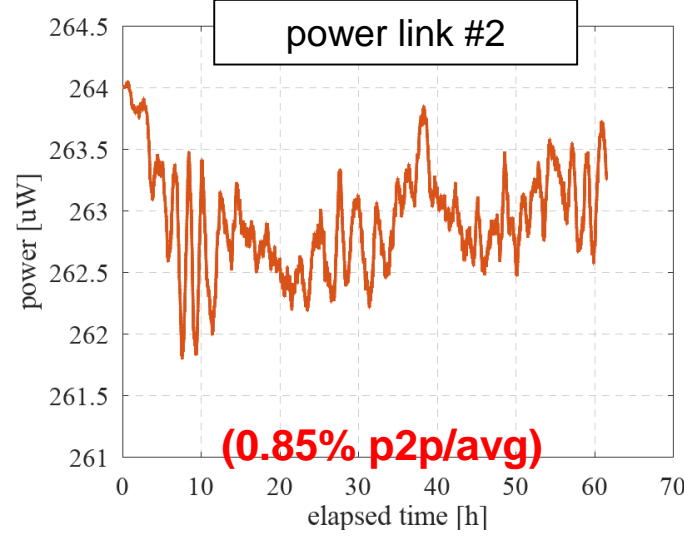
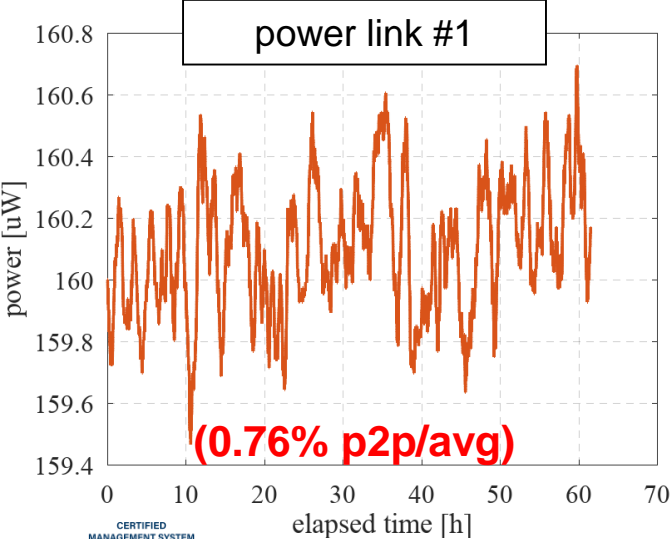
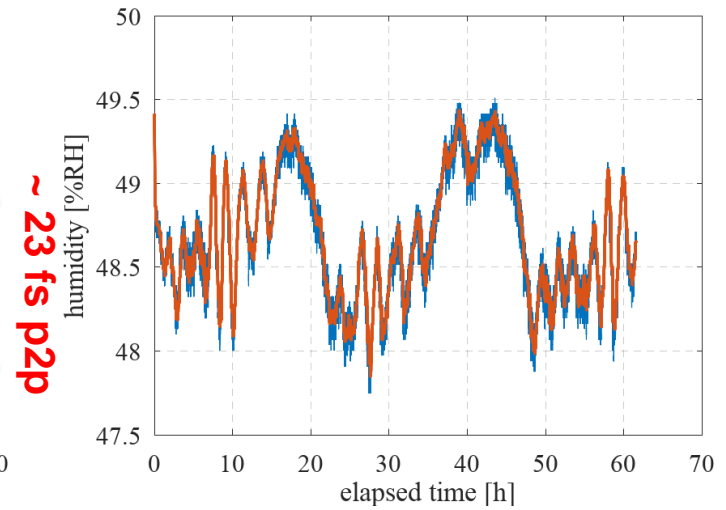
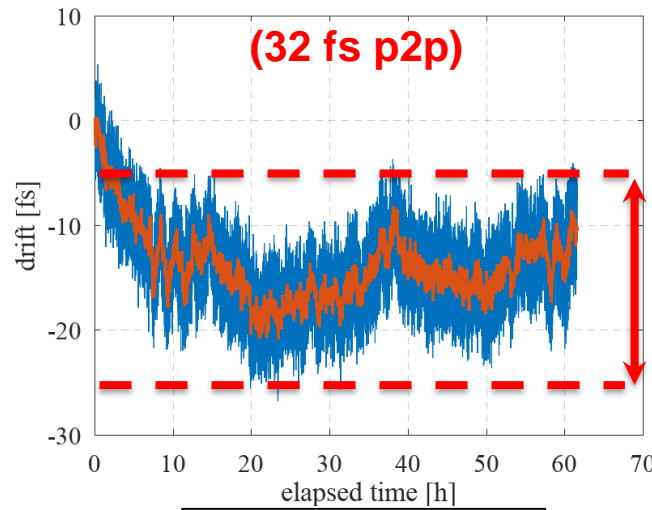
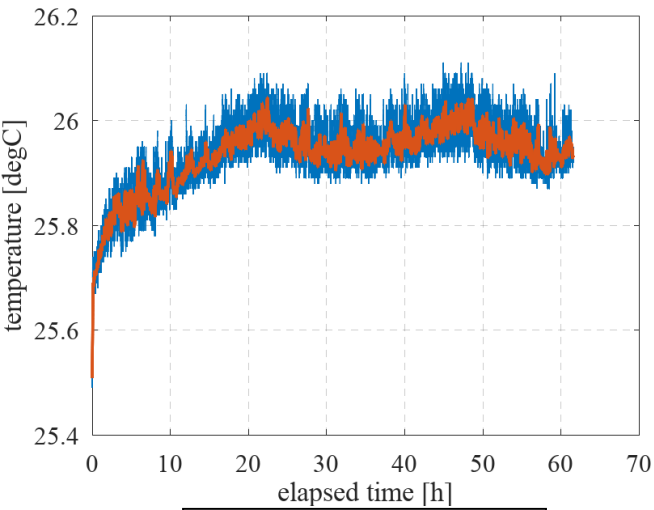
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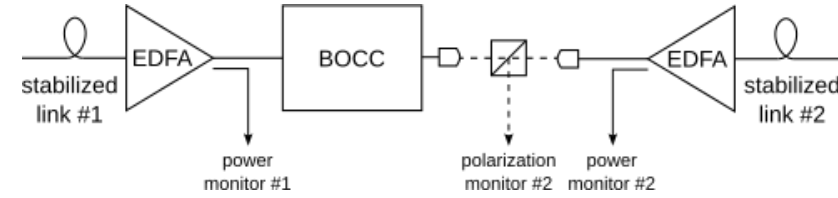
Current and future activities



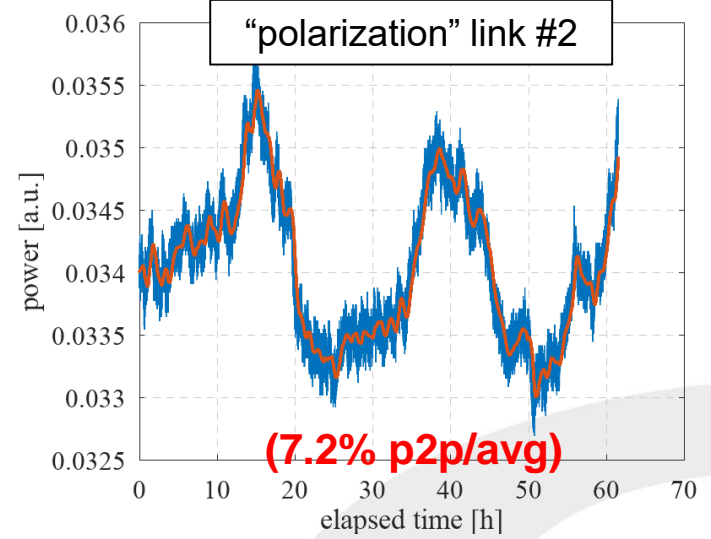
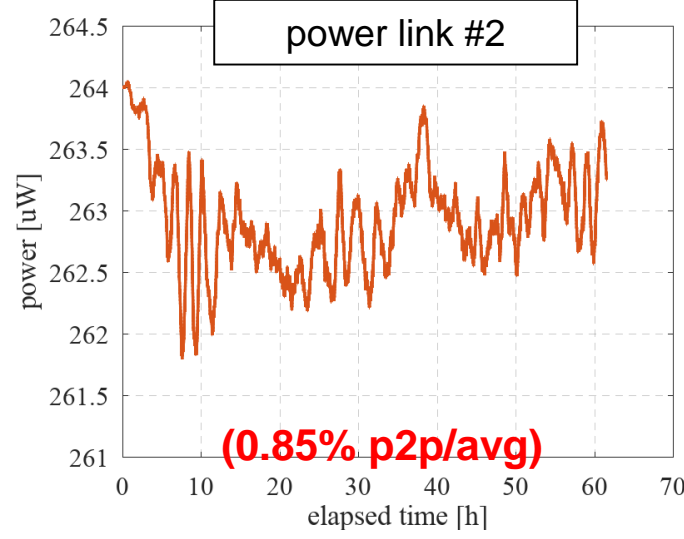
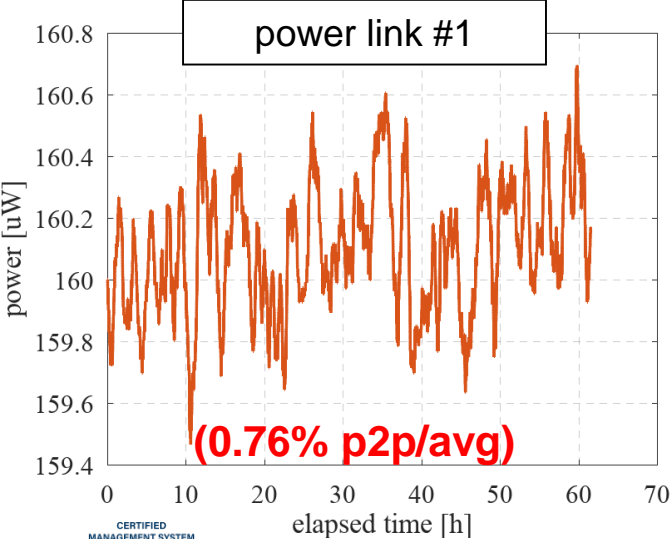
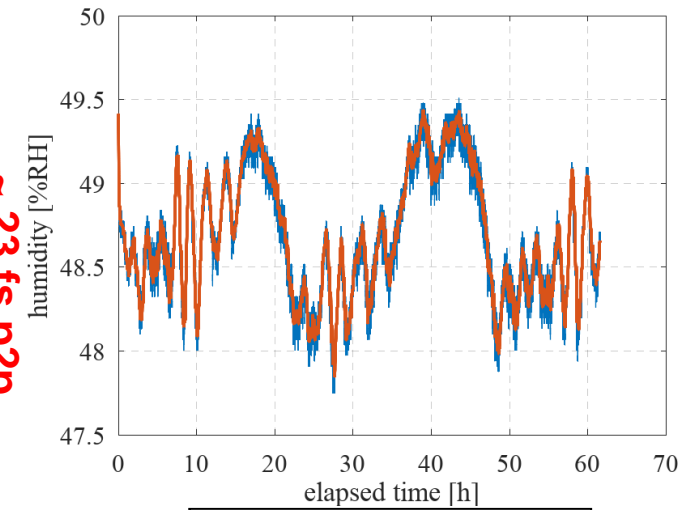
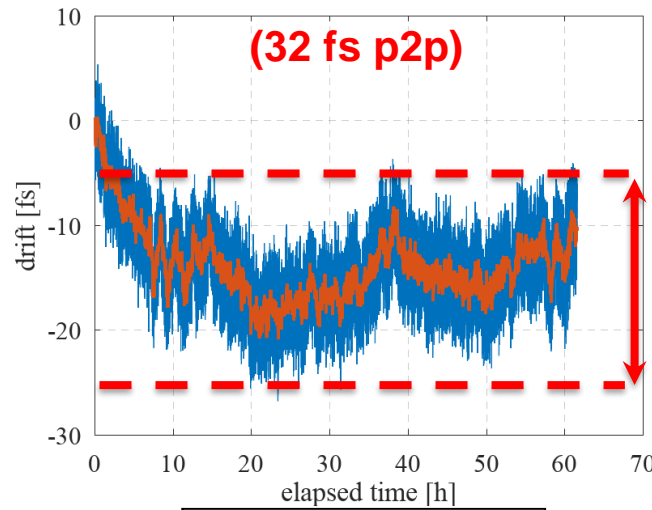
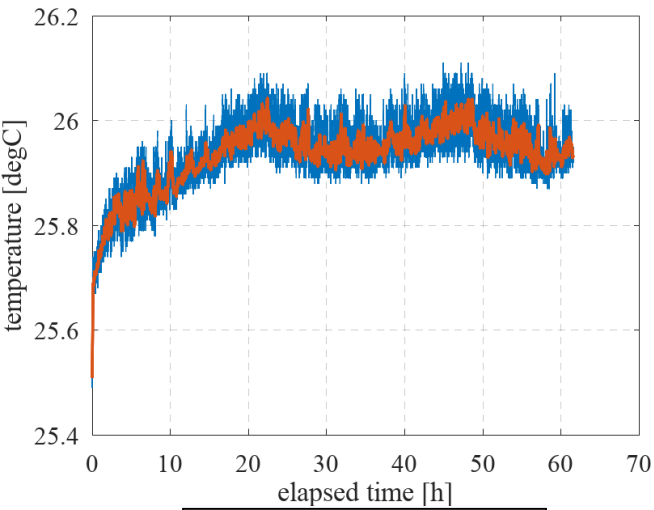
OOL drift measurement (preliminary)



Current and future activities



OOL drift measurement (preliminary)

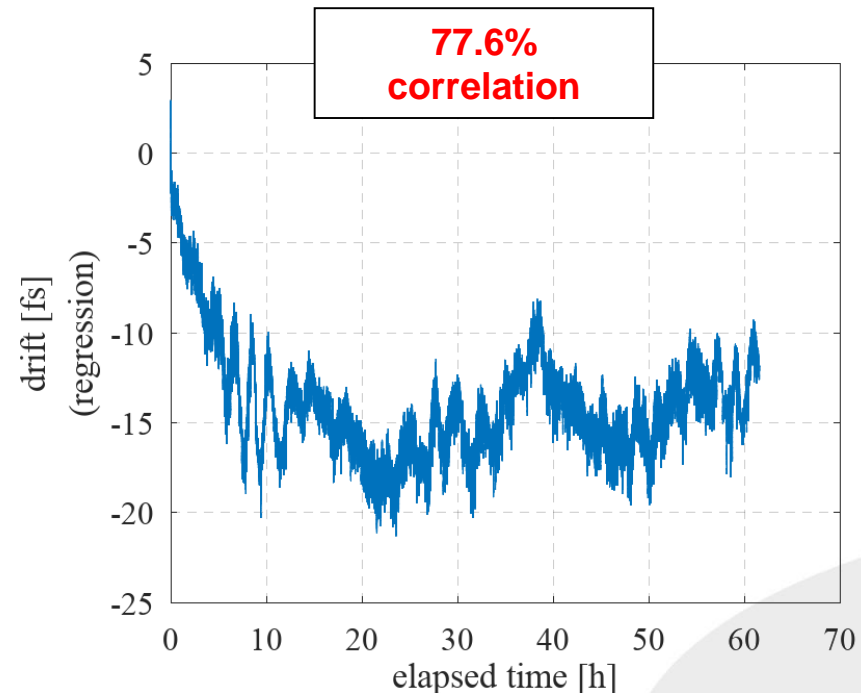
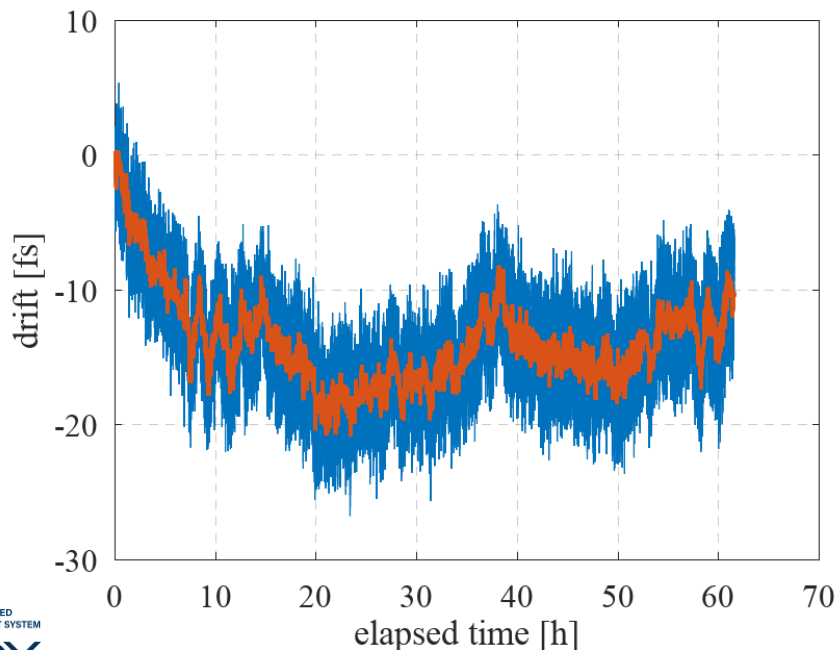


OOL drift measurement (preliminary)

developed a model of measurement doing a multivariate linear regression analysis (a possible time lag effect due to the humidity is not considered)

normalized_drift =

$$\begin{aligned}
 & -0.039 * \text{normalized_power_avg_contrib_link1} \\
 & +0.566 * \text{normalized_power_avg_contrib_link2} \\
 & +0.095 * \text{normalized_humidity_contrib} \\
 & -0.373 * \text{normalized_temperature_contrib}
 \end{aligned}$$



Current and future activities

- activities on the pulsed subsystem extension
 - ongoing drift measurements between two stabilized links
 - integration in the control system
 - polarization stabilization at the input of extension
- new HVAC system for the timing room
 - integrated temperature and humidity control with better stability
 - reduction of the environmental acoustic noise
 - decoupling from the building air conditioning
- investigations about possible replacement of the OMO
 - it has been running for more than 13 years
 - outdated architecture (out of production, limited support)
 - wishing for a laser with a unique mode-locking condition
 - need to seed a PM system (pulsed extension)

Thank you!



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BACKUP SLIDES

CERTIFIED
MANAGEMENT SYSTEM

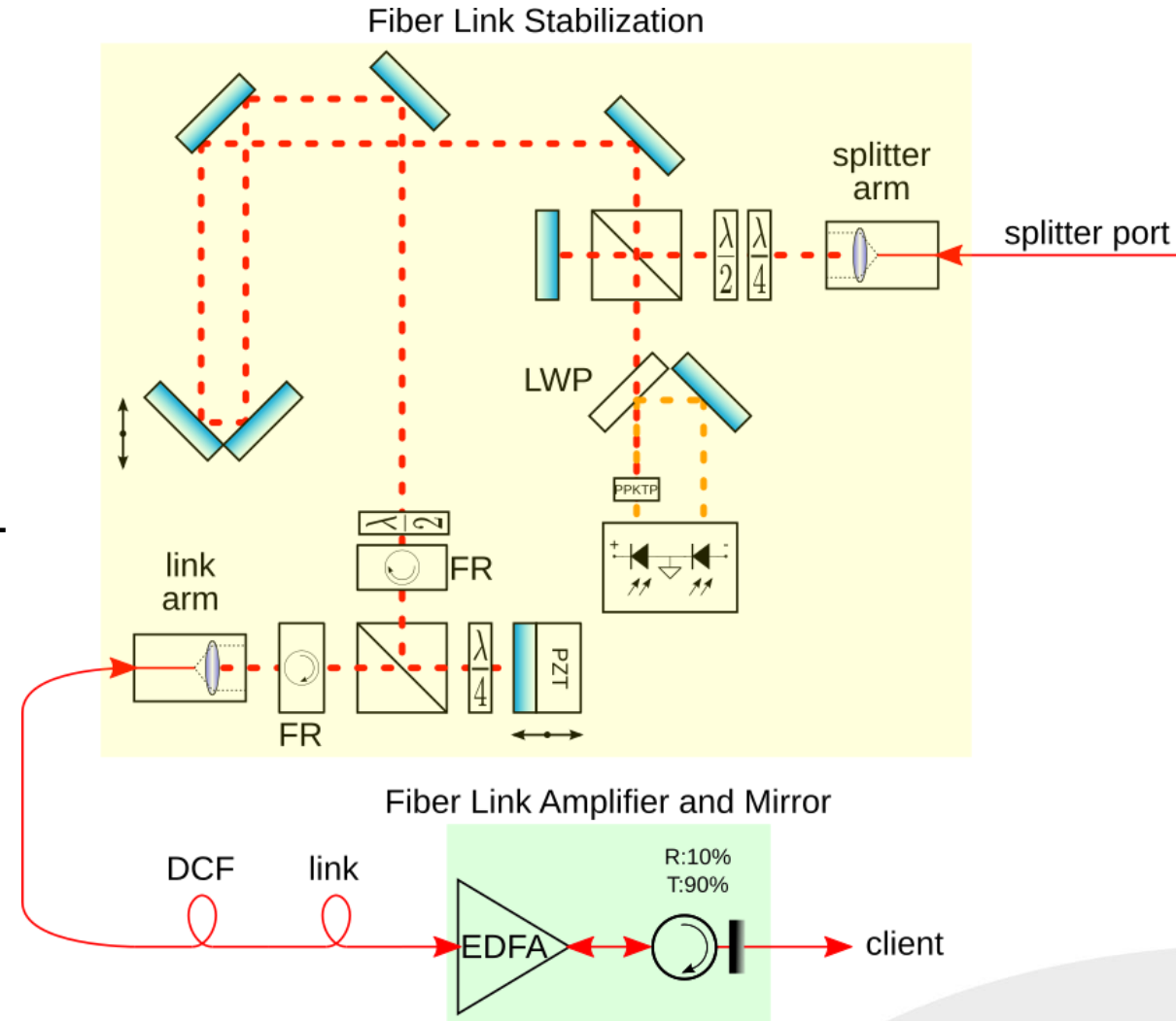


UNI EN ISO 9001:2015
UNI ISO 45001:2018

satellite event of “FELs of Europe 2nd Topical Workshop”
Perspectives and Future Challenges in Optical and RF Synchronization Systems
Hamburg, Nov 14, 2023

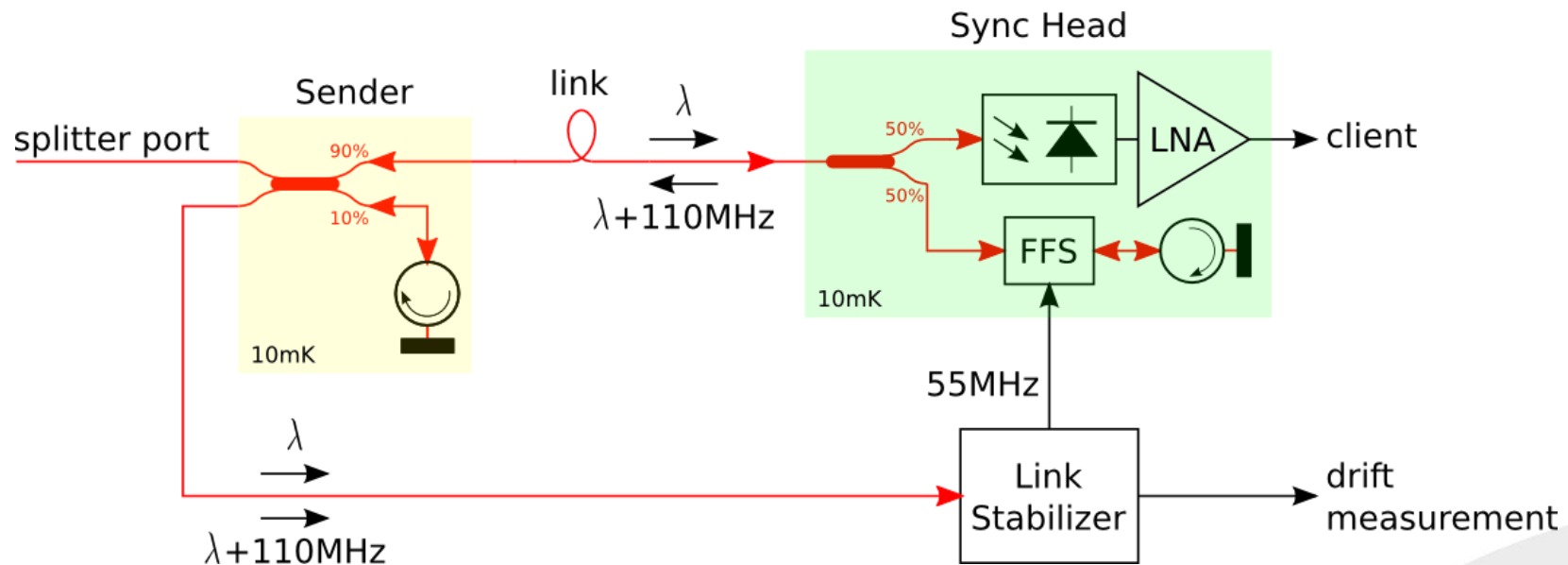
System overview: pulsed stabilization

- a link is actively stabilized
- based on the balanced cross-correlation scheme proposed for the first time at MIT
- “natural” choice to lock pulsed lasers

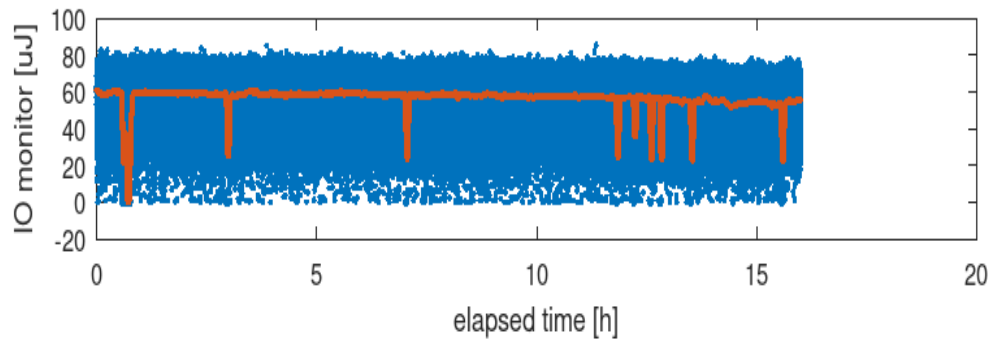
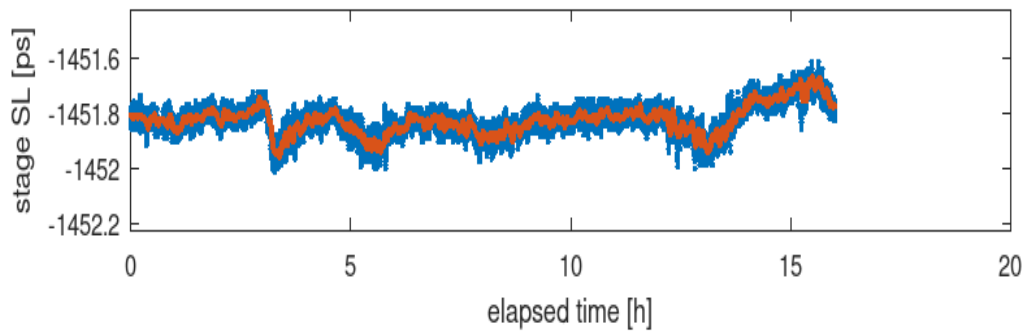
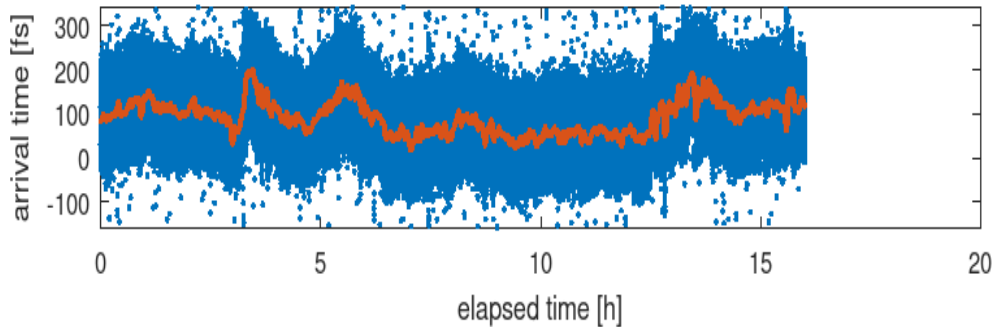


System overview: CW distribution

- a link is not actively stabilized
- heterodyne detection for the measurement of the optical phase with a Michelson interferometer, the original scheme was developed at LBNL
- tightly integrated with the LLRF controller to compensate for group delay drifts (stable RF to the plant)



Long-term FEL stability



Long-term longitudinal instabilities are controlled by a beam-based feed-forward compensation scheme.

We have implemented an optimization tool

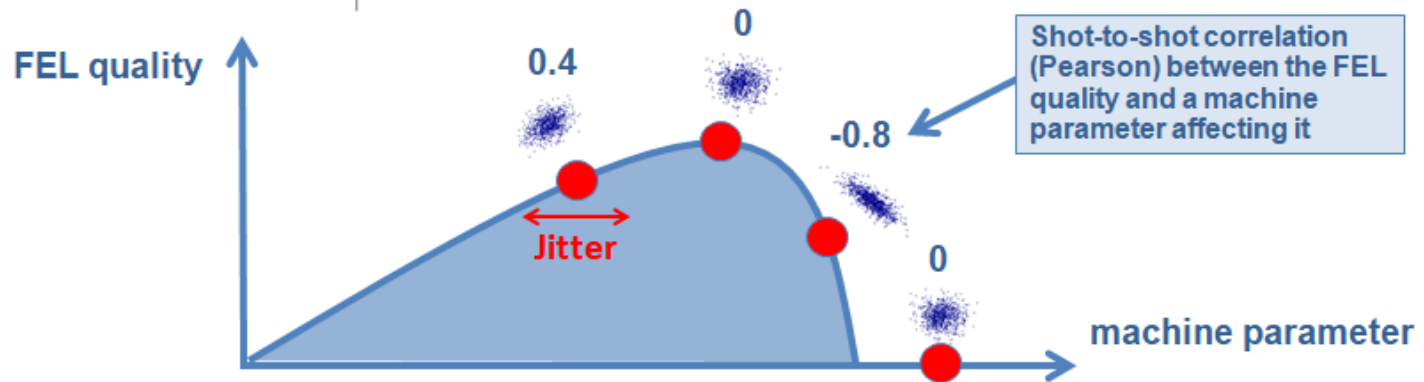
- **target:** the minimization of the correlation between the BAM and IO monitors
- **sensor:** bunch arrival monitor
- **actuator:** motorized piezo stage controlling the relative delay between the seed laser and the electrons.



Long-term FEL stability



Optimization Through Correlation Minimization



Courtesy of Giulio Gaio

- The function "**FEL quality vs. parameter**" (unknown) is supposed to have a maximum
- If the variable is affected by jitter, it is easy to measure the shot-to-shot correlation, which can be positive (left side), zero (top) or negative (right side)
- Based on the correlation sign, we know in which direction to move the variable by means of the actuator in order to restore the optimum working conditions
- **This optimizer is run continuously during machine operations**; the FEL performance is restored or kept optimal with almost no disruption for the beamline experiments
- This optimizer is generic; for each implementation the following variables have to be identified:
 - **Target**: the objective function to maximize, which is usually the FEL energy or a combination of FEL parameters
 - **Sensor**: the variable whose correlation with the target has to be minimized
 - **Actuator**: the variable used to change the sensor value

"Advances in Automatic Performance Optimization at FERMI", ICALEPCS 2017
<http://icalepcs2017.vrws.de/papers/tumpa07.pdf>