

SURFACE IMPEDANCE OF MULTILAYERED SUPERCONDUCTING CAVITIES

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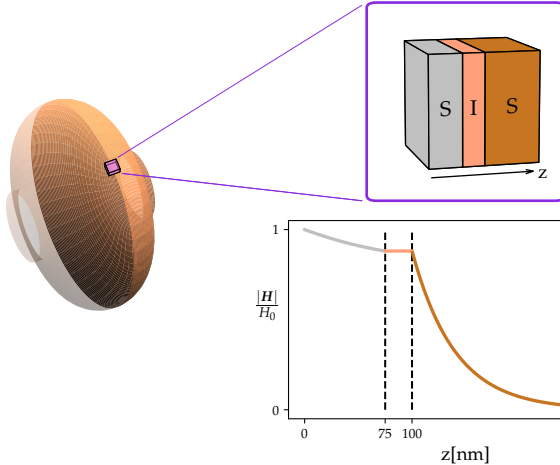
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MOTIVATION

Section 1



Why ?*

1. Niobium is expensive
2. Increase in energy efficiency
3. Higher accelerating fields

How ?

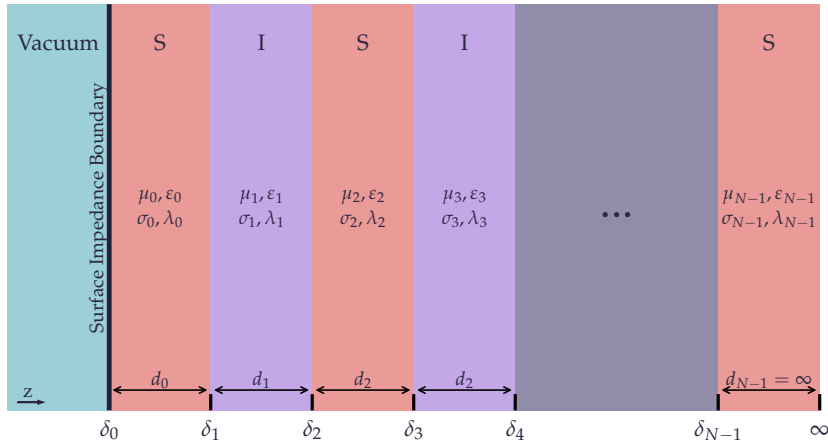
1. Replace bulk Nb with Cu, Al, etc. substrates
2. Better thermal conducting substrate
3. Shield with higher H_c material

* Valente-Feliciano, A.-M. *Superconductor Science and Technology* (2016)

REDUCTION TO SIBC

Section 2

ANALYTICAL SOLUTION



Solve Maxwell's equations in every layer $k \in \{0, \dots, N-1\}$:

$$E_x^{(k)} = \begin{pmatrix} C_{2k} \\ C_{2k+1} \end{pmatrix} \cdot \begin{pmatrix} e^{j\alpha_k z} \\ e^{-j\alpha_k z} \end{pmatrix} := \mathbf{C}_k \cdot \mathbf{u}_k$$

$$H_y^{(k)} = -\frac{\alpha_k}{\omega\mu_k} \begin{pmatrix} C_{2k} \\ C_{2k+1} \end{pmatrix} \cdot \begin{pmatrix} e^{j\alpha_k z} \\ -e^{-j\alpha_k z} \end{pmatrix} := -\frac{\alpha_k}{\omega\mu_k} \mathbf{C}_k \cdot \mathbf{v}_k$$

where $\alpha \in \mathbb{C}$ depends on material type:

$$\text{Insulator : } \alpha^2 = \mu\epsilon\omega^2$$

$$\text{Normal Conductor : } \alpha^2 = \mu\epsilon\omega^2 - j\mu\sigma\omega$$

$$\text{Superconductor (two-fluid) : } \alpha^2 = \mu\epsilon\omega^2 - j\mu\sigma\omega - \frac{1}{\lambda^2}$$

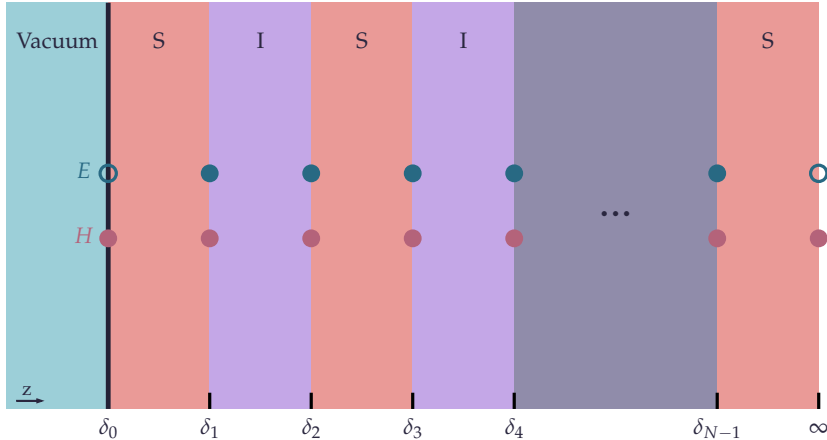
Surface impedance boundary condition

$$\mathbf{n} \times \mathbf{E} = Z(\mathbf{n} \times (\mathbf{n} \times \mathbf{H}))$$

yields surface impedance

$$Z(\omega) = \frac{E_x^{(0)}(\delta_0)}{H_y^{(0)}(\delta_0)} = -\frac{\omega\mu_0}{\alpha_0} \frac{\mathbf{C}_0 \cdot \mathbf{u}(\delta_0)}{\mathbf{C}_0 \cdot \mathbf{v}(\delta_0)}$$

$\Rightarrow$ We need the coefficient vector $\mathbf{C}_0$


$$2N \text{ Unknowns} = 1 \text{ vacuum constraint} + 2(N - 1) \text{ interface constraints} + 1 \text{ infinity constraint}$$

Mathematically the constraints are:

- Vacuum constraint:

$$H_y^{(0)}(\delta_0) = H_0$$

- Interface constraints:

$$E_x^{(k)}(\delta_{k+1}) = E_x^{(k+1)}(\delta_{k+1})$$

$$H_y^{(k)}(\delta_{k+1}) = H_y^{(k+1)}(\delta_{k+1})$$

- Infinity constraint:

$$\lim_{z \rightarrow \infty} H_y^{(N-1)}(z) = 0$$

Implied relations between coefficients:

- Vacuum constraint:

$$\mathbf{c}_0 \cdot \begin{pmatrix} 1 \\ -1 \end{pmatrix} = -\frac{\omega\mu_0}{\alpha_0} H_0$$

- Interface constraints:

$$\mathbf{c}_k \cdot \mathbf{u}_k(\delta_{k+1}) = \mathbf{c}_{k+1} \cdot \mathbf{u}_{k+1}(\delta_{k+1})$$

$$\mathbf{c}_k \cdot \mathbf{v}_k(\delta_{k+1}) = \gamma_k \mathbf{c}_{k+1} \cdot \mathbf{v}_{k+1}(\delta_{k+1}), \quad \gamma_k = \frac{\mu_k}{\mu_{k+1}} \frac{\alpha_{k+1}}{\alpha_k}$$

- Infinity constraint:

$$\mathbf{c}_{N-1} = \mathbf{c} \begin{pmatrix} 0 \\ 1 \end{pmatrix}$$

Recursion relations via linear combination of interface constraints:

$$\begin{aligned}\mathbf{C}_k \cdot \begin{pmatrix} 1 \\ 0 \end{pmatrix} &= \frac{1}{2} e^{-j\alpha_k \delta_{k+1}} \mathbf{C}_{k+1} \cdot (\Gamma_k \mathbf{u}_{k+1}(\delta_{k+1})), & \Gamma_k &= \text{diag}(1 + \gamma_k, 1 - \gamma_k) \\ \mathbf{C}_k \cdot \begin{pmatrix} 0 \\ 1 \end{pmatrix} &= \frac{1}{2} e^{j\alpha_k \delta_{k+1}} \mathbf{C}_{k+1} \cdot (\Gamma_k^\tau \mathbf{u}_{k+1}(\delta_{k+1})), & \Gamma_k^\tau &= \text{diag}(1 - \gamma_k, 1 + \gamma_k)\end{aligned}$$

yields characteristic matrix equation for each layer:

$$\mathbf{C}_k = \tau_{k,k+1} \mathbf{C}_{k+1}, \quad \tau_{k,k+1} = \frac{1}{2} \begin{pmatrix} e^{-j\alpha_k \delta_{k+1}} [\Gamma_k \mathbf{u}_{k+1}(\delta_{k+1})]^T \\ e^{j\alpha_k \delta_{k+1}} [\Gamma_k^\tau \mathbf{u}_{k+1}(\delta_{k+1})]^T \end{pmatrix}$$

and consequently a single transfer matrix:

$$\mathbf{C}_0 = T \mathbf{C}_{N-1} := \left[\prod_{k=0}^{N-2} \tau_{k,k+1} \right] \mathbf{C}_{N-1}$$

Now notice:

$$\mathbf{C}_0 = T\mathbf{C}_{N-1} = CT \begin{pmatrix} 0 \\ 1 \end{pmatrix} = C \begin{pmatrix} T_{01} \\ T_{11} \end{pmatrix}$$

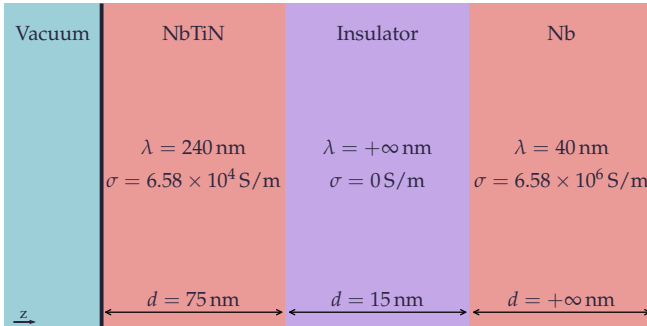
So we find the surface impedance:

$$Z(\omega) = -\frac{\omega\mu_0}{\alpha_0} \frac{T_{01} + T_{11}}{T_{01} - T_{11}}$$

- Transfer matrix depends on all material parameters
- $Z(\omega)$ is determined by transfer matrix, which we can compute
- $Z(\omega)$ is a non-linear complex-valued function of ω

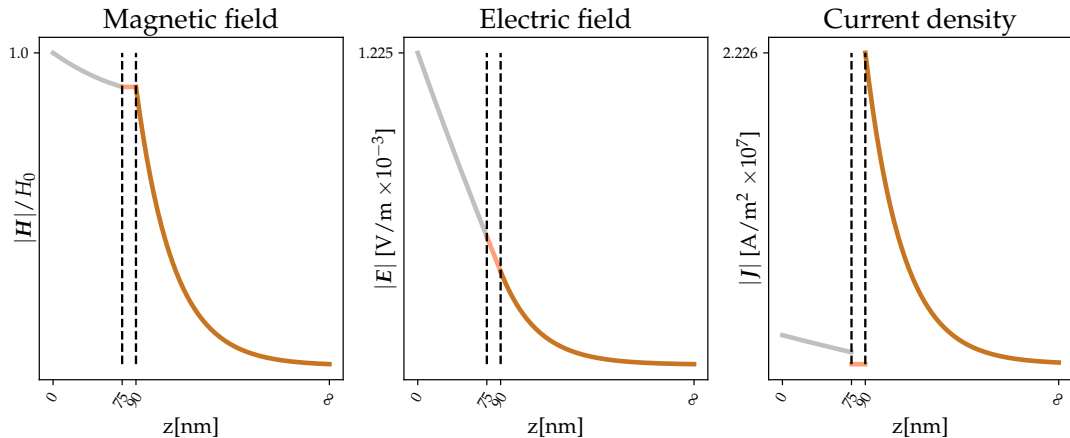
EXAMPLE

Bulk Nb with generic insulator layer and NbTiN sputtering at $f = 1.3 \text{ GHz}^*$



$$Z(\omega) = 21.462 \times 10^{-9} \Omega + 1.225 \times 10^{-3} j \Omega$$

* Keckert S., *PhD Dissertation, Universität Siegen* (2020)



EIGENVALUE PROBLEM

Section 3

WEAK FORMULATION

Weak formulation from Maxwell's equation with surface impedance boundary leads to the following weak formulation:

$$\frac{1}{\kappa^2} \int_{\Omega} dV [(\nabla \times \mathbf{u}) \cdot (\nabla \times \mathbf{v})] + \frac{\tau}{\kappa} \frac{Z_0}{Z(\omega)} \int_{\partial\Omega} dS [(\mathbf{n} \times \mathbf{u}) \cdot (\mathbf{n} \times \mathbf{v})] + \tau^2 \int_{\Omega} dV [\mathbf{u} \cdot \mathbf{v}] = 0$$

where $\mathbf{u}$ is the trial function and $\mathbf{v}$ is the test function, and

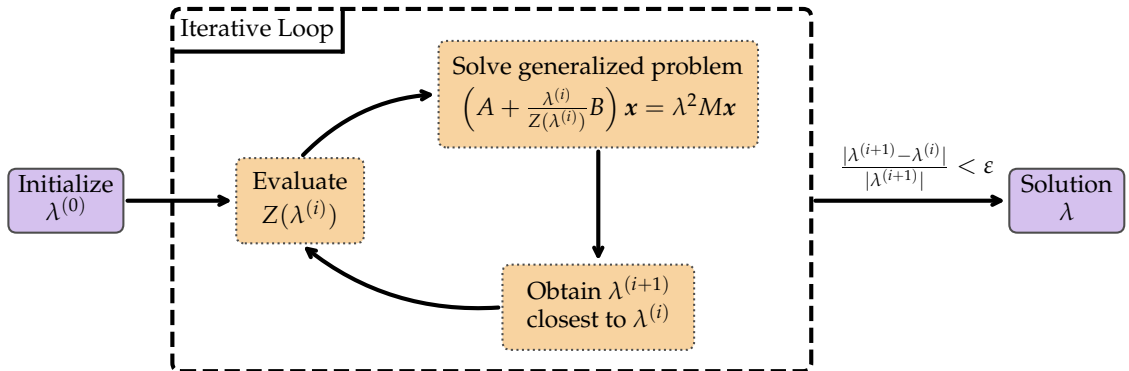
$$\kappa = \frac{2\pi f}{c}, \quad \tau = -\frac{1}{2Q} + j$$

The resulting non-linear complex eigenvalue problem is then of the form:

$$A\mathbf{x} + \frac{\lambda}{Z(\lambda)} B\mathbf{x} = \lambda^2 M\mathbf{x}$$

NONLINEAR PROBLEM

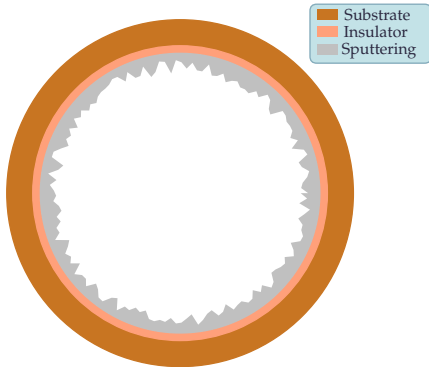
We solve the non-linear problem using a fixed point iteration



OUTLOOK & CONCLUSION

Section 4

OUTLOOK



- Replace thickness of sputtering layer with stochastic process, i.e. $Z(\omega) \rightarrow Z(\mathbf{r}, \omega)$
- Model stochastic process with Karhunen-Loeve expansion informed by experimental data.
- Use polynomial chaos expansion to efficiently compute statistics of the quality factor, e.g. mean and standard deviation.

CONCLUSION

- Multilayered cavities can be modelled via SIBC
- Analytical solution can support many multilayer variations
- Resulting eigenvalue problem is non-linear and complex-valued, but can be handled with fixed-point iteration

Questions?