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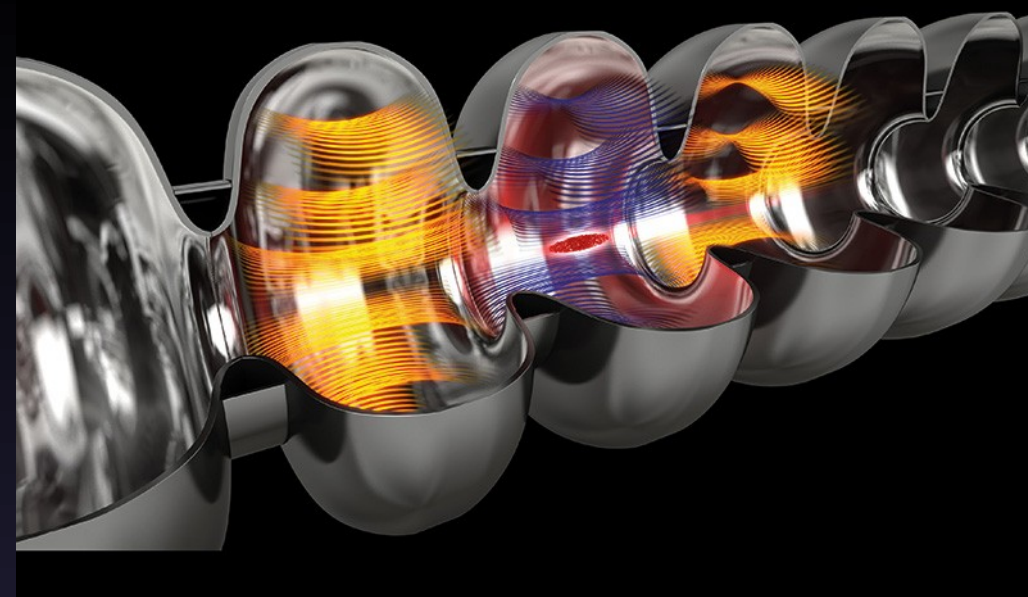
Sensitivity Measurements for Mid-T heat treated SRF Cavities

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Motivation: Higher Performance in RF Cavities

- Interest in Cavities with higher performance (high quality factor Q_0 and high accelerating field E_{acc})
- Q_0/E_{acc} curves higher after mid-T heat treatment compared to no mid-T
- Also higher Sensitivity probably due to flux trapping after mid T heat treatment
- Sensitivity defined as $S = \Delta R_s / B_{trapped}$: Ratio of surface resistance between two measurement types (with and without ext. B) per trapped magnetic field

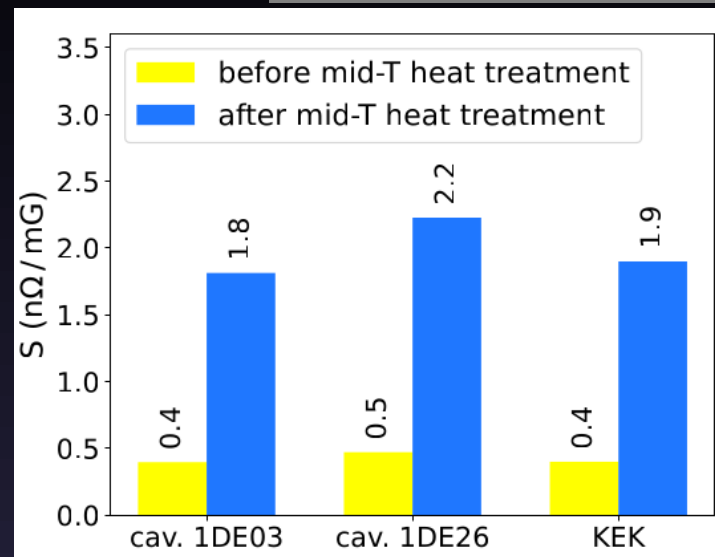
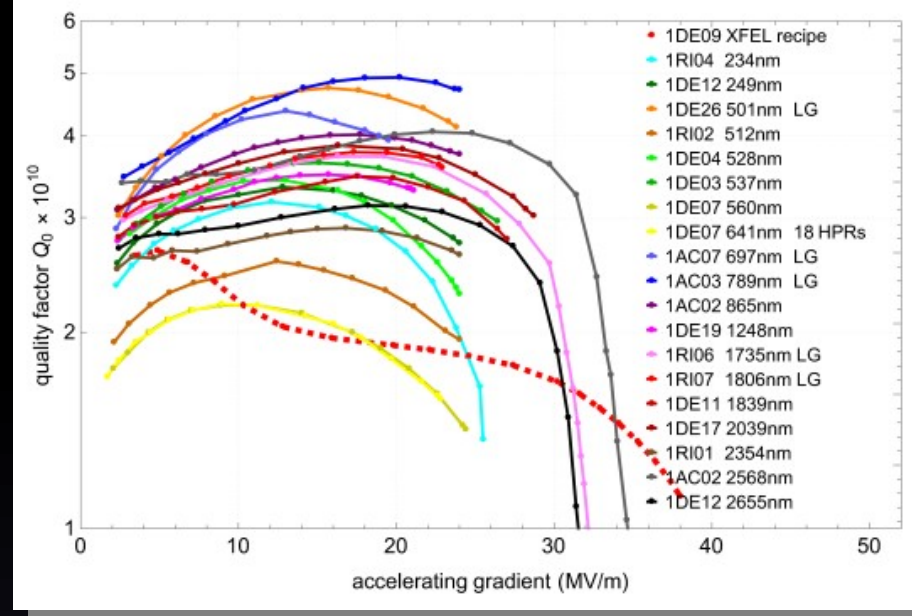
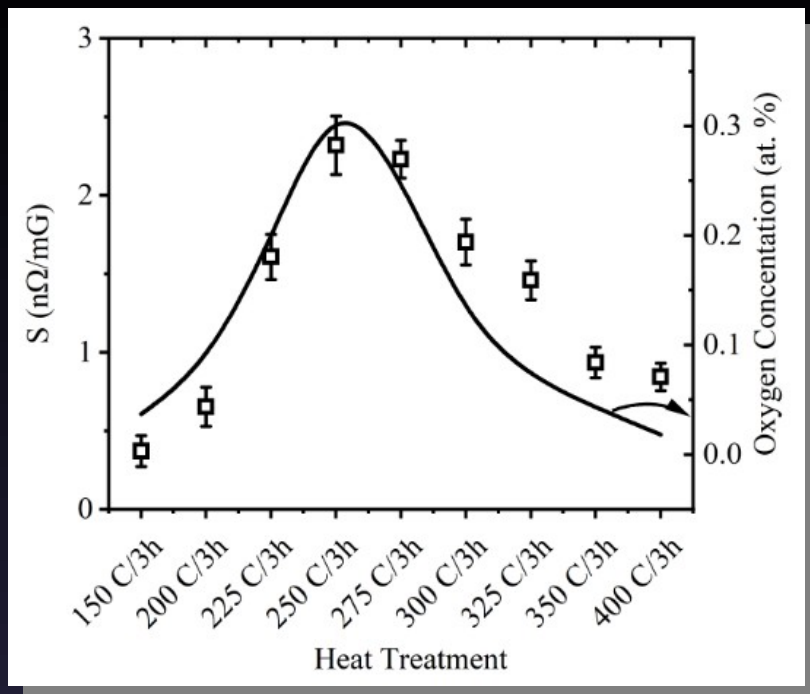
→ **Investigation of the correlation between Sensitivity S and mid-T heat treatment**



Physical
Measurement
Properties

Mid-T Heat Treatment

- Medium temperature approx. 250-350 °C
- ~3-20 h



- Mid-T → higher Q_0/E_{acc} curve, but earlier quench
- Sensitivity increases with mid-T heat treatment

[Impact of medium temperature heat treatment on flux trapping sensitivity in srf cavities, P. Dhakal, et al. arXiv:2405.10085v1, 2024, Correlation of SRF performance to oxygen diffusion length of medium temperature heat treated cavities*. arXiv:2407.07779v1, 2024]

Quality factor Q_0 vs. Accelerating field E_{acc}

Q_0 : defined as stored energy per dissipated power in cavity walls

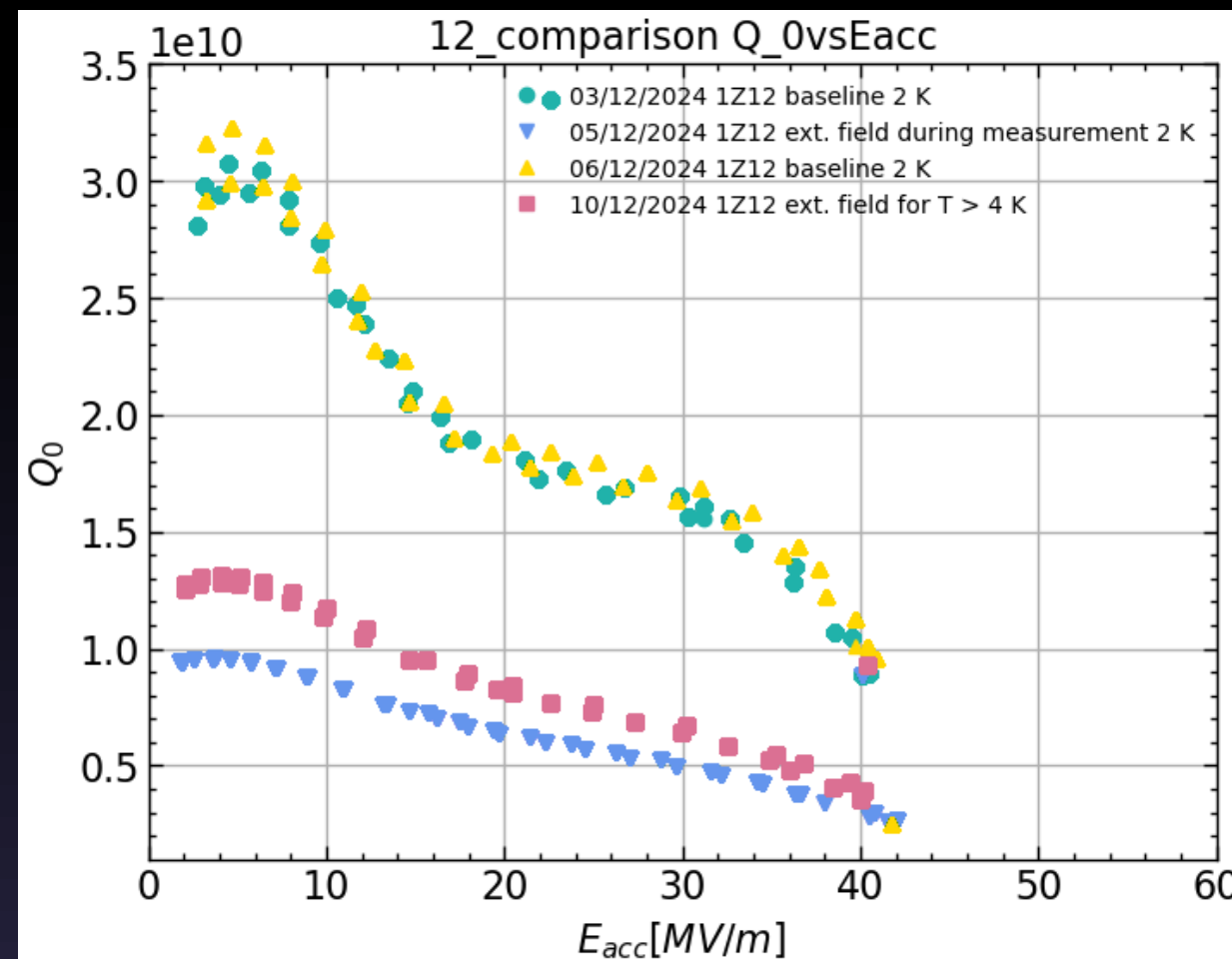
Influences : shape, electropolishing techniques, cleanliness of niobium surface, mid-T heat treatment, etc.

E_{acc} : Average accelerating electric field that electron sees during transit through cavity

To find R_s and later S we use:

$$R_s(E_{acc}) = G/Q_0(E_{acc})$$

with Geometry factor $G=271.5 \Omega$



Sensitivity S and Surface Resistance R_s



$$\text{Sensitivity } S = \Delta R_s / B_{\text{trapped}}$$

dependent on pinning centres
in bulk material

Surface resistance:

$$R_s(T, B) = R_{BCS}(T) + R_{res} + R_{flux}(B)$$

R_{BCS} : temperature dependent contribution by
Bardeen Cooper Schrieffer (BCS) theory

$R_{flux}(B)$: impact by normal conducting pinning
centers with dependence on magnetic field

R_{res} : constant residual resistance

Magnetic Field and the Meissner state

SC: $T < T_c = 9.2 \text{ K}$, $B < B_c = 0.22 \text{ T}$ for 2 K

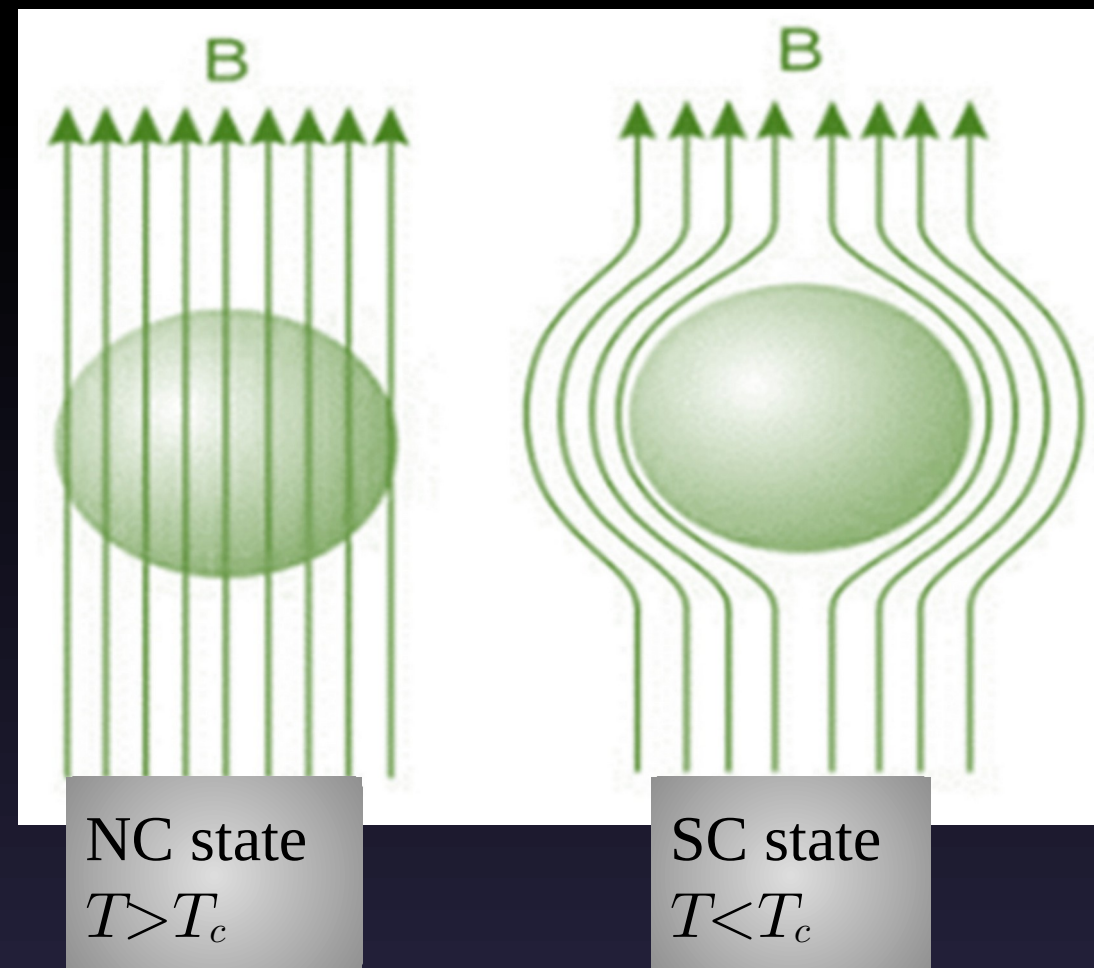
$$B_{\text{trapped}} = ((B_{nc} - B_{sc}) / (M * B_{nc} - B_{nc})) * B_{\text{ambient}}$$

Meissner factor $M = B_{sc, \text{Meissner}} / B_{nc}$: difference between theoretical possible and experimentally measured field

M derived from simulation data considering cavity geometry and ideal Meissner state

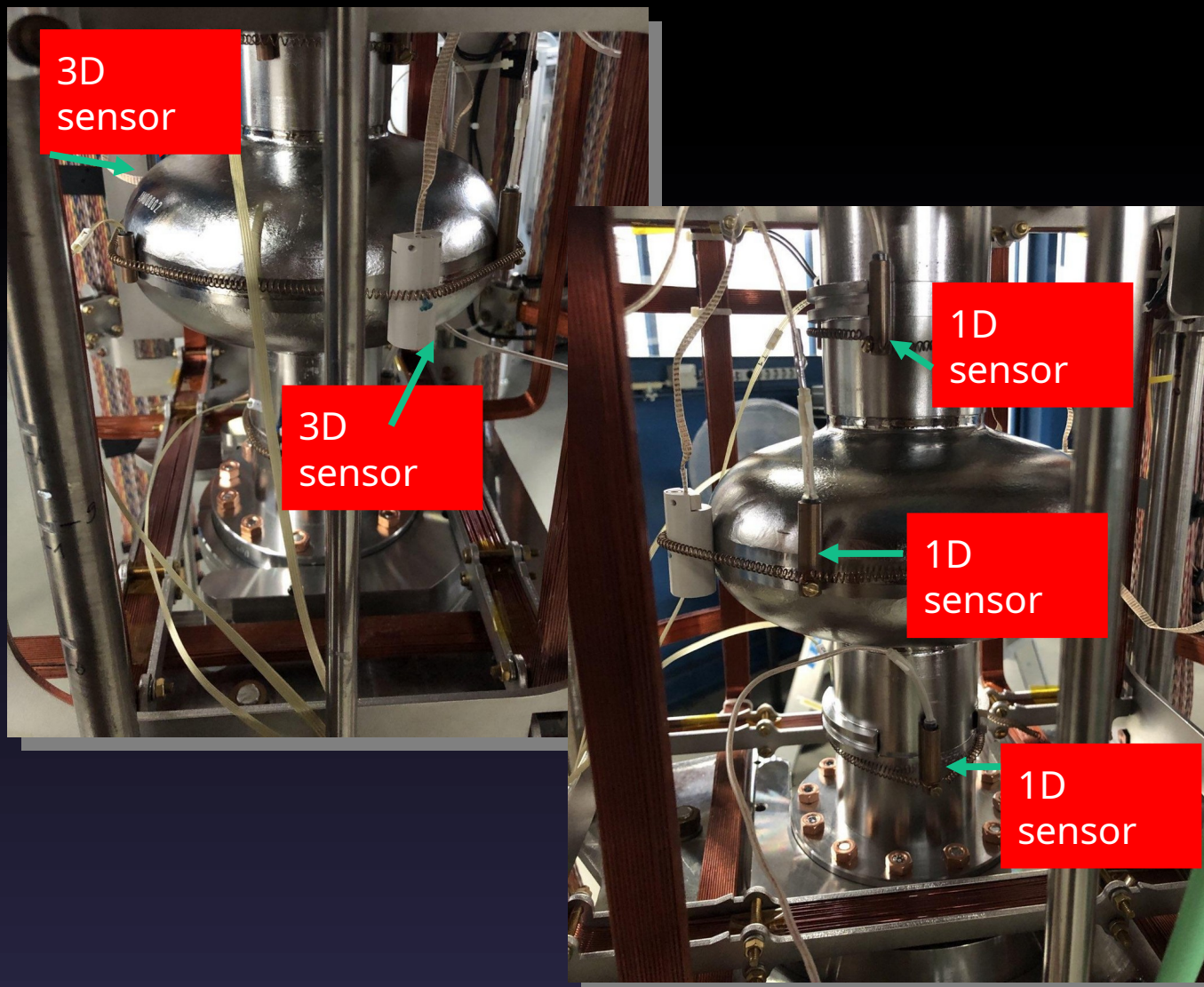
B_{nc} : magn. field in normal conducting state

B_{sc} : magn. field in superconducting state



Measurement Process

Single-cell SRF Cavity



- Niobium SRF cavity
- Two 3D Bartington magnetosensors for magnetic field measurements
- Three 1D Bartington magnetosensors, z-axis

Measurement of magnetic field lines at sensors' location

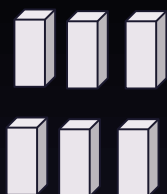
Measurement Components and Challenges

Server AV2



Measurement Components

Filters



Dispatcher Box

X Y Z(sensor 1)
X Y Z(sensor 2)

Panelmeter: ADC converter, analog-to-digital converter

DecaPSU: Power Supply Unit, supplies sensors with power

sensor 1

sensor 2

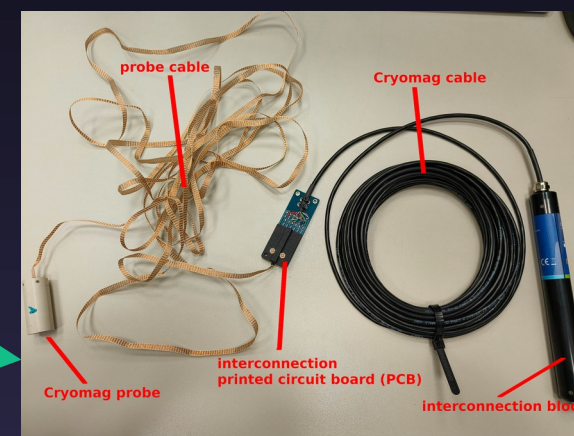
XATC2

3D Sensors with electronic rods



Challenges

- Low Pass Filters: filter out interference signals in 3D sensors that probably stem from conduction wires
- Assembly of electronic rod deviating from Bartington® recommendation

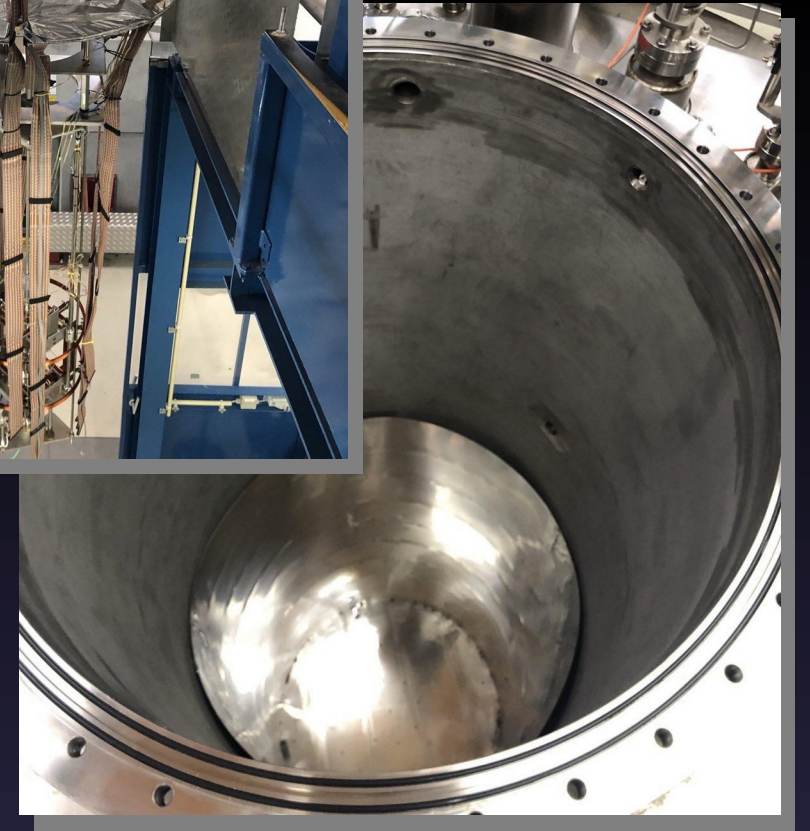
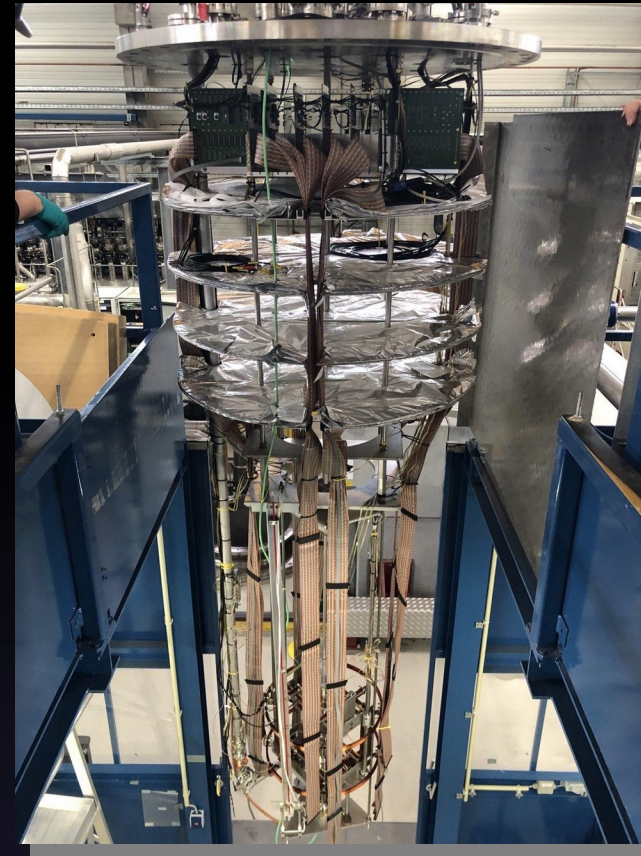


Cavity Measurement Process

Two different measurement modii: with/without Helmholtz-coil for determining $\Delta R_s \rightarrow S$

Expected magnetic field with activated Helmholtz coils at equator by calculation: $7.2 \mu\text{T}$, for $I = 23 \text{ mA}$

Ambient field inside concrete pit(without insert): $\leq 100 \text{ nT}$ (offset), included in measured magnetic background field



Results for Cavity 1Z12

Measurement Process

New single cell medium grain niobium cavity

No mid-T heat treatment

XFEL treatment: 800 °C+ low-T 120 °C

1. 1st baseline measurement

-cooldown to 2 K, $B_{ext} = 0$

2. Magnetic field measurement

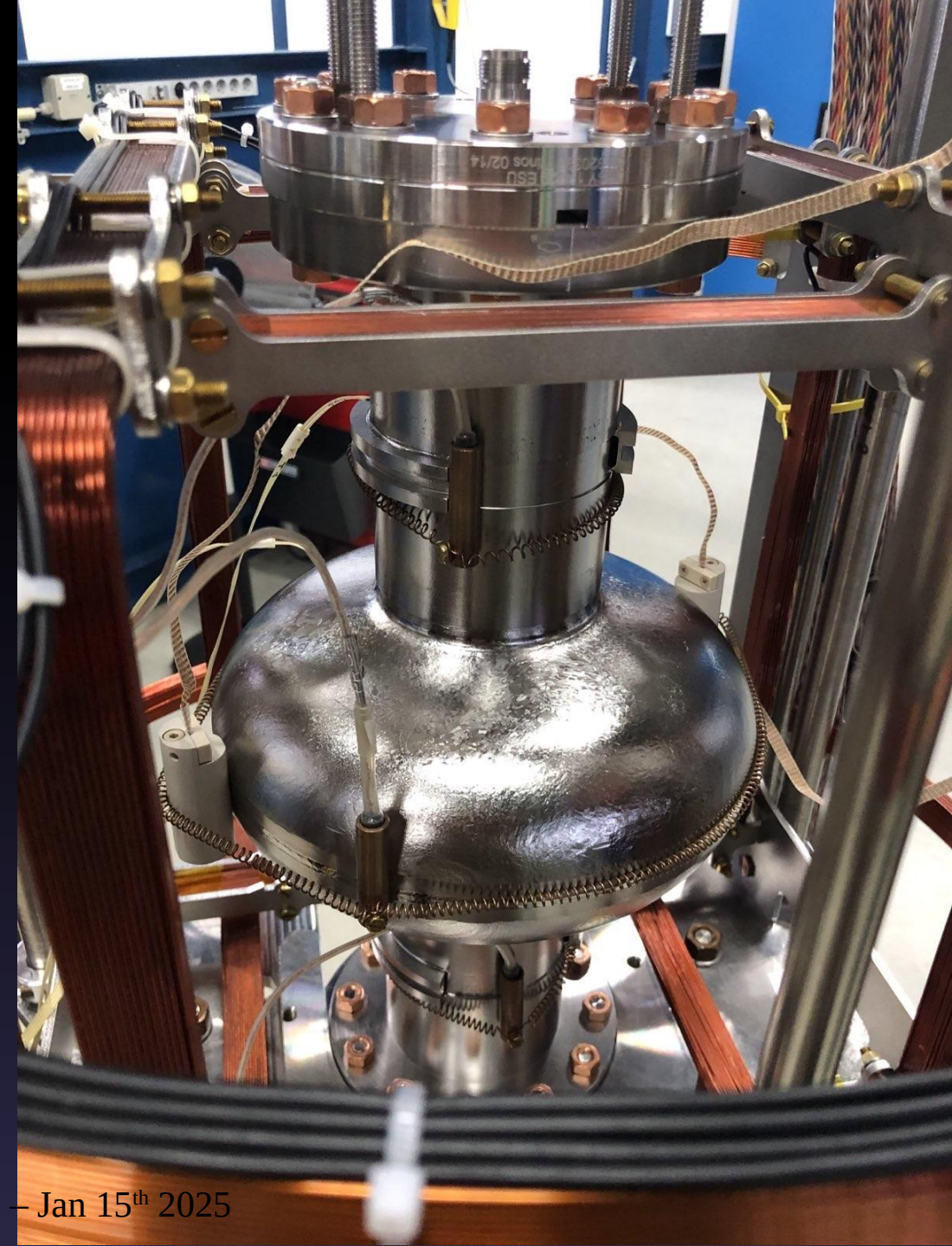
-warmup to 40 K, $B_{ext} \approx 7.2 \mu\text{T}$, cooldown to 2 K

3. 2nd baseline measurement

-warmup to 20 K, cooldown to 2 K, $B_{ext} = 0$

4. Magnetic field measurement

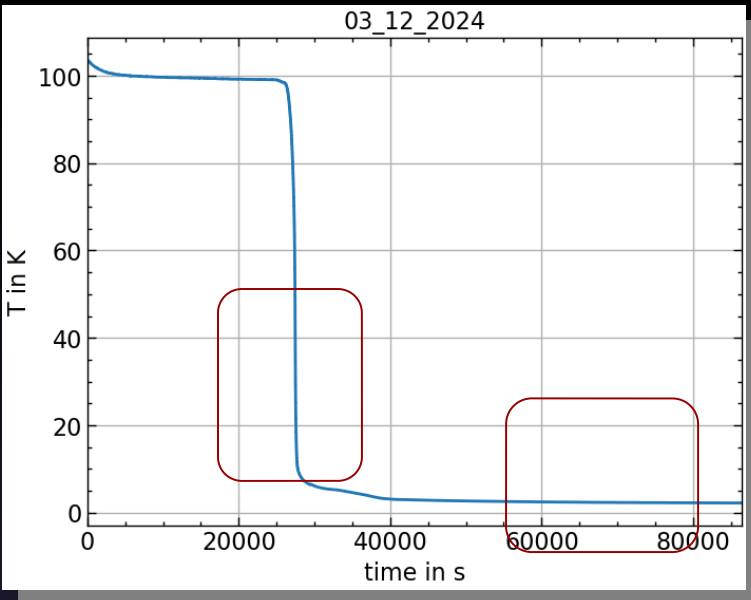
-warmup to 20 K, $B_{ext} \approx 7.2 \mu\text{T}$, cooldown to 4 K, $B_{ext} = 0$, cooldown to 2 K



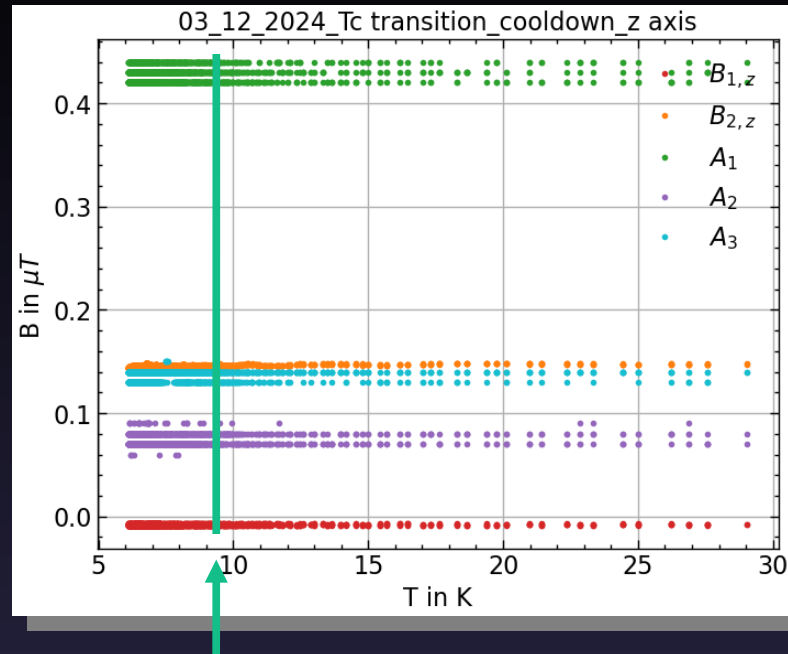
1st baseline measurement

1st baseline measurement
-cooldown to 2 K, $B_{ext} = 0$

- B1,z: 3D Sensor z-axis (equator)
- B2, z: 3D Sensor z-axis(equator)
- A1: 1D Sensor (upper beam pipe)
- A2: 1D Sensor (equator)
- A3: 1D Sensor (lower beam pipe)

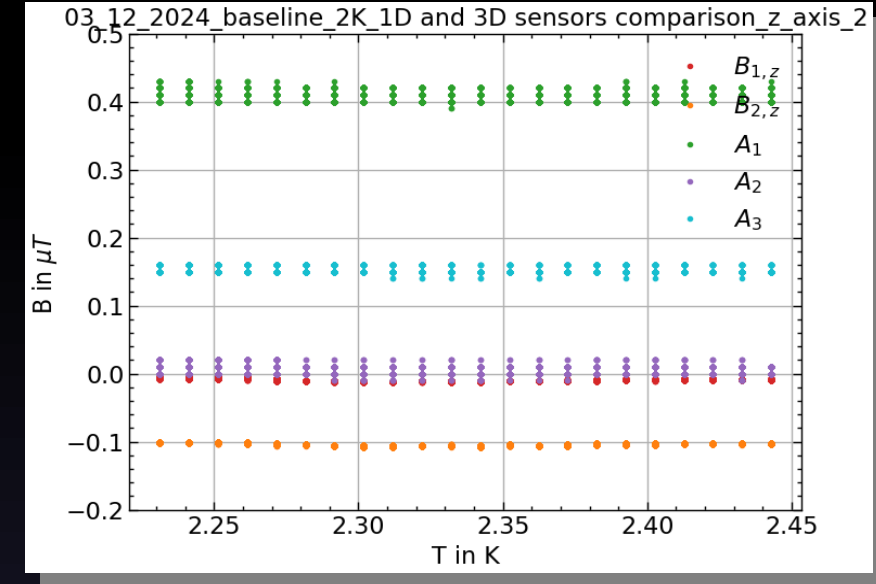


Cooldown from 100 K to 2 K



Transition T_c

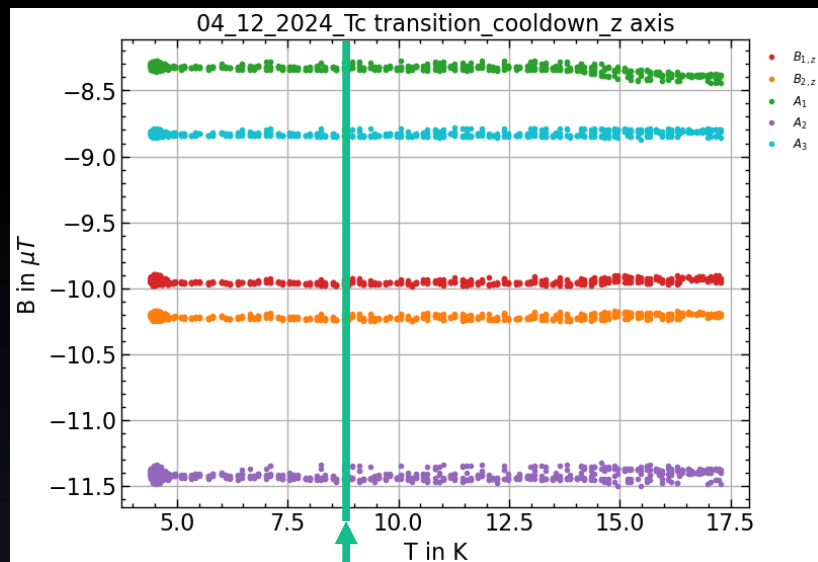
Expectation: no change in magnetic field behaviour as no B_{ext}



Baseline measurement ($B_{ext} = 0$)

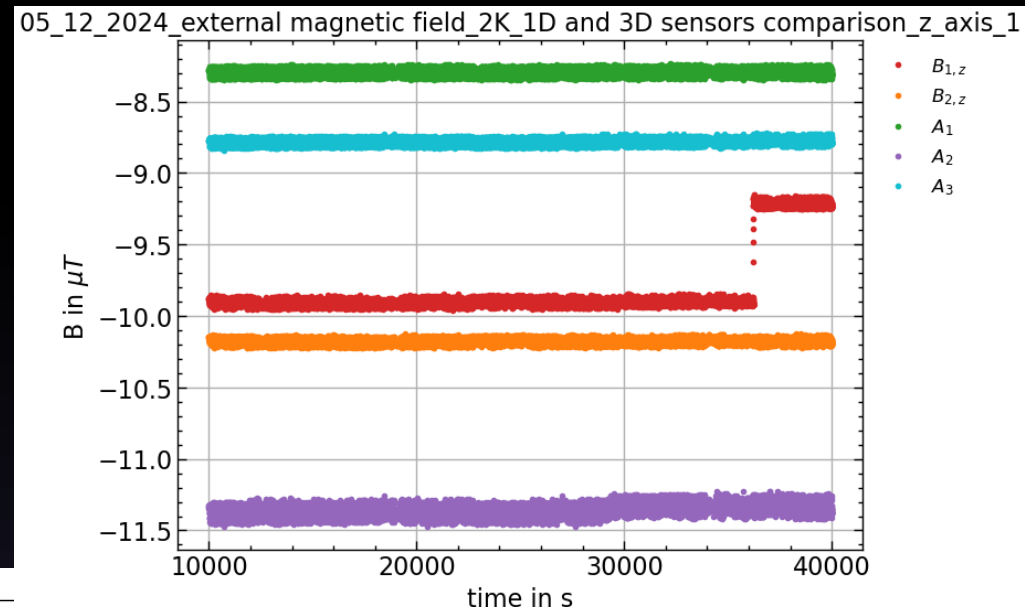
Difference in field between two 3D sensors:
0.1 μT , expected ambient field ≤ 100 nT

1st Magnetic field measurement



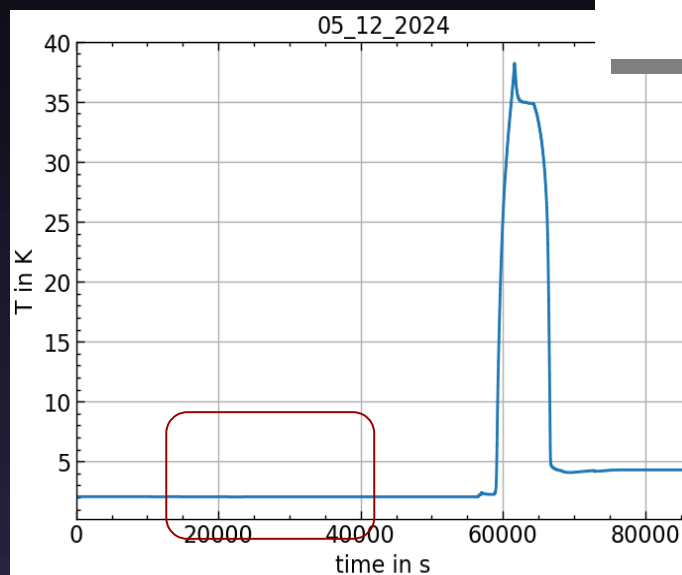
field measurement

-warmup to 40 K,
 $B_{ext} \approx 7.2 \mu T$, cooldown
to 2 K



Transition T_c

Expectation: rise in magnetic values
at T_c



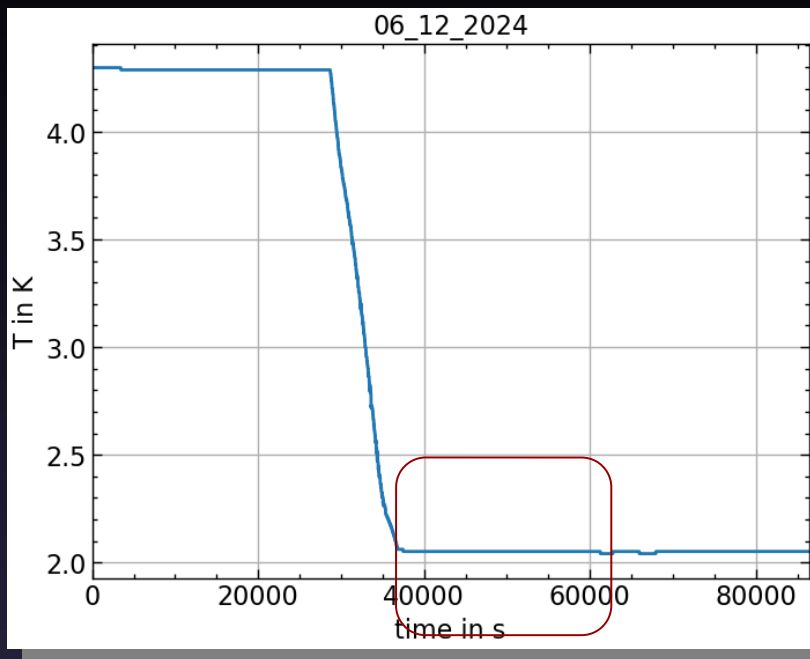
Expectation: higher B values compared
to baseline, agreement(?) with calculated
value $\sim 7.2 \mu T$

Difference between 3D sensors: $0.3 \mu T$

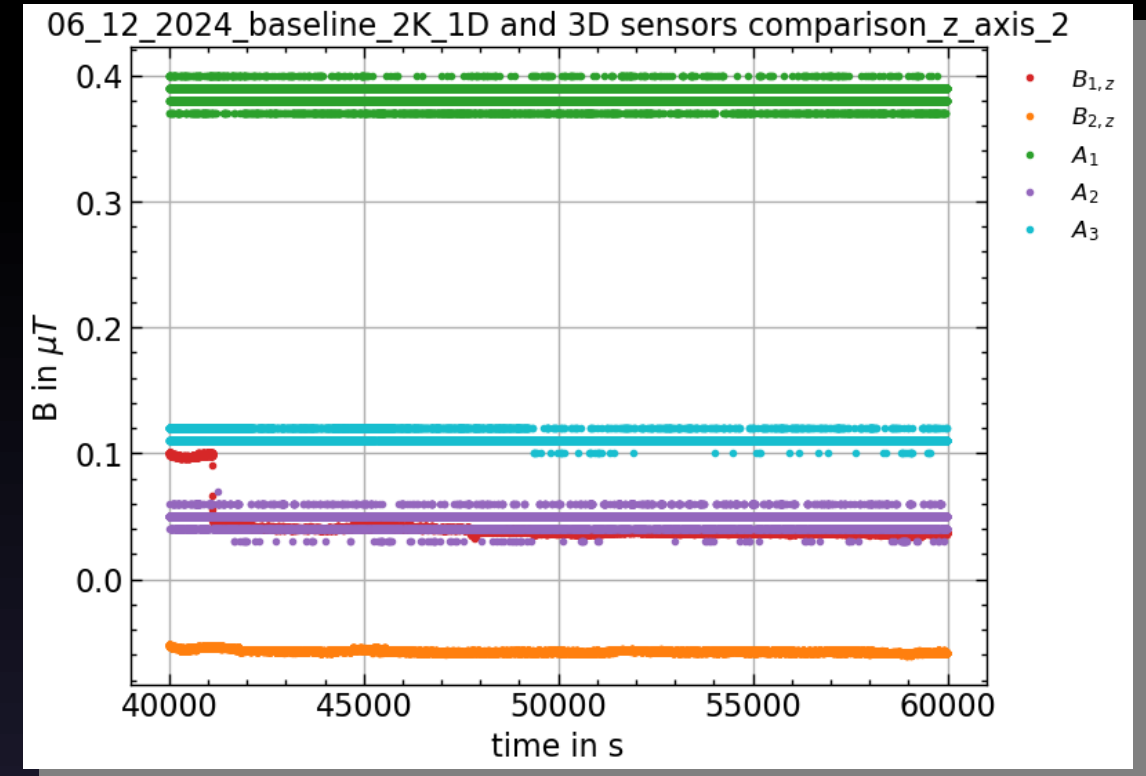
2nd baseline measurement



2nd baseline measurement
-warmup to 20 K, cooldown to 2 K,
 $B_{ext} = 0$



Cooldown to 2 K

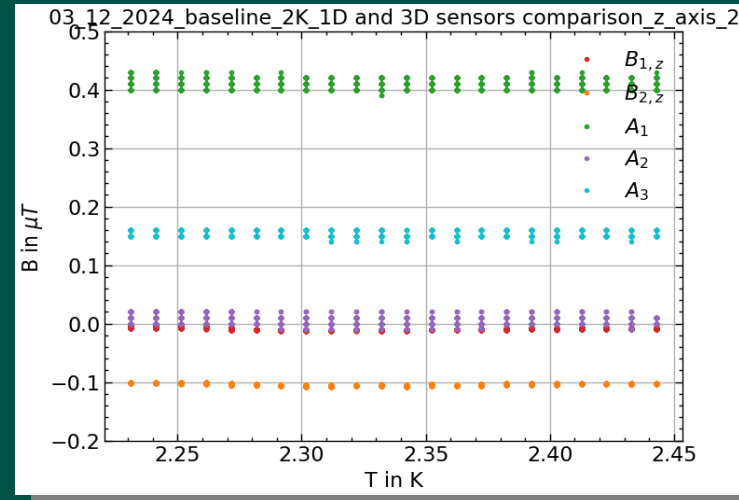
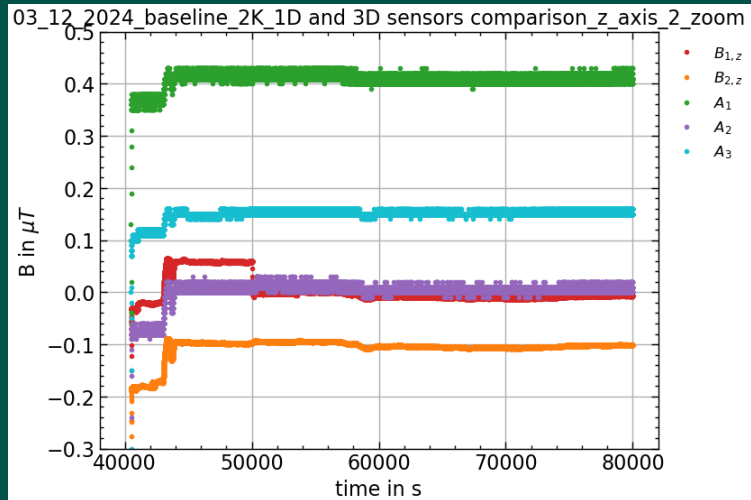


Baseline measurement ($B_{ext} = 0$)

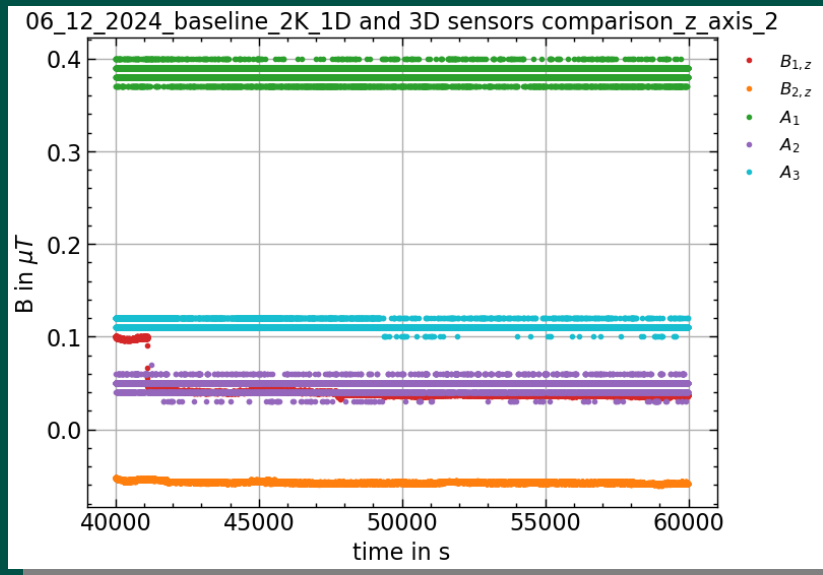
Expectation: values expected compare to 1st baseline measurement, expected ambient field ≤ 100 nT

Difference between 3D sensors: $0.1 \mu T$

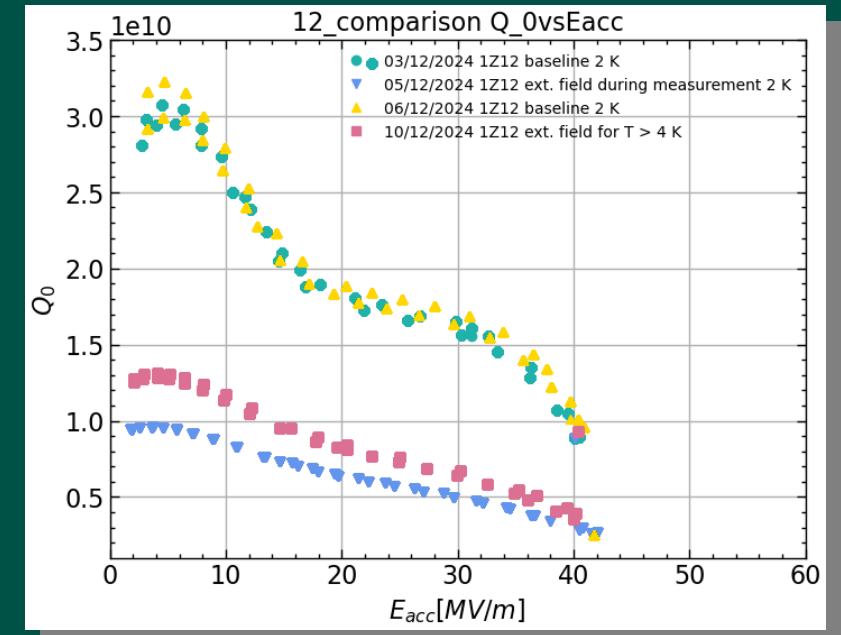
Comparison baseline measurements



1st baseline measurement over time and temperature



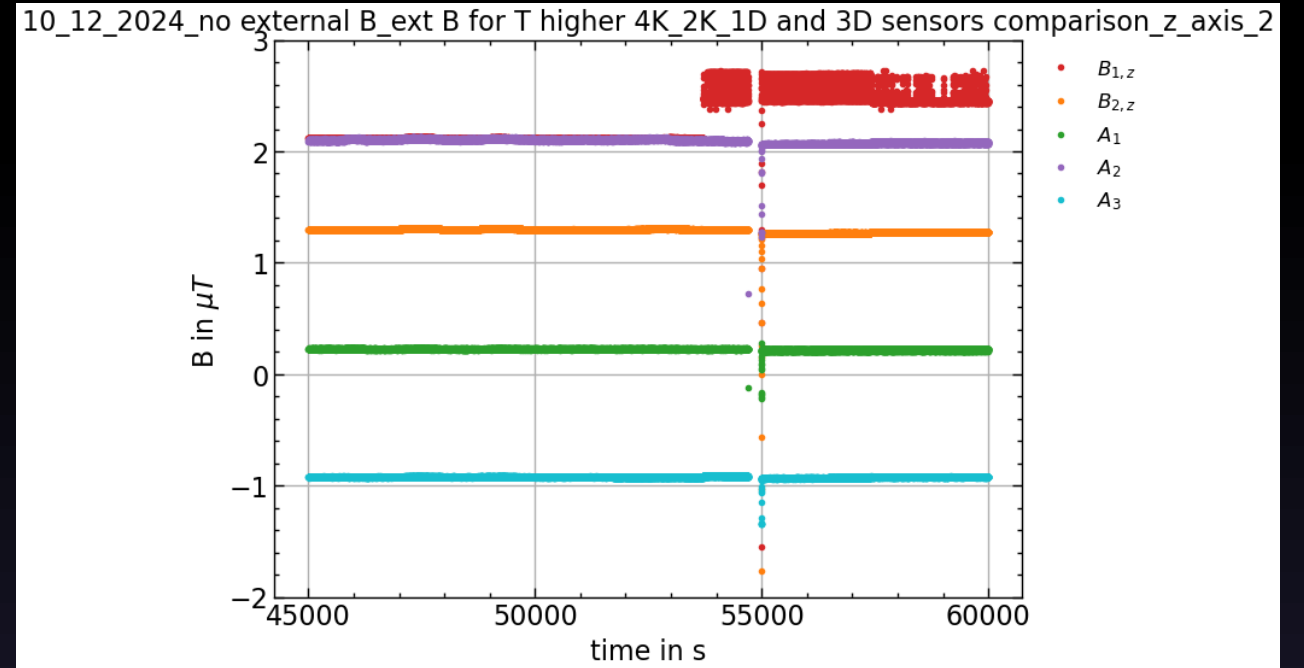
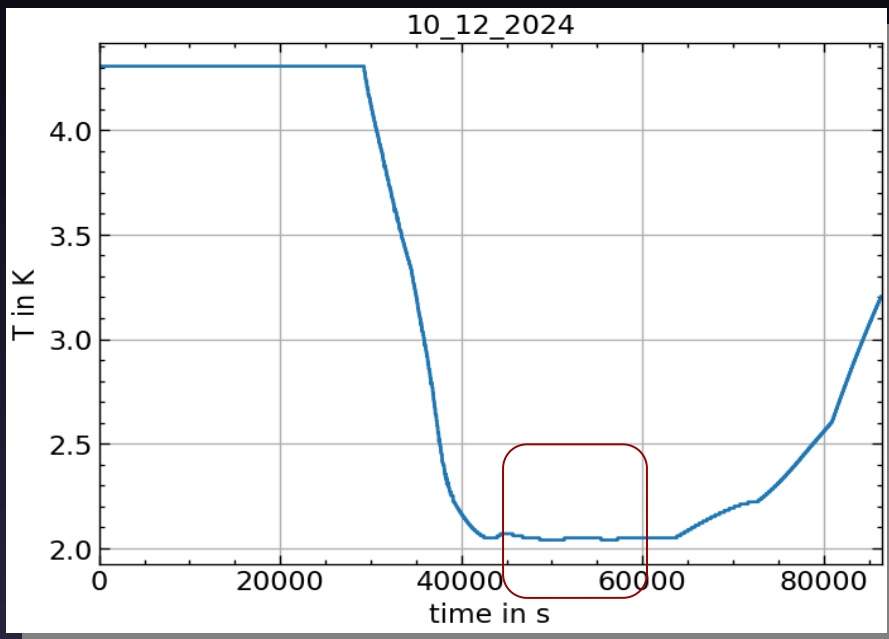
2nd baseline measurement over time



2nd Magnetic field measurement

Field measurement

-warmup to 20, $B_{ext} \approx 7.2 \mu\text{T}$,
cooldown to 4 K, $B_{ext} = 0$,
cooldown to 2 K

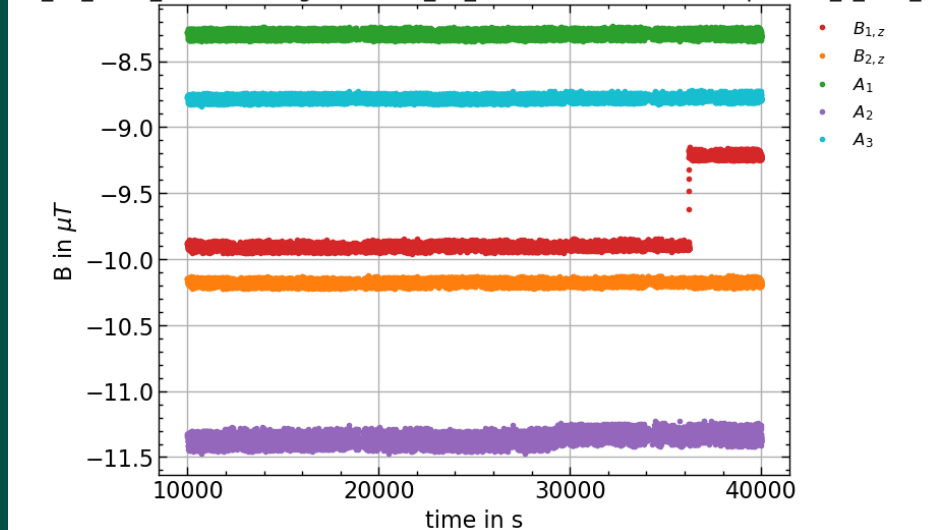


Expectation: magnetic field values expected lower as in first magnetic field measurement as field not applied during measurement

Difference between 3D sensors: $\sim 1 \mu\text{T}$

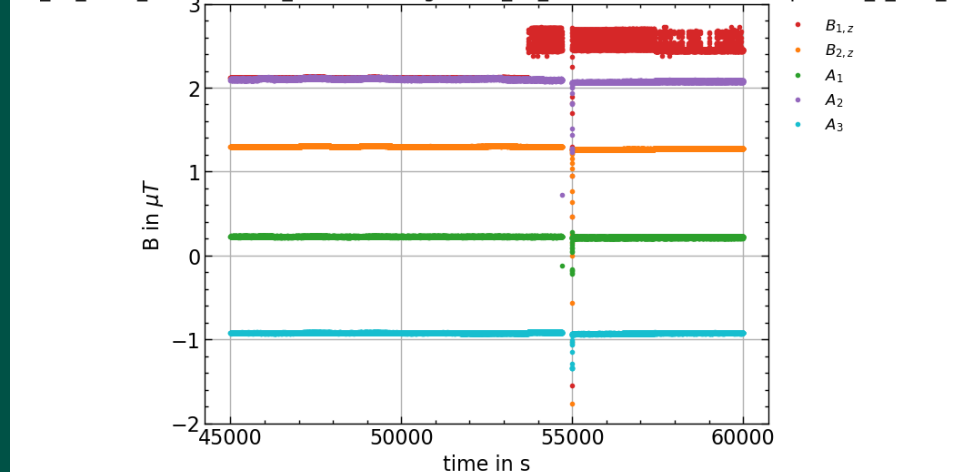
Comparison magnetic field measurements

05_12_2024_external magnetic field_2K_1D and 3D sensors comparison_z_axis_1

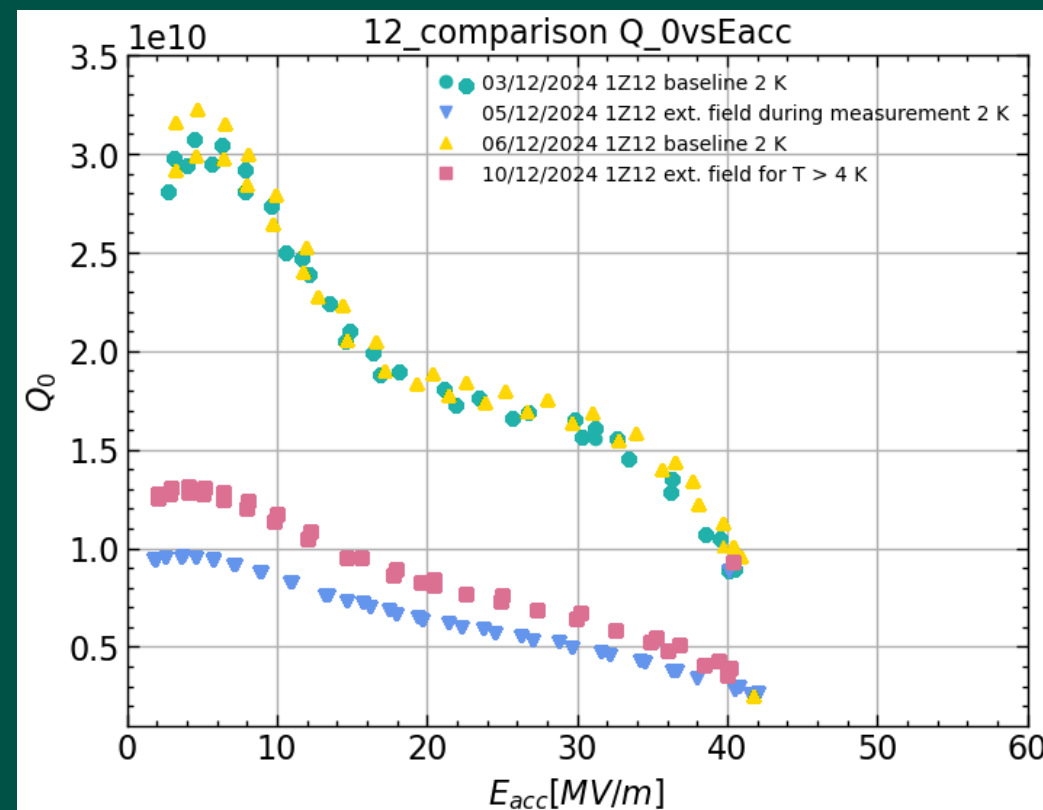


1st magnetic
field
measurement

10_12_2024_no external B_ext B for T higher 4K_2K_1D and 3D sensors comparison_z_axis_2



2nd magnetic
field
measurement



With B_{ext} : trapped magnetic field results in lower Q_0
because of disturbance of the Meissner effect
Without B_{ext} : higher performance of Meissner effect

Near-future Outlook



- Understanding data: differences in sensors, noise in data, validity of results
- Determining S from Q_0/E_{acc} measurements
- Comparison between XFEL-type and mid-T baked cavities

Further Resources!



- -Correlation of srf performance to oxygen diffusion length of medium temperature heat treated cavities*, C. Bate, et al. arXiv:2407.07779v1, 2024.
- -Further improvement of medium temperature heat treated srf cavities for high gradients*, L. Steder, et al. arXiv:2407.12570v1, 2024.
- -Impact of medium temperature heat treatment on flux trapping sensitivity in srf cavities*, P. Dhakal, et al. arXiv:2405.10085v1, 2024.
- -Impact of medium temperature heat treatments on the magnetic flux expulsion behavior of srf cavities*, J. C. Wolff, et al. 2023.
- -Rf superconductivity for accelerators, H. Padamsee, et al. (book)