

Warm Vacuum Systems

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Outline

- some basics on **accelerator vacuum**; discussion on XFEL vacuum level
- warm sections **overview** and issues
- RF gun; bunch compressor
- transport lines; beam distribution
- collimator unit; water cooled Ti insert
- **undulator vacuum system**:
 - choice of material, intersection; cavity BPM; spont. radiation; pressure profile
- summary

Beam Vacuum

usually UHV (Ultra High) Vacuum systems

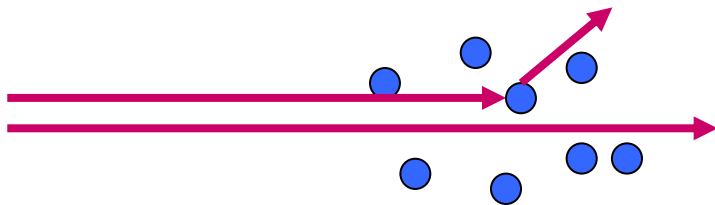
$P \sim 10^{-9}$ mbar; storage ring: beam lifetime \sim several 10h

standard air pressure 10^3 mbar \rightarrow 12 orders of magnitude!

extreme care has to be taken during production of components; no contaminations, oil etc.

in XFEL conditions somewhat relaxed because beam passes only once!

$P \sim 10^{-7}..10^{-6}$ mbar is acceptable in transport lines; close to cold cavities pressure should be better $\sim 10^{-9}$; particle free !



beam particles scatter at residual gas molecules \rightarrow loss of beam

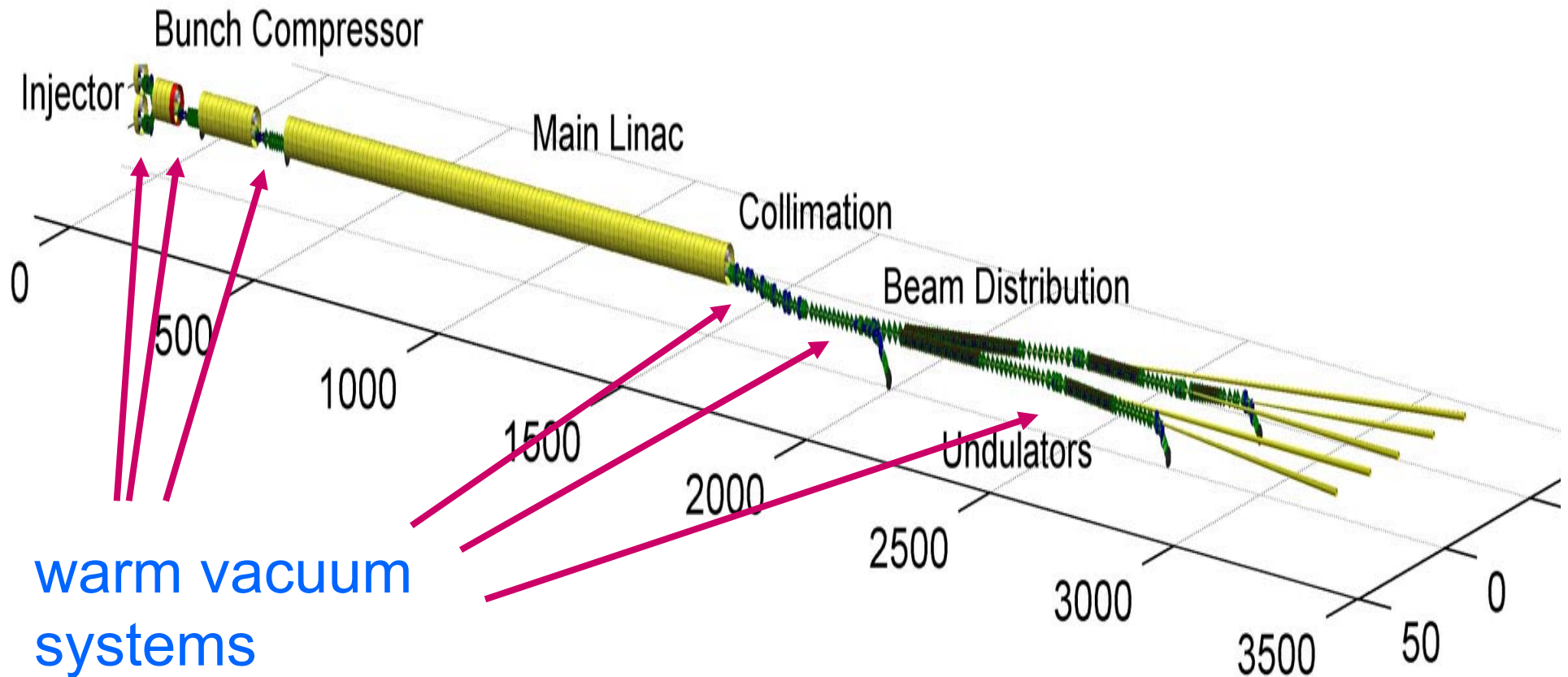
goal: loss/beam $\leq 10^{-9}$

$P_{\max} = 300\text{kW} \rightarrow P_{\text{loss}} < 0.3\text{mW}$

warm vacuum – materials, components

- chamber materials:
 - stainless steel (special chambers eg. bunch compressor)
 - copper (pipes in transport lines, absorbers)
 - extruded aluminum ? (undulator)
- pumps:
 - mobile turbo-pump units
 - ion getter pumps (appx 500units)
 - Ti sublimation pumps
- chamber supports, flange connections, diagnostics, tech. interlock systems, all metal valves...

Overview XFEL, Warm Sections

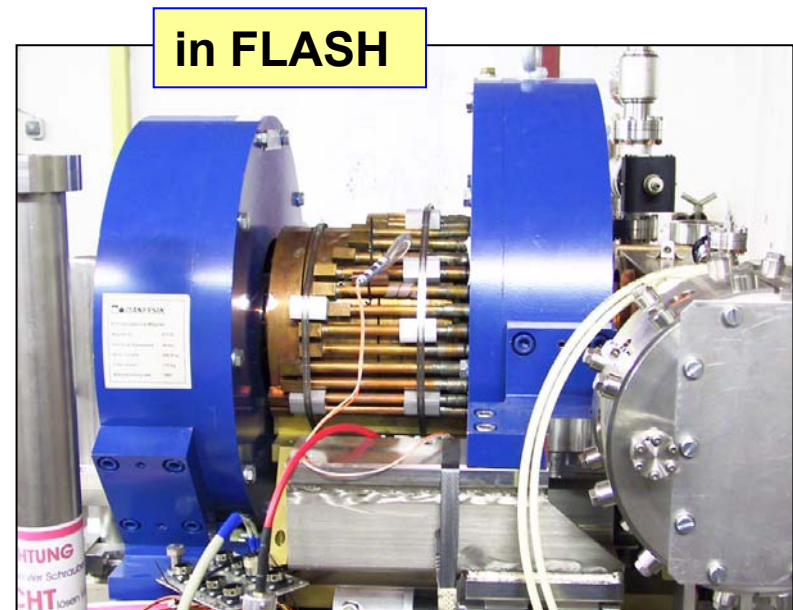
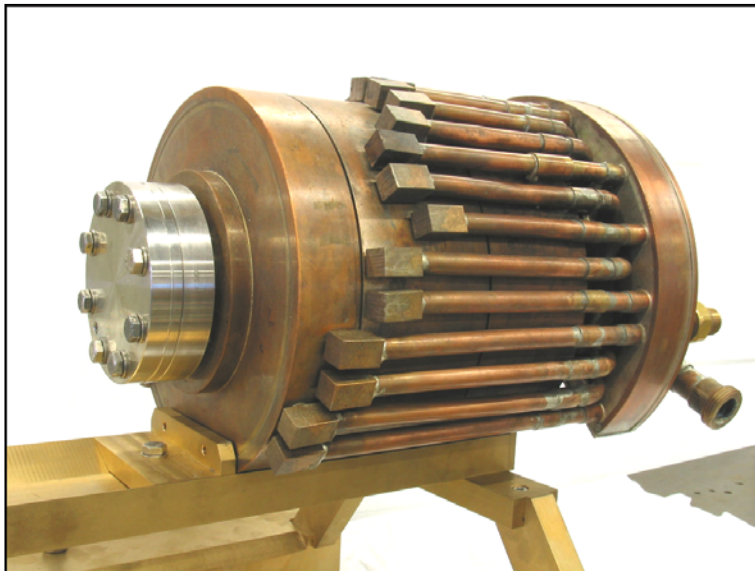


Categories of Sections/Components

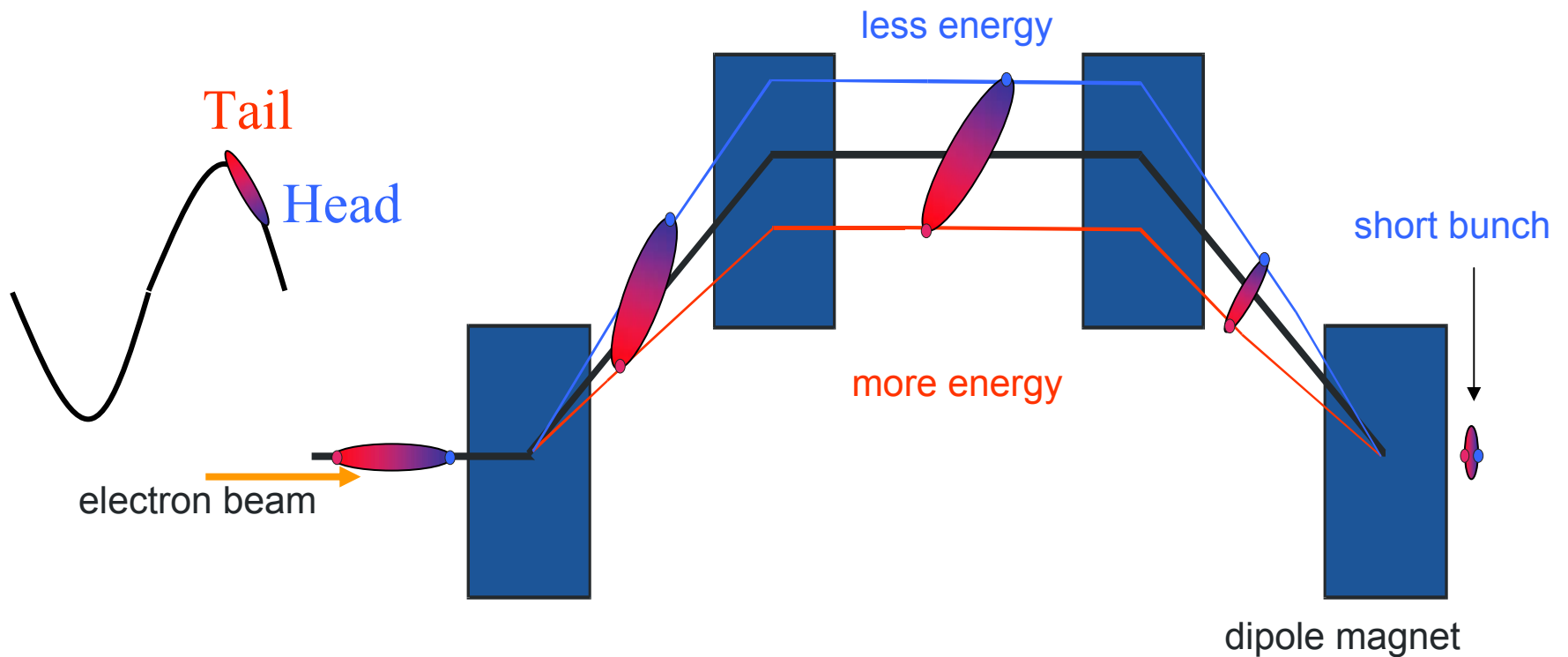
section	length	issues
injectors I,II	111,5m	RF-guns: continuous R&D program, particle free, high complexity (WP19, WP8)
compressors, diagnostic	160m	flat steel chambers, copper coating, narrow tolerances (WP19, WP8)
collimator section	209m	precision collimator units, material: Ti, complex diagnostic section
undulator chambers	713m	small aperture, low roughness, high conductivity
beam distribution	1.737m	optimized for cost, low complexity, copper pipes

RF Gun – Particle Source

- **high accelerating gradient** to counteract repelling space charge forces → **large heat dissipation**, good cooling essential to maintain dimensions!
- 1½ cell RF acc. structure, **brazing** in vacuum furnace
- cathode specially prepared, eg. Cs₂Te for low electron work-function; needs **constantly low pressure ~10⁻¹⁰mbar** to maintain properties



Bunch Compressor Section

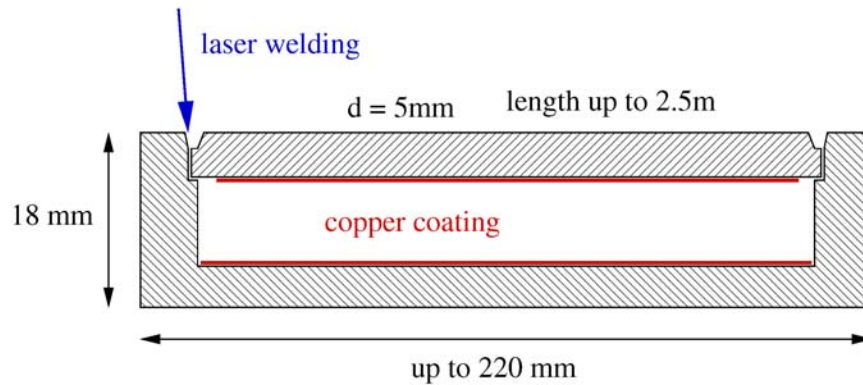


desired: varying compression ratio via varying bump strength/amplitude

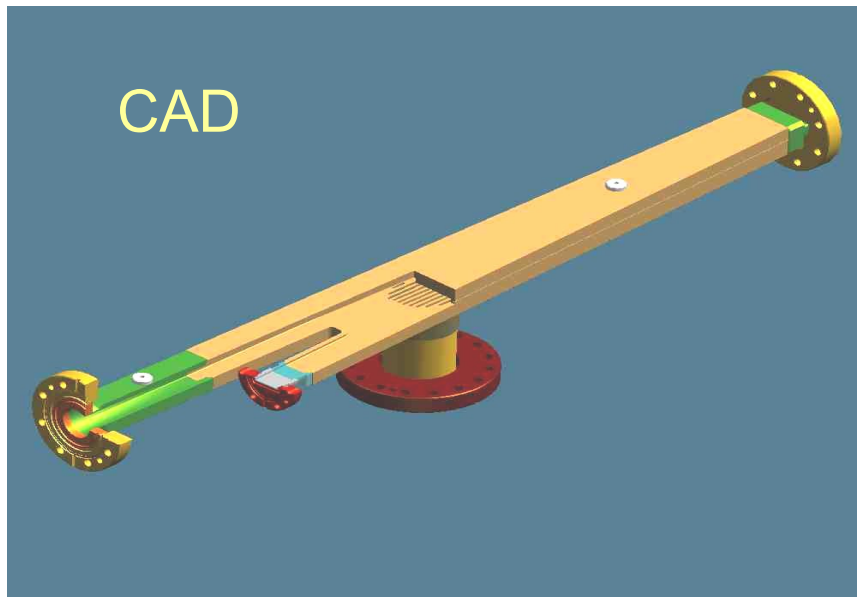
→ vacuum chamber: flat and wide aperture!

Compressor Chambers

- from steel sheets, laser beam welded, small μ_r
- particle free prepration (close to cold cavities)
- many diagnostics ports for beam monitoring, SR observation

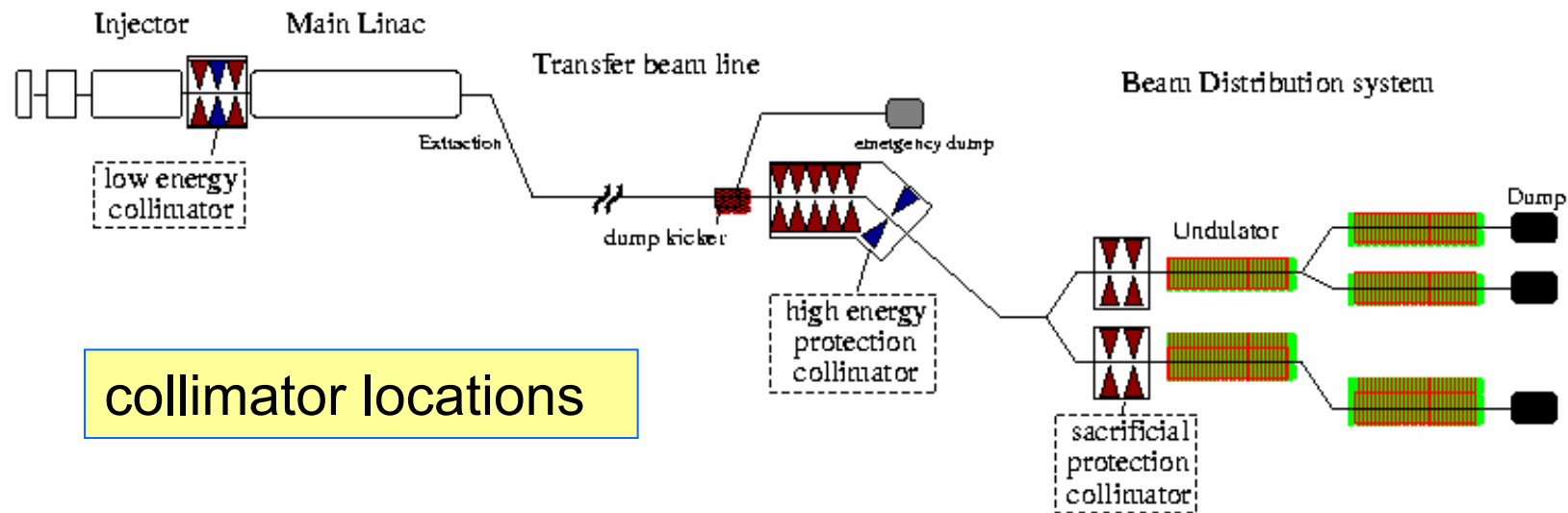


stainless s. copper coated;
5mm wall; large width;
straightness critical!



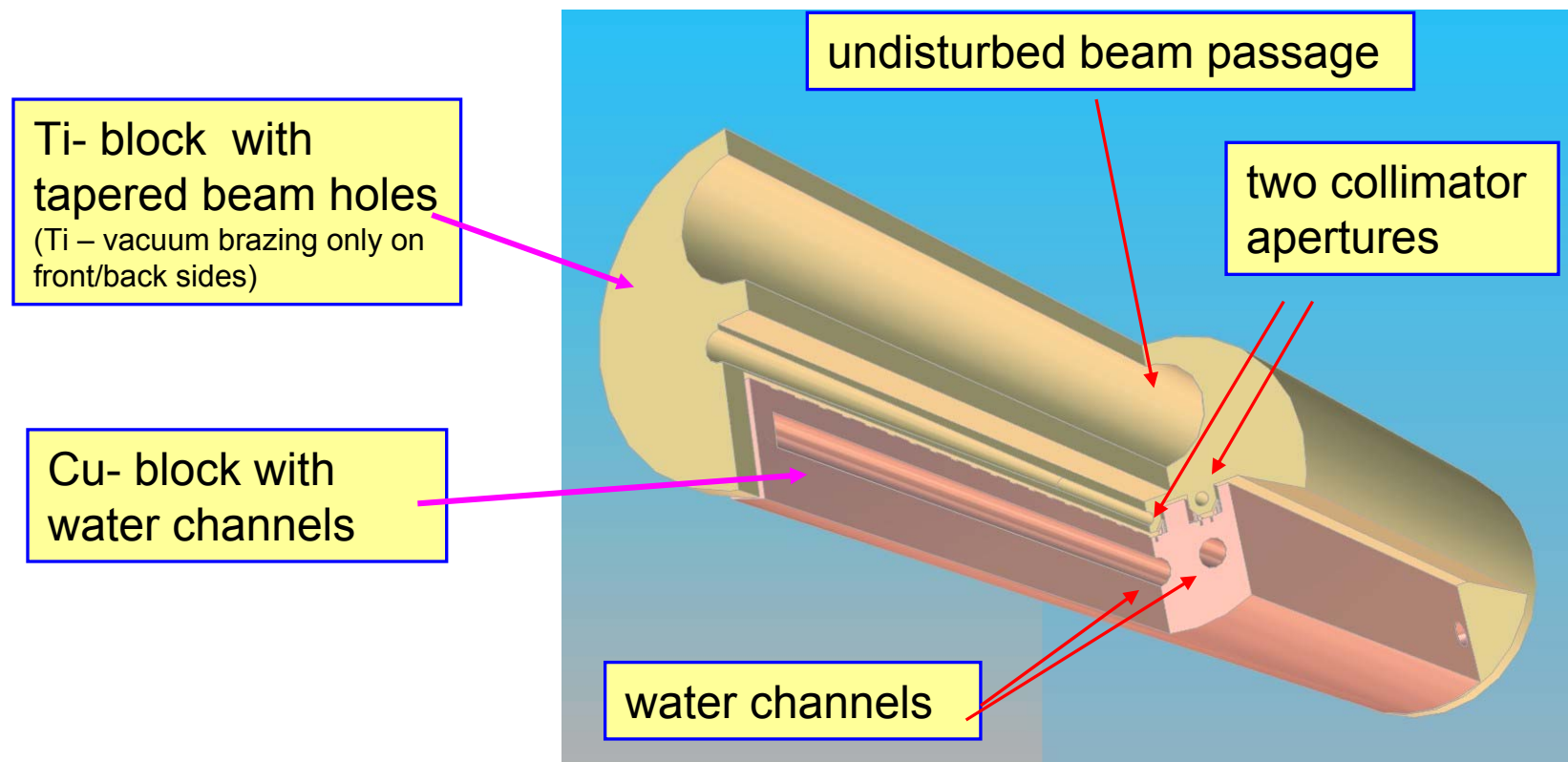
Collimation System

- purpose: avoid direct beam hits (mis-steered) or loss (halo) in the undulator (radiation may demagnetize permanent magnets)
- remove dark-current generated in cavities
- collimator should withstand beam hit for few bunches; made from Ti



Collimator Block - Titanium Insert

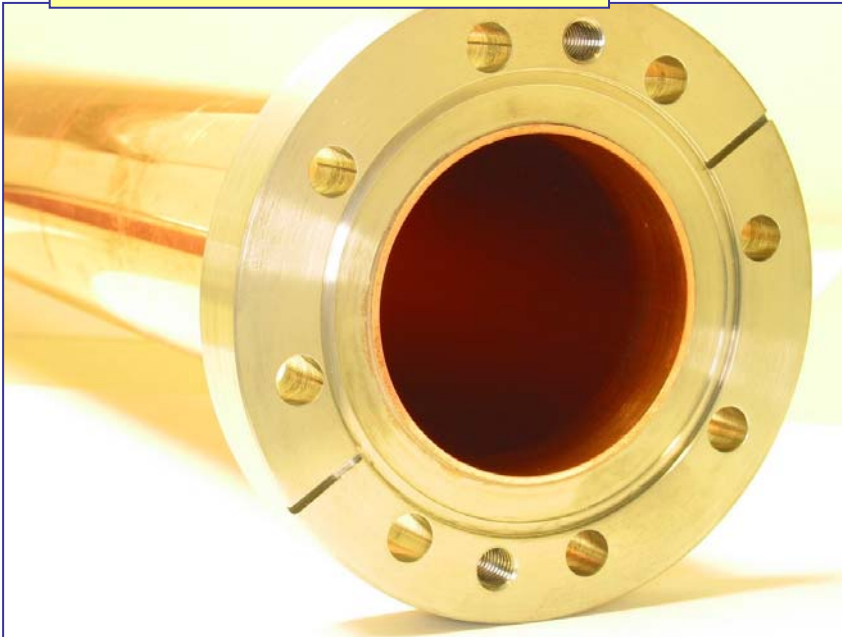
- **Collimator Units** ensure that mis-steered beam or dark-current cannot hit undulator magnets
- choose Ti for high stress resistance in case of mis-steered beam hit
concept: three interchangeable apertures (holes)
- Ti insert with brazing connection to water cooled Cu block (continuous loss of dark current possible); need to test brazing



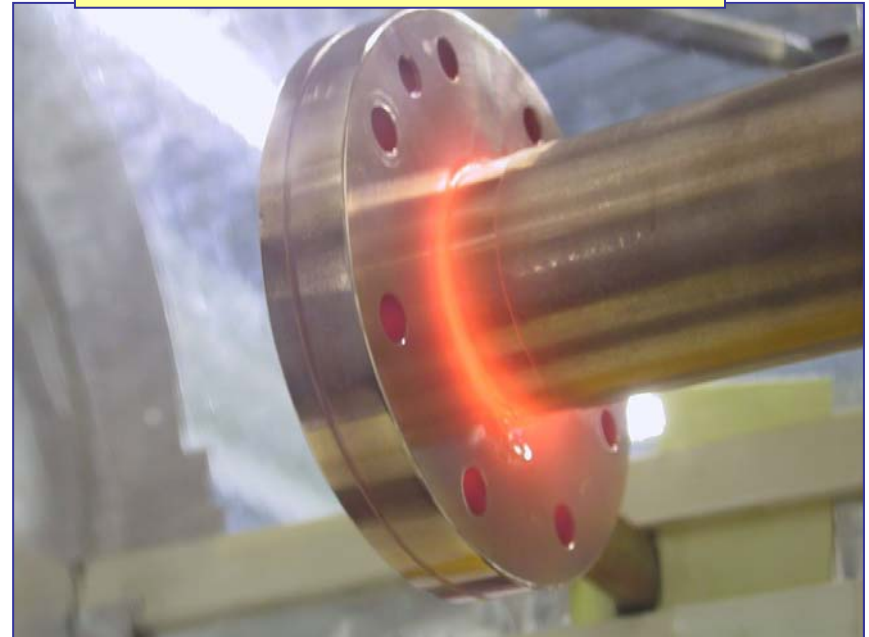
Beam Distribution System

- length 1.7km; optimized for cost; ID 50mm circular pipes;
- high electrical conductivity required; material copper; brazing connection to CONFLAT flanges
- ion getter pumps (60l/s) every ~6m; est. pressure $5 \cdot 10^{-9}$ mbar
- issue: cleaning of the chambers and keeping oxidation at a minimum

Cu pipe with CF flange



inductive brazing of flange



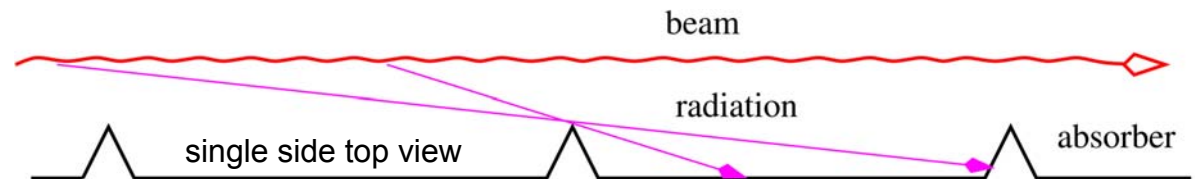
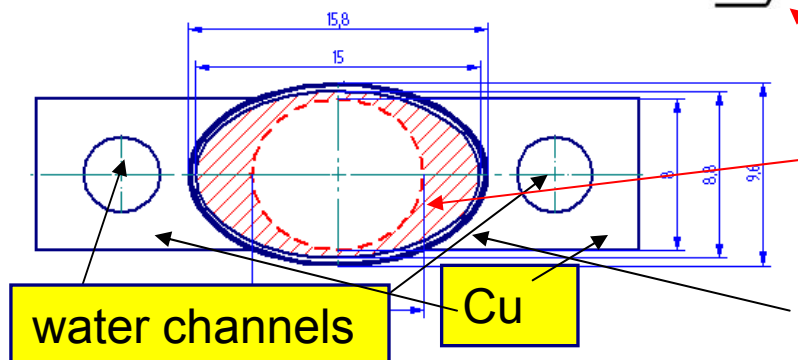
Undulator Section Vacuum System

- each undulator section contains ~40 undulator units (5m) and 40 intersections (1.1m); length ~240m; 3 sections planned
- spontaneous X-ray radiation amounts to maximally 8W/m; absorbers needed!
- small aperture chamber (~9mm inner height) to allow for small magnet gaps → high field strength
- high conductivity; small roughness!
- small aperture leads to poor vacuum conductivity and rel. high pressure
- intersection (1.1m) with bellows unit, radiation absorber, cavity BPM, phase shifter (chicane to vary beam path length on nm scale), quadrupole
- for chamber two possible solutions under study: elliptical steel chamber or extruded Al profile

radiation parameters/geometry

	parameters (example)
beam/undulator	$E=20\text{GeV}$, $B_{\text{max}}=1.3\text{T}$, $\lambda_u=48\text{mm}$, $K=6$
spontaneous radiation	typ. opening angle: $\theta_x=150\mu\text{m}$, $\theta_y=25\mu\text{m}$ shadow angle: $\psi_x=500\mu\text{rad}$, $\psi_y=75\mu\text{rad}$
radiation power	$P'=6.5\text{W/m}$ on absorbers (LCLS: 22mW/m)
HOM Power:	$P'=2\text{W/m}$, unavoidable, with air cooling $\Delta T \approx 6^\circ\text{C}$!

option with steel tube shown; alternative: Al profile



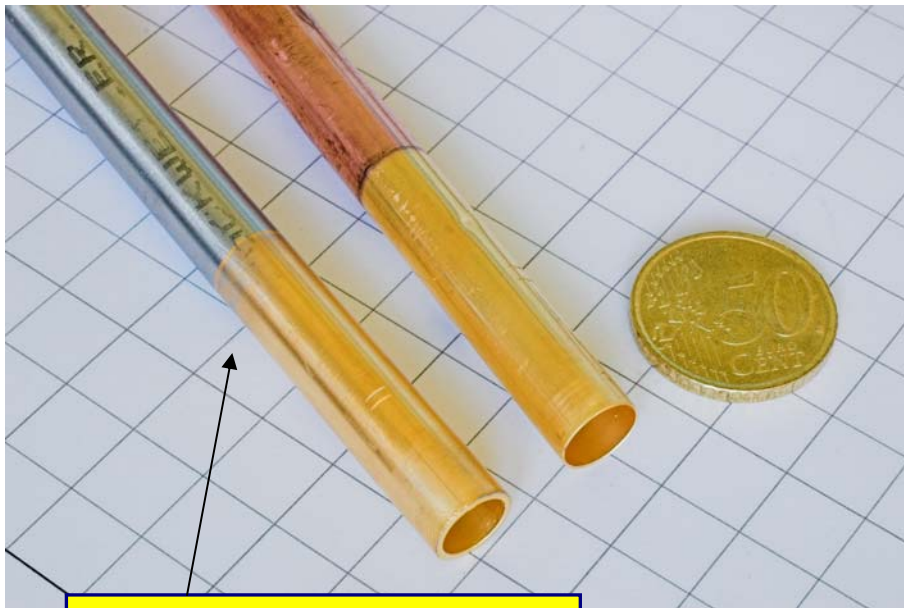
absorber every 6.1m

elliptical steel (?)
tube 15x8.8mm² ID

at large angles
radiation still
hits pipe

Options for Undulator Chamber Material

- steel tube – difficult to find manufacturer; formed to elliptical shape, brazing connection (tolerances!) to water channel; μ_r critical!
- Al tube – easier to make; integrated water channel; presumably higher roughness; tolerances critical for wall thickness; larger photon desorpt.
- optimization of coating/oxide layer in collaboration with swedish colleagues; vacuum quality of coating?

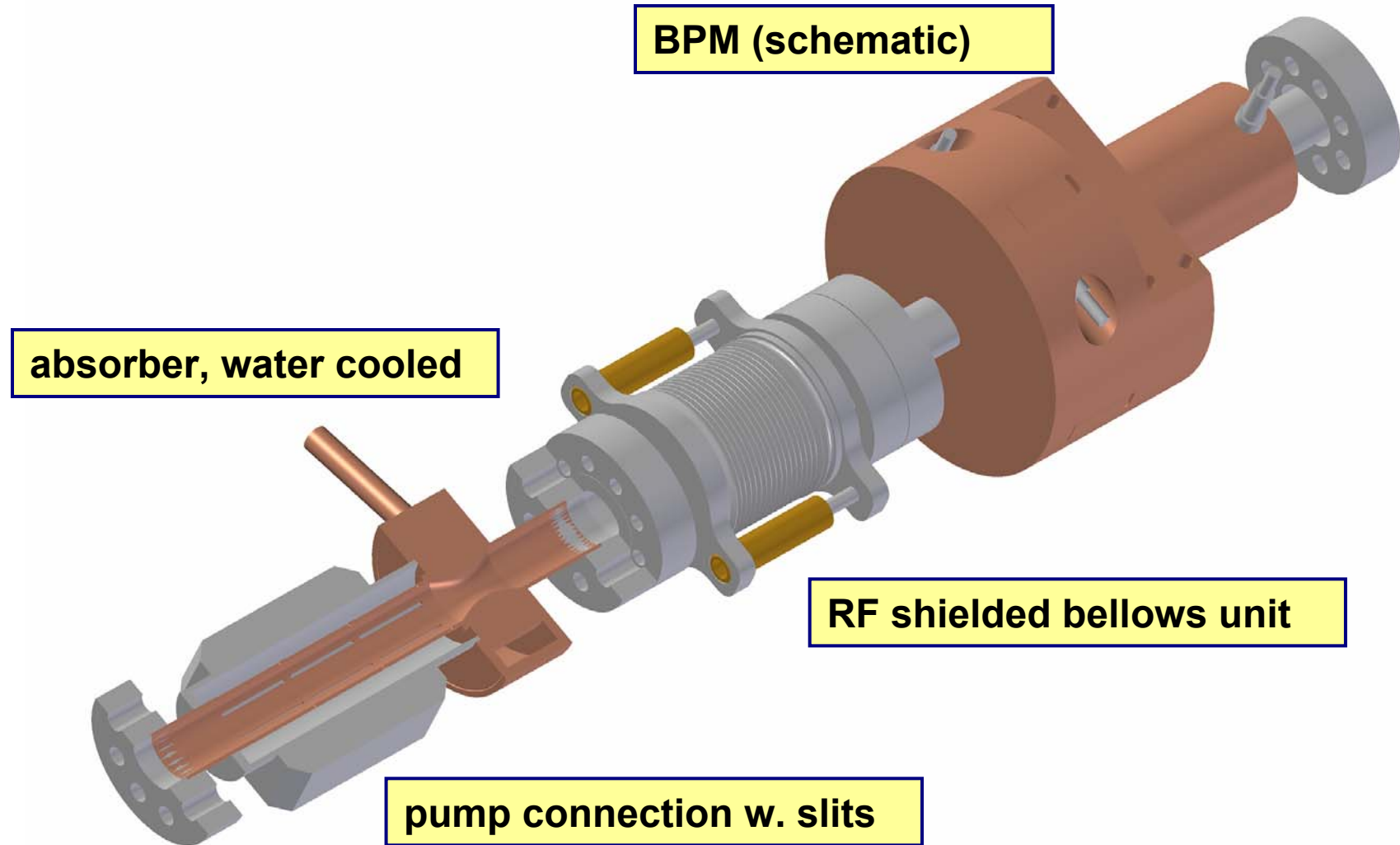


steel tube, test sample, gold plated

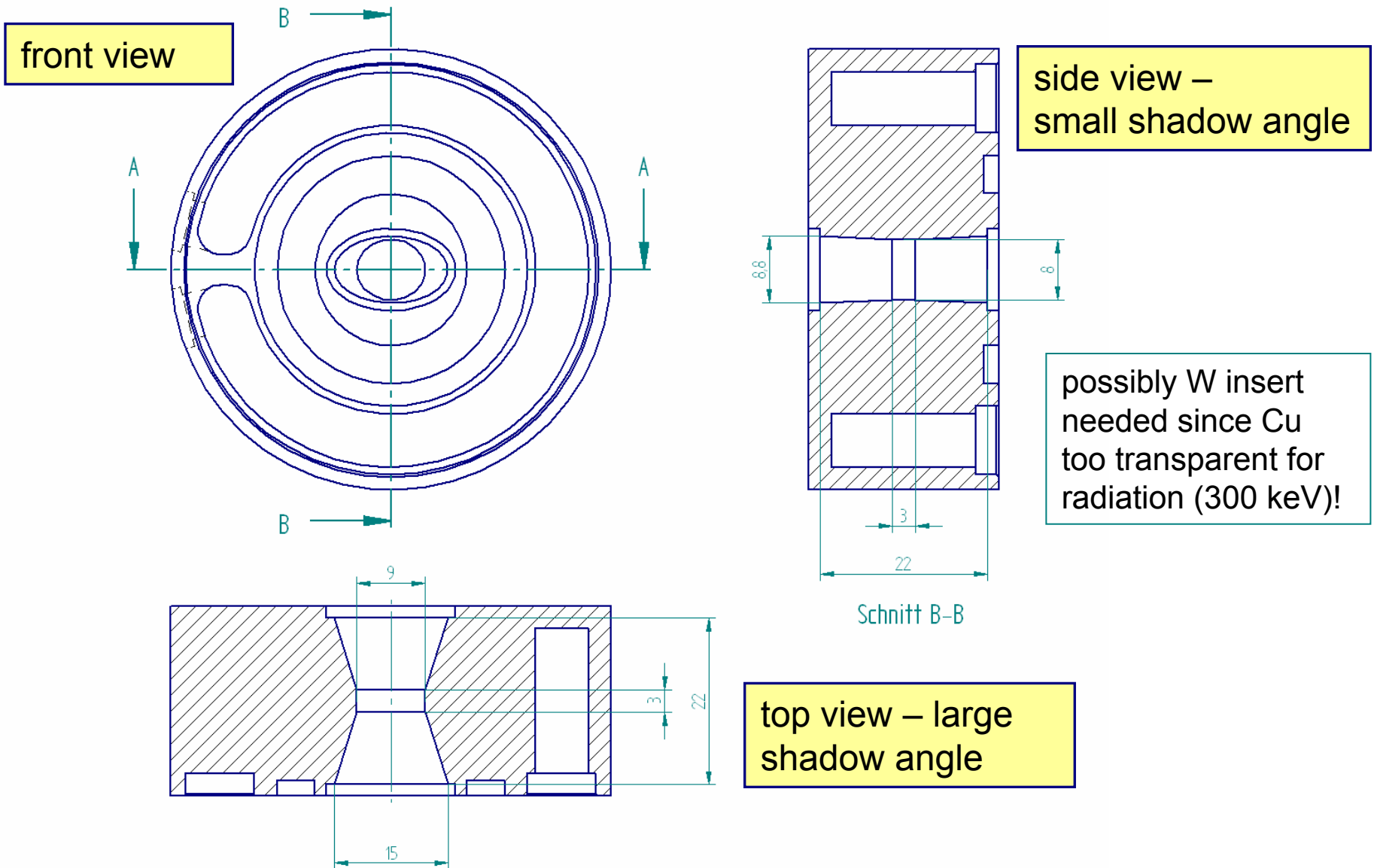


Al profile, test sample, integrated cooling

intersection between undulators – major components



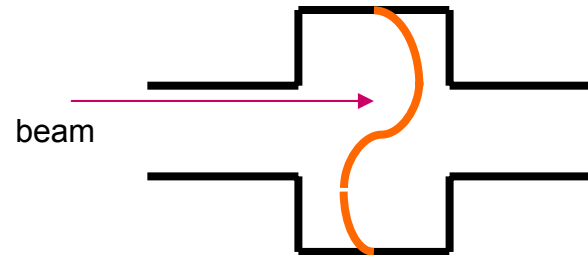
layout of tapered absorber



Cavity BPM

principle:

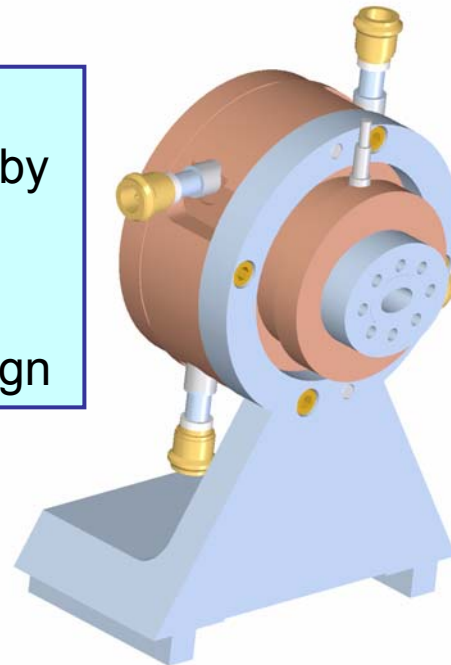
offset beam excites dipole mode; strength of signal is prop. to beam offset



- cavity → stronger signal, more precise than buttons
- frequency $\sim 4..5\text{GHz}$; possibly not multiple of 1.3GHz because of dark current

principle design and machining proposal by T.Wohlenberg

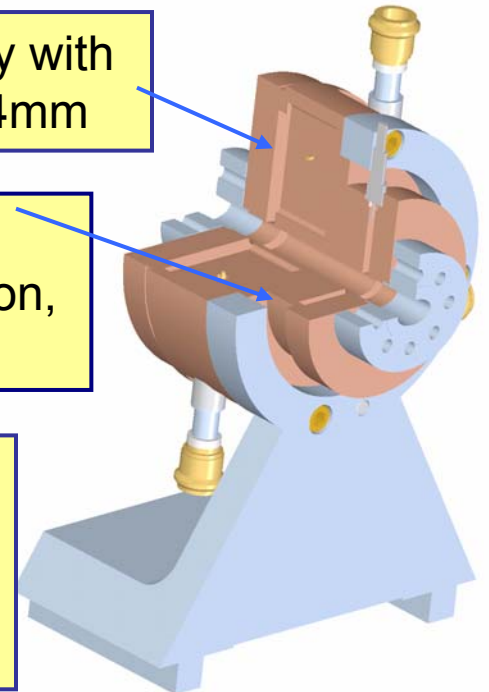
ideas taken from NLC/ILC/SSCS design



TM011 Cavity with couplers, $h=4\text{mm}$

TM010 cavity for charge normalization, phase reference

exact dimensions to be determined;
outer diameter $\sim 110\text{mm}$ @ 4GHz

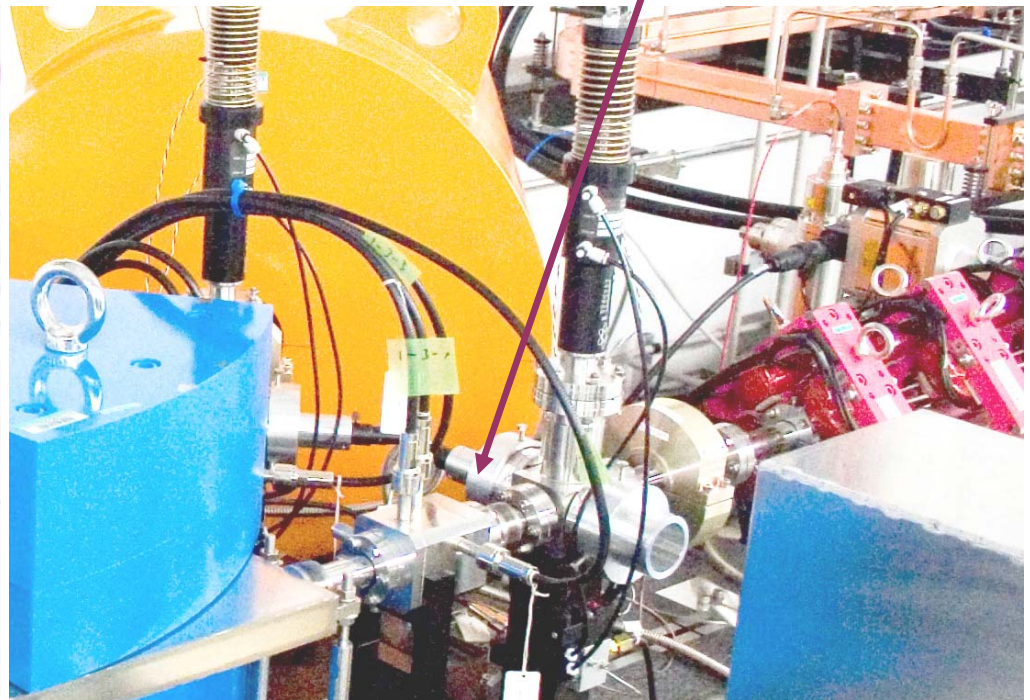
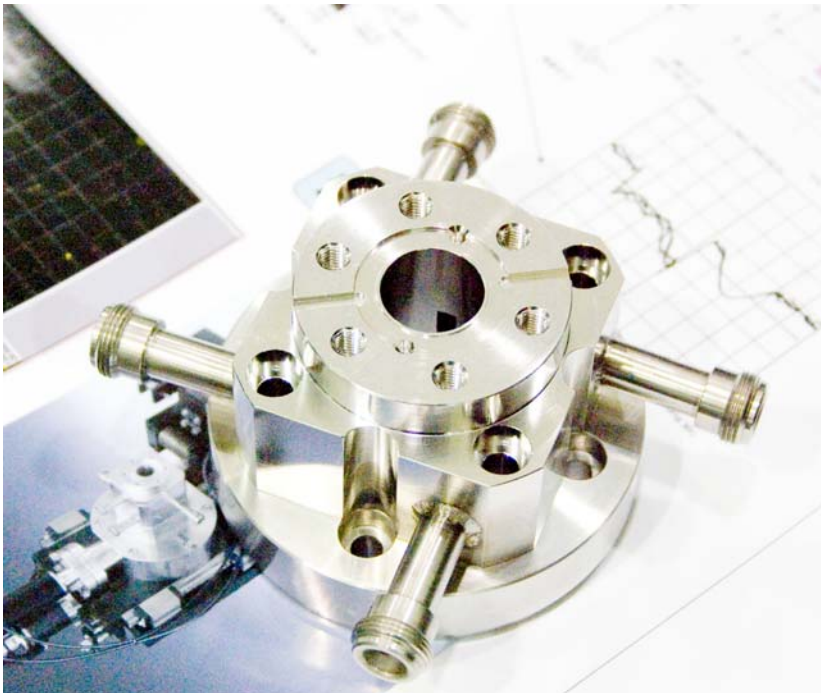


Cavity BPM – SPRING8(SCSS) Design

- TM011 cavity at 4.76GHz, brazed stainless steel, $Q \sim 130$
- integrated TM010 cavity as charge monitor, ext. phase reference!
- much emphasize on ADC – 11Bit at 238MHz (spring8 internal development!?), anticipated res. $< 1\mu\text{m}$

→ **good prototype for us !**

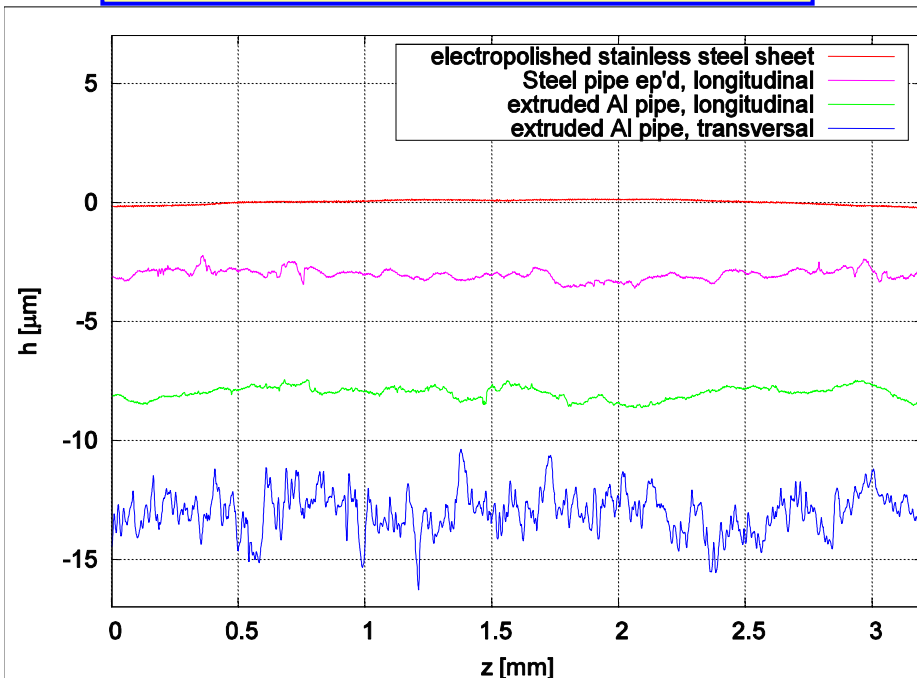
in beamline, with
reference cavity



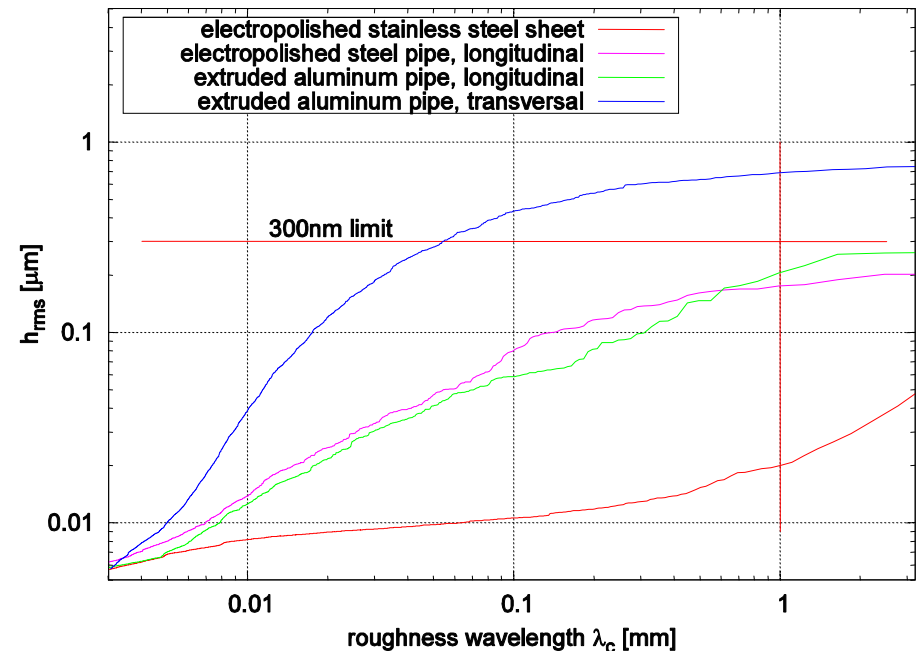
Mechanical Properties of Vacuum Pipe in Undulator

- thin oxide layer (dielectric) Al: 5nm, Cu: 1nm, Au:?
- roughness rms<300nm@1mm wavelength
- high el. conductivity, low outgassing, thin wall, water cooling

surface profiles of materials



integrated power spectrum of profiles



Overview Wakefield-Effects

unavoidable: resistive wakes from narrow pipe → sets the scale for other effects

rms energy spread from l.wake:

M.Dohlus

I. Zagorodnov:

resistiv (Al):

49.5 V/pC m

geometric

absorber

16 V/pC

bellows unit

5 V/pC

flange gap

2.4 V/pC

long pumping slit

<0.2 V/pC

oxid layer

Cu 1nm

1.1 V/pC m

Al 5nm

5.7 V/pC m

roughness

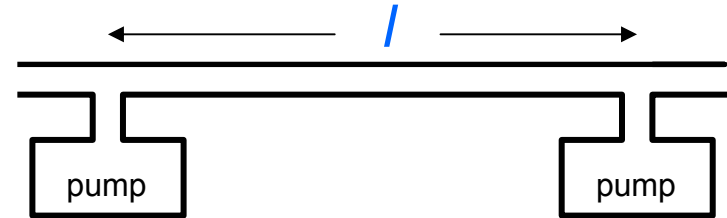
Al 600nm(!)

9 V/pC m

→ oxide layer is rel. important; above quoted numbers ambitious, consider Au coating → collaboration with Swedish university, Lars Westeberg

conductance limited vacuum system

- pumps at a distance of $l=6.1\text{m}$
- small pipe is conductance limited;



$$\text{conductance} = \frac{\text{amount of gas (moles or molecules)}}{\text{time} \cdot \text{pressure difference}} \quad [\text{mbar l} / \text{mbar s}]$$

gas equation $pV = nRT \rightarrow [\text{mbar l}]$ is a measure for the amount of gas!

is constant (293K)

conductance $\sim d^3 \rightarrow$ strong scaling with pipe dimensions

average
pressure

$$P_{avg} = Aq \left(\frac{l^2}{12c} + \frac{l}{S} \right)$$

Aq – outgassing; thermal but mainly photon radiation

l – length, pump distance

c – conductance

S – pumping speed

term remains/dominates, even for $S \rightarrow \infty$

pressure simulation with photodesorption

- this system is extremely conductance limited ($c = 0.125 \text{ l m / s}$)
- expected average pressure $\approx 7 \cdot 10^{-7} \text{ mbar}$ (Al), $\approx 10^{-7} \text{ mbar}$ (SS)
- vacuum will improve from conditioning!

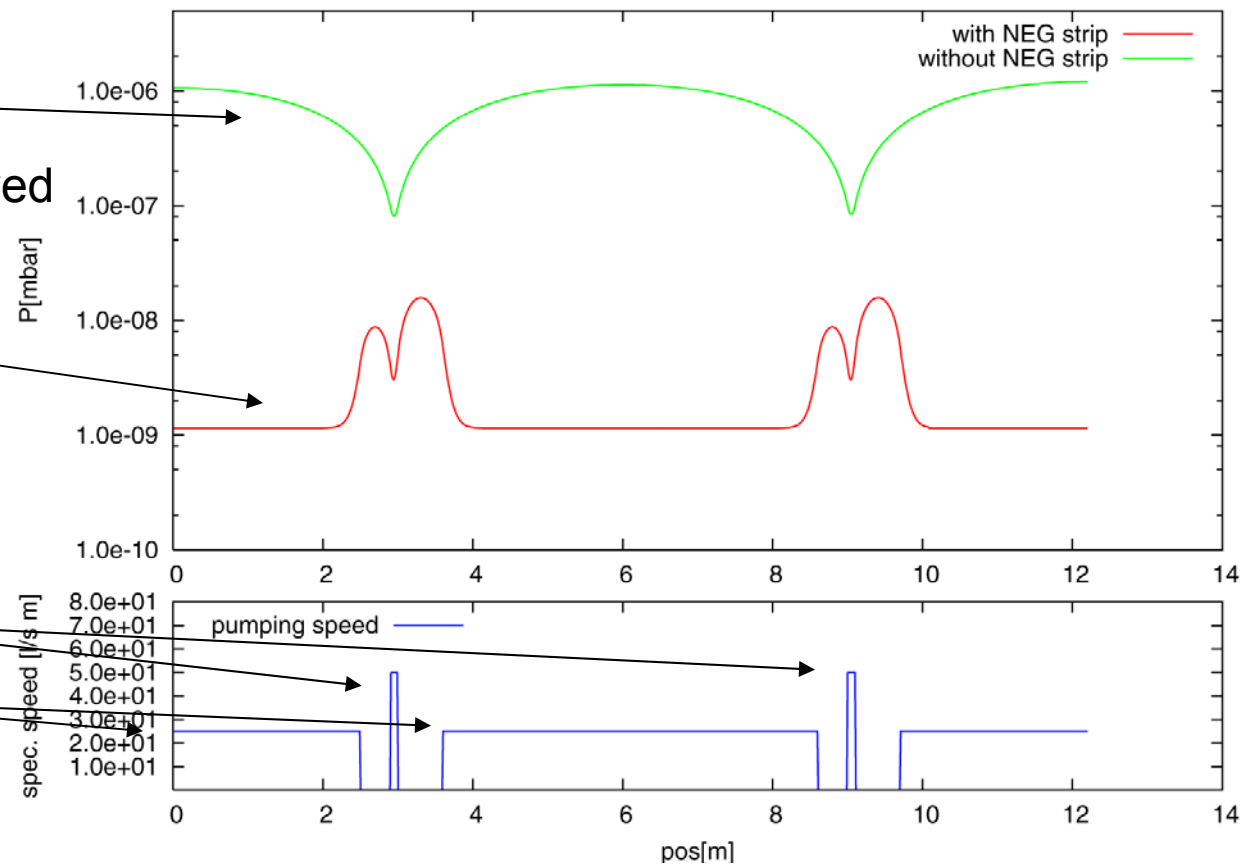
with lumped pumps as
planned, Al pipe
(full 300kW beam, improved
by $\times 2$ after 60 days)

with NEG pump
(not needed)

pumping speed per m

lumped pump

NEG strip



Status and Summary

- presently “cataloging” of all vacuum sections completed; **detailed cost and manpower estimate available**
- **technologically difficult** sections: undulator/collimator are under work to develop strategy (issues: tolerances, roughness, oxide layer, brazing exotic mat. combinations)
- **technically complicated** sections: bunch compressor flat chambers with tight tolerances; particle free preparation
- other sections standard technology – Cu pipes; ion getter pumps etc.; although **large quantity**