

L6 preparation status and plans

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Outline

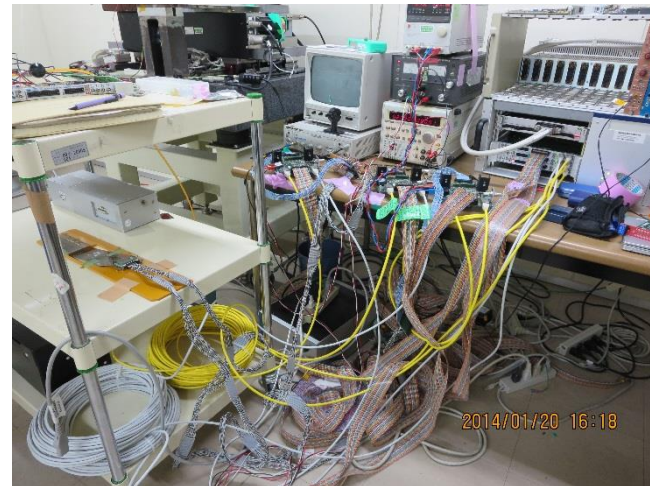
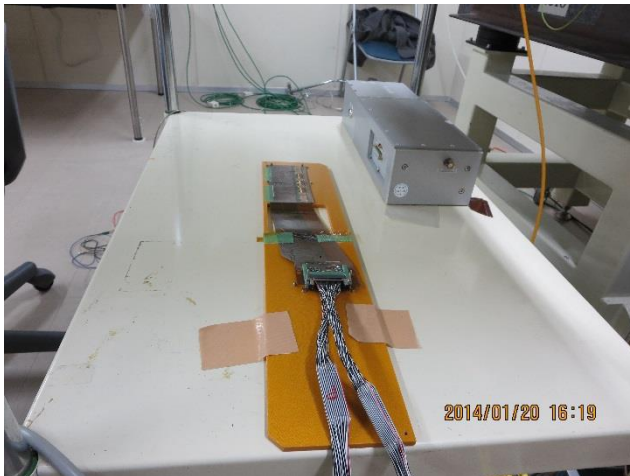
- **Electrical QA/QE** (Junya Sasaki, University of Tokyo)
- **Mechanical QA/QE** (Nobuhiro Shimizu, Takeo Higuchi, University of Tokyo, Kavli IPMU)
- **Ladder production jigs** (Yoshiyuki Onuki, University of Tokyo)
- **Wire bonding** (Tomoko Iwashita, Kavli IPMU)
- **Glue dispensing study** (Yoshiaki Seino, Niigata University)
- **Pre-bending of Origami+z** (Tomoko Iwashita&Nobuhiro Sato&Takeo Higuchi)
- **Plan**

Electrical QA/QE

Motivation:

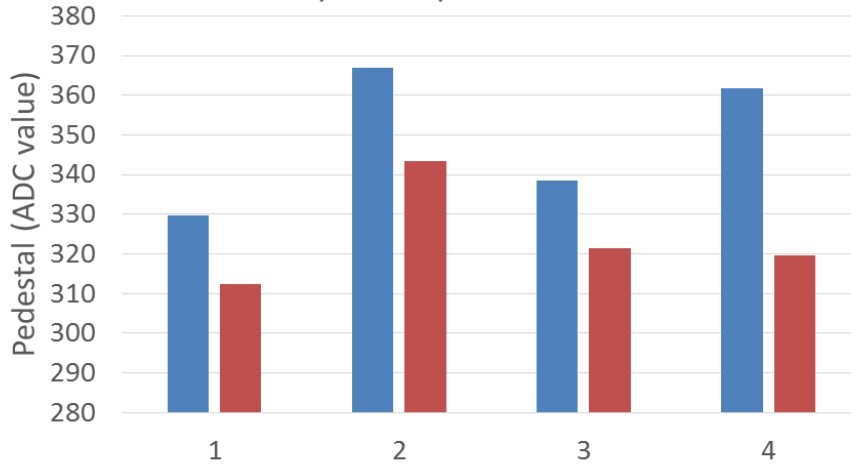
Electrical connection assurance between DSSD-APV25 with comparison before and after the wire-bonding.

- Origami module assembled in autumn 2011(after bonding. w/ DSSD)
- Origami +z implemented APV25(before bonding. w/o DSSD)
- APVDAQ system at KEK.
 - Measurement of Test pulse height, Noise and Pedestal w/ and w/o DSSD.

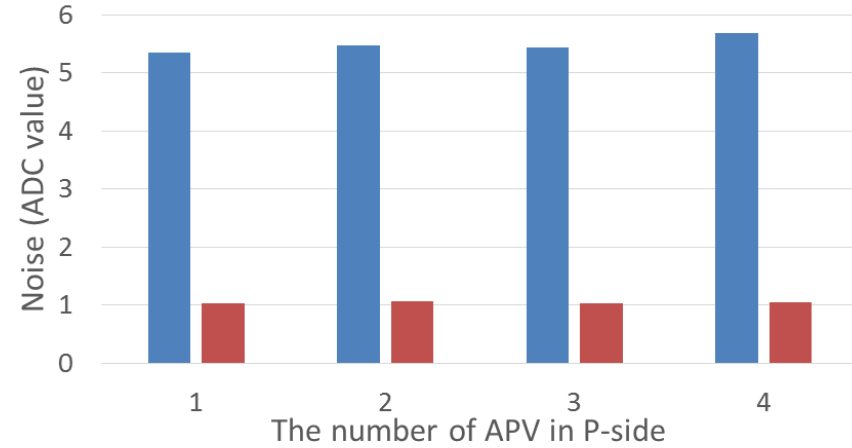


Readout test result

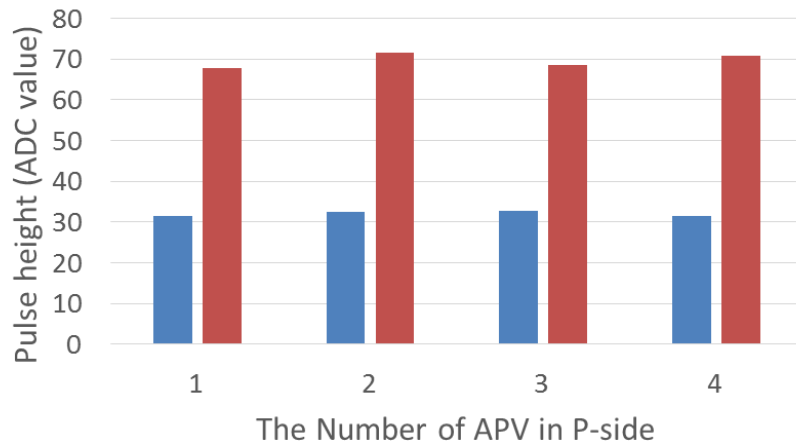
Pedestal for each channels in P-side
w/ and w/o DSSD



Noise average for each channels
w/ and w/o DSSD in P-side



Pulse height average for each channels
w/ and w/o DSSD in P-side



■ w/ DSSD ■ w/o DSSD

Pulse Height	LOW	HIGH
Noise	HIGH	LOW
Pedestal	HIGH	LOW

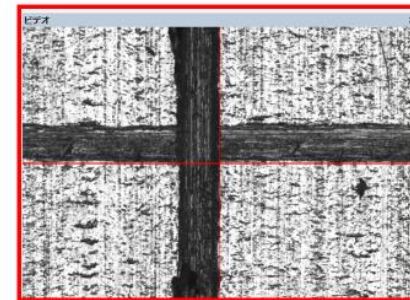
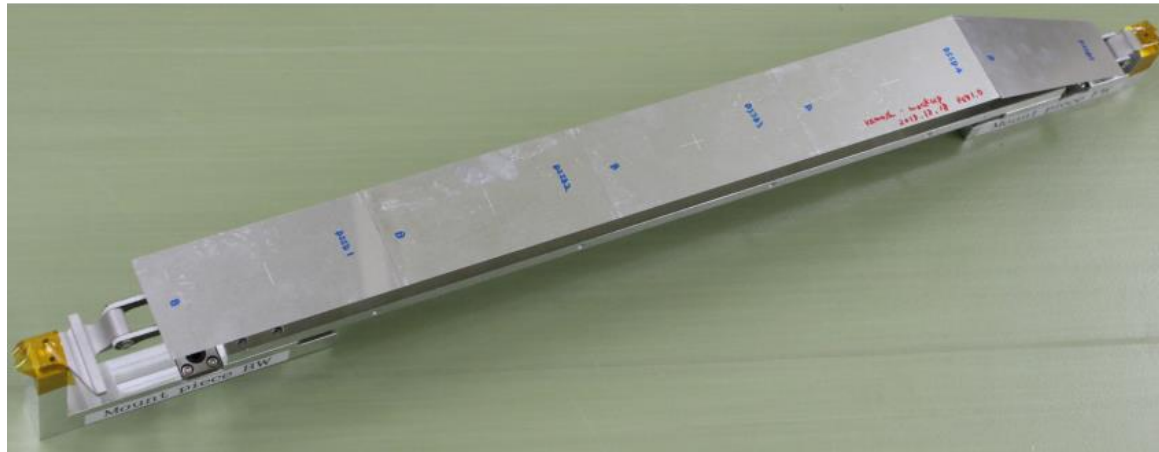
These information can be used for
electrical connection assurance
of bonding wire between APV25 and DSSD

Mechanical QA/QC

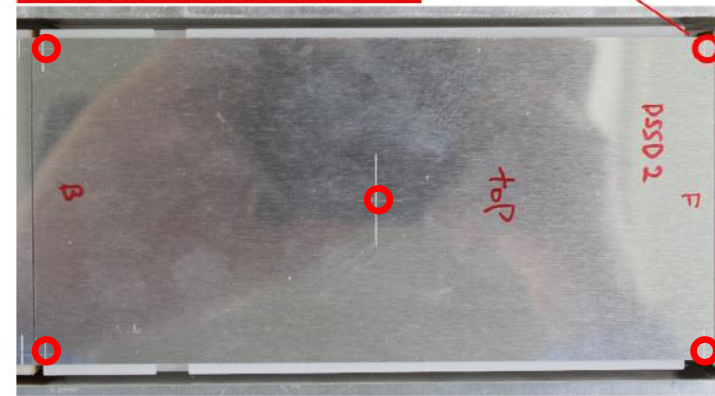
Motivation:

DSSD alignment measurements in the assembly and after the assembly to understand which procedure affect the precision critically.

- DSSD: Al-plates w/ scratched alignment marks.
- Ribs and MBs: rev0
- No Kokeshi-pins
- No FLEXes

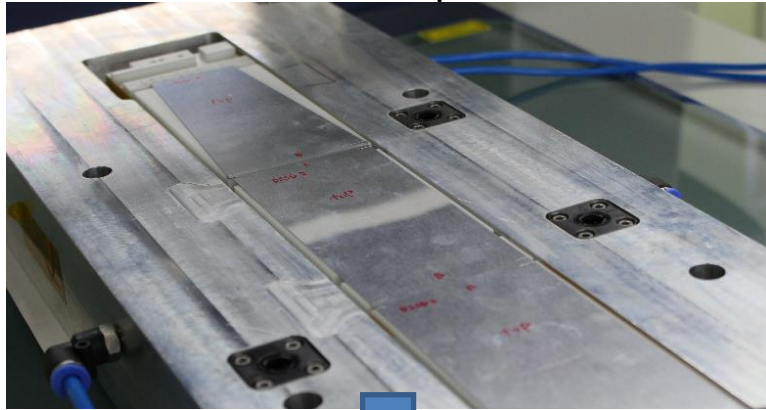


Scratched cross hair
substitute for the
alignment mark

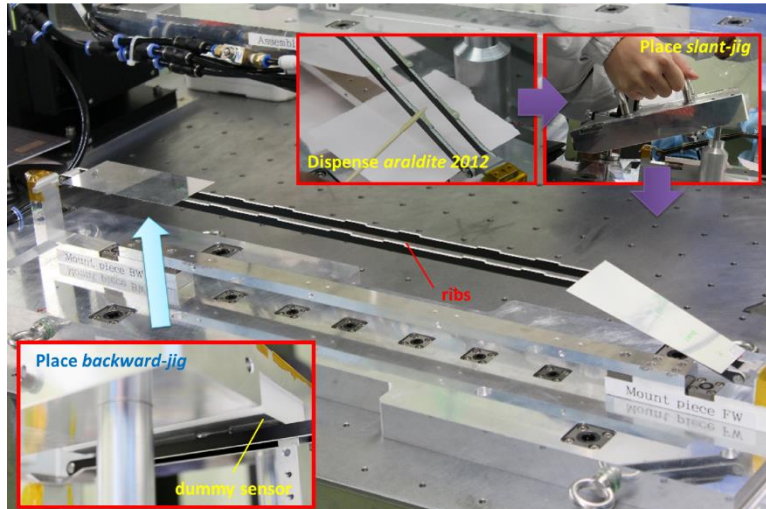


Mech.QA in mockup assembly

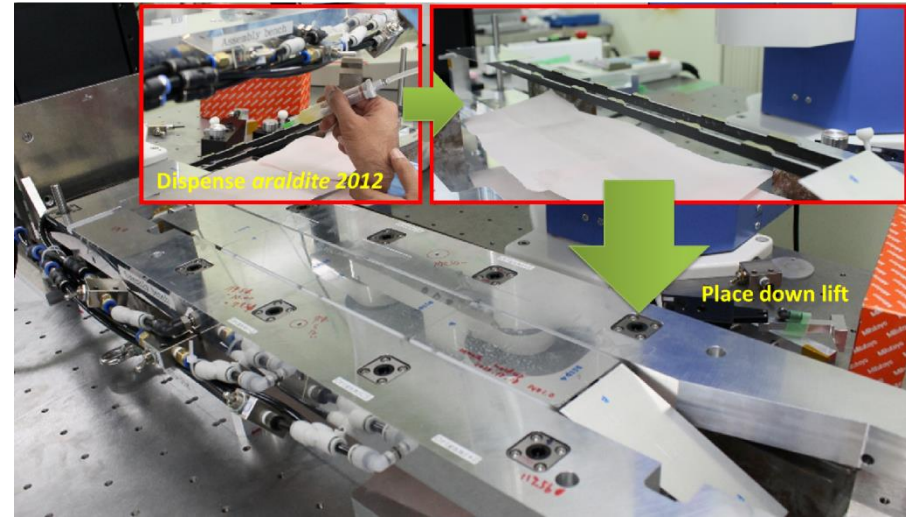
1) **DSSD position measurement** after placing 5 DSSDs on the flat plane.



2) Gluing FW and BW DSSD on the ribs



3) Gluing Origami DSSD on the ribs



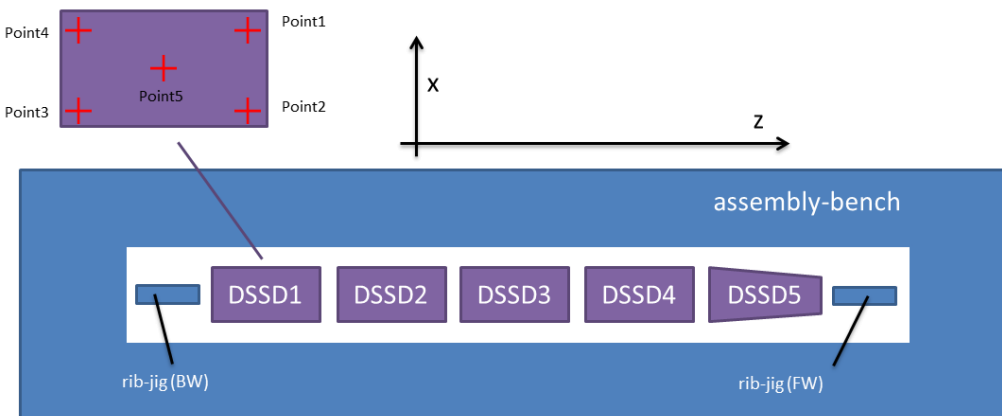
4) **DSSD position measurement** again



Mech. QA result

Point	Δx (μm)	Δz (μm)	Point	Δx (μm)	Δz (μm)
DSSD1			DSSD3		
$\Delta\theta^* = (5.9 \pm 0.08) \times 10^{-3}$ (rad)			$\Delta\theta^* = (-4.8 \pm 0.8) \times 10^{-4}$ (rad)		
$\Delta x = -211 \mu\text{m}, \Delta z = -21 \mu\text{m}$			$\Delta x = -77 \mu\text{m}, \Delta z = 127 \mu\text{m}$		
1	-160	-47	1	-80	126
2	-156	7	2	-81	119
3	-267	6	3	-70	123
4	-269	-45	4	-66	126
5	-211	-21	5	-77	127
DSSD2			DSSD4		
$\Delta\theta^* = (-4.8 \pm 0.8) \times 10^{-4}$ (rad)			$\Delta\theta^* = (-5.3 \pm 0.8) \times 10^{-4}$ (rad)		
$\Delta x = -64 \mu\text{m}, \Delta z = 131 \mu\text{m}$			$\Delta x = -86 \mu\text{m}, \Delta z = 126 \mu\text{m}$		
1	-64	131	1	-91	126
2	-68	127	2	-92	122
3	-58	126	3	-80	120
4	-57	129	4	-83	126
5	-64	131	5	-86	126

- Feedback from Mechanical QA to assembly procedure was established in principle.
- The $\Delta x, \Delta z$ shows the difference of DSSD position between 1) and 4) in previous slide.
- O(100 μm) shifts observed. DSSD2-4 shows same shift and rotation tendency.
 - Loose diameter tolerance of linear bush shaft (max. $\sim 60\mu\text{m}$)
 - Movement caused by transfer of DSSD from jig to jig (max. $\sim 10\mu\text{m}$)
 - Movement of MBs. In this assembly, MBs fixed by kapton tape instead of Kokeshi-pin. Same effect as shown [the slide](#) might be happen.
- Anyway, we need further mockup study.



Ladder production jigs

Feedback from mockup ladder QA result by Shimizu:

“BW module and three Origami DSSDs have different trans/rotation behavior.”

→(I am doubting) 2 possible sources of trans/rotation movement might be happen during the assembly in

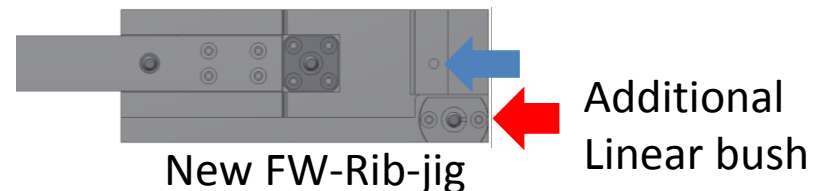
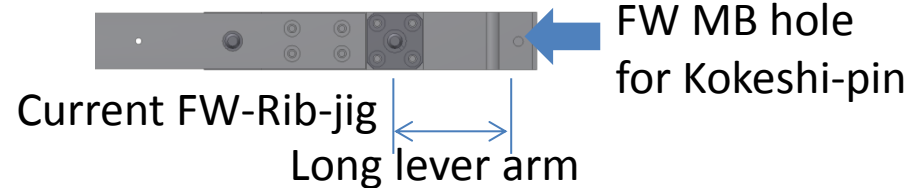
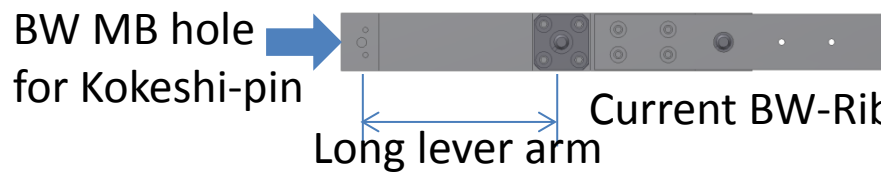
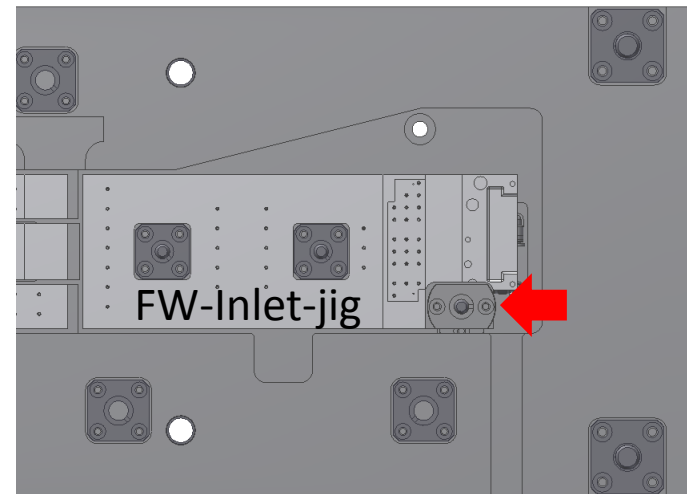
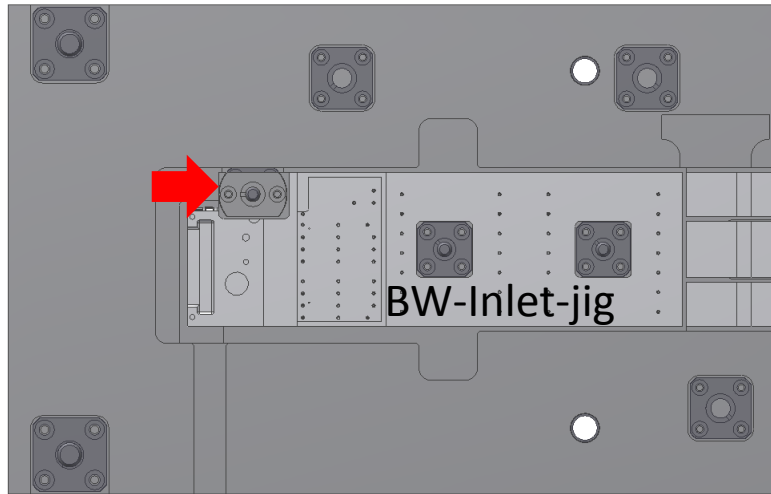
- Backward module assembly procedure.
 - Poor diameter tolerance of shaft pin (Pointed out by Shimizu).
 - **BW Inlet-jig** and **Backward-jig** (it may be same situation in FW module)
- Gluing Origami modules on the ribs procedure.
 - Poor diameter tolerance of shaft pin (Pointed out by Shimizu).
 - Rib distortion from MB rotation (Pointed out by Shimizu)
 - **Rib-jig** and Assembly-bench. Especially Rib-jig.

BW(FW) Inlet-jigs and Backward-jig and Rib-jig will be revised.

According to the revise of Inlet-jigs, **Basement-jig** also will be revised.

I'll release jigs and procedures with revised jigs at up coming B2GM Feb.

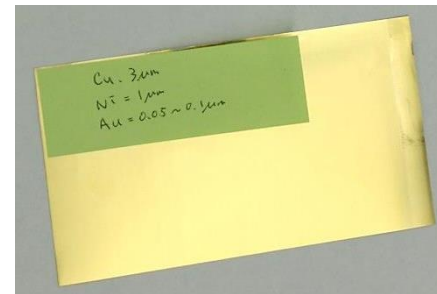
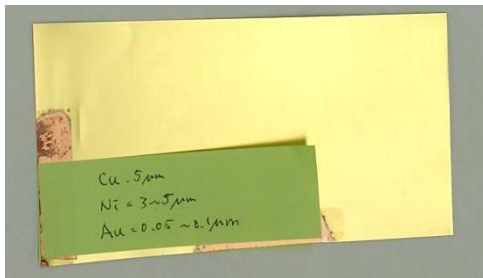
Improvement of Inlet-jig and Rib-jig



Lever arms between MB hole and next linear bush will be decreased.
 Additional linear bush constraint the position and contribute better reproducibility.

Wire bonding

- Comparison of Pull Strength by *Ni* Thickness
 - Tokai-Densi Co., PA1&2 manufacturing company, provide two samples for the checking of bondability
 - Sample **A**: Cu 3-5 μm , **Ni 1 μm** , Au 0.05-0.1 μm
 - Sample **B**: Cu 3-5 μm , **Ni 3-5 μm** , Au 0.05-0.1 μm
 - Tokai-Densi prefers the Sample A since better yield.

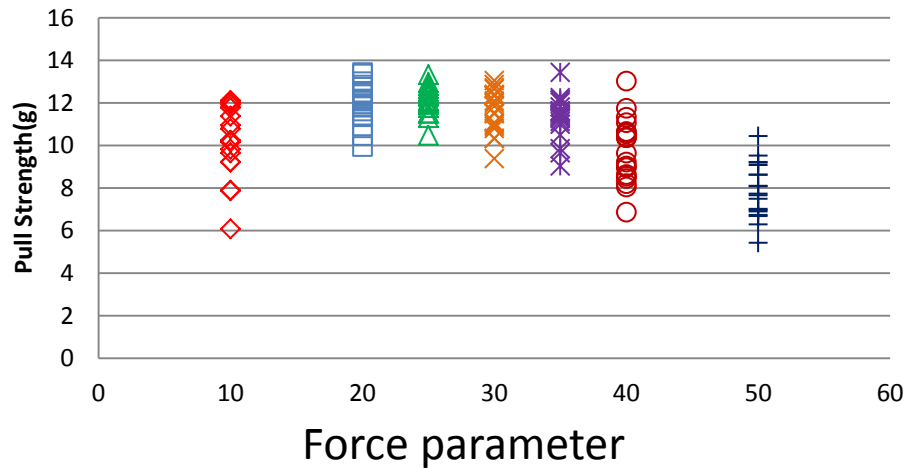


- Wire bonding and pull test was performed to compare with the bondabilities of sample A and B

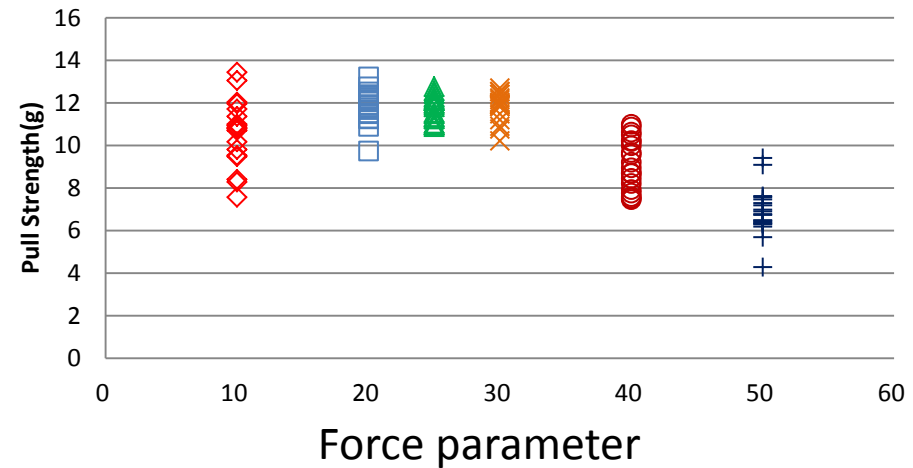
Wire bonding result

After the bonding parameter of power was tuned at 60 to maximum pull strength

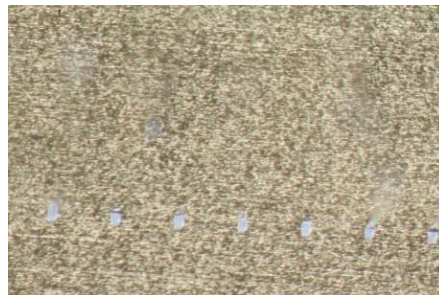
Sample A: Ni=1 μ m



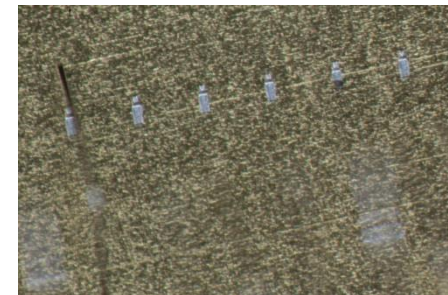
Sample B: Ni=3-5 μ m



Bond foot at Force 25



Bond foot at Force 25



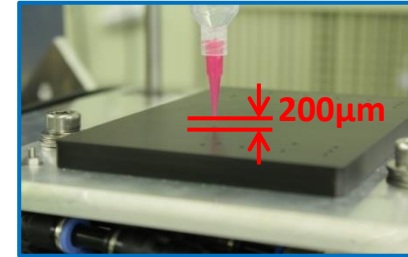
It looks not so different and both usable.

We can accept request of Sample A from manufacturing company.

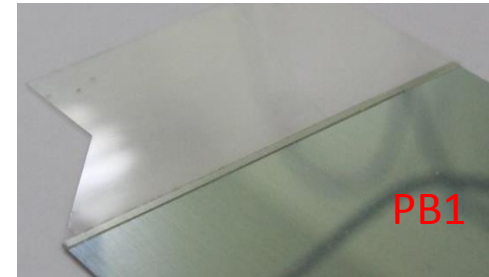
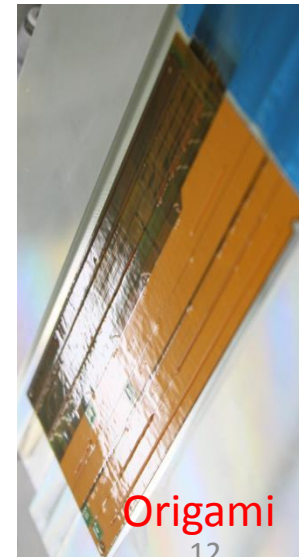
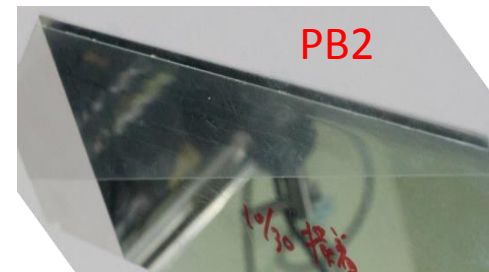
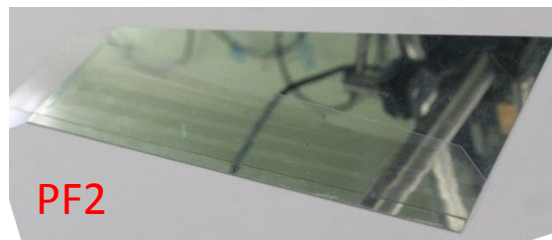
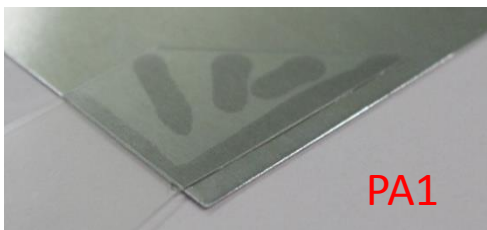
Glue dispensing study

Tuned basic parameters

- Glue : Araldite2011(50ml cartridge)
- Temperature of lab-room : $23 \pm 1^\circ\text{C}$
- Air pressure : 0.4MPa
- Nozzle : Plastic tapered nozzle. Inner diameter 0.25mm, SH25TT-B
- Clearance between the tip of nozzle and the surface : $200 \pm 18\mu\text{m}$
- Dispensing speed : 20mm/s for wire bonding part.
- Centrifugal machine : AW-20-3 (rpm=2575) for 400sec
- Time to start dispensing after the mixing: 15 min(incl. test dispensing)



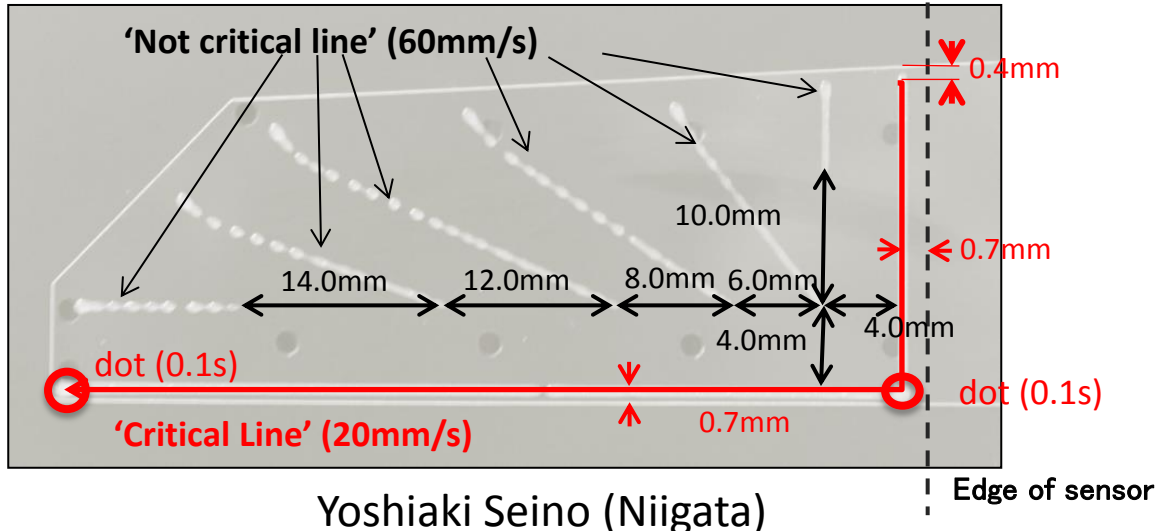
Dispensing patterns



Dispensing parameter and pattern

Two sets of glue dispensing parameters:

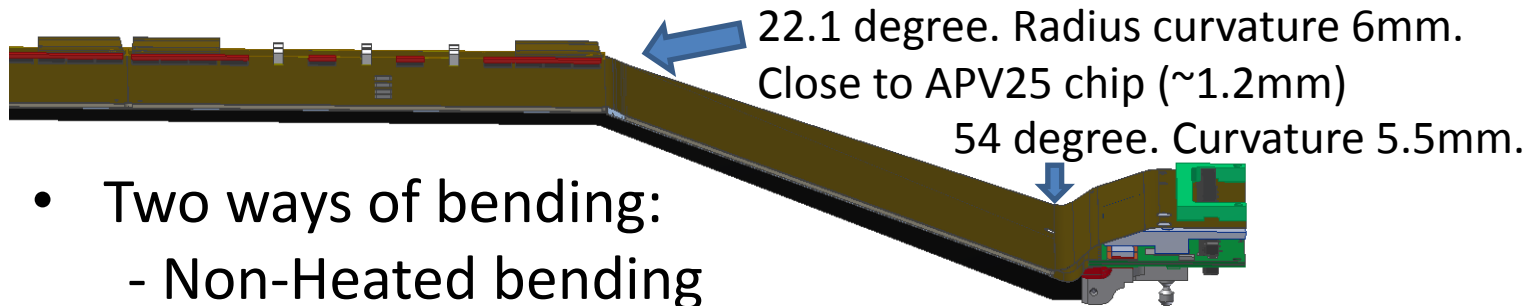
- **Area underneath wire bonding pads**
 - Critical for bondability. → **Should spend much time for better bondability.**
 - Typically small area
 - Should be dispensed uniformly and precisely
- The other area
 - Not critical for bondability
 - Typically larger area
 - Should be faster to cover large area. Viscosity change in a few 10 minutes.



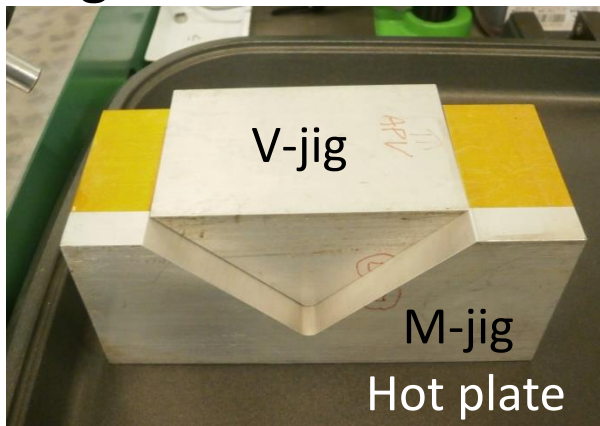
Pre-bending of Origami+z

- Only L6 matter.

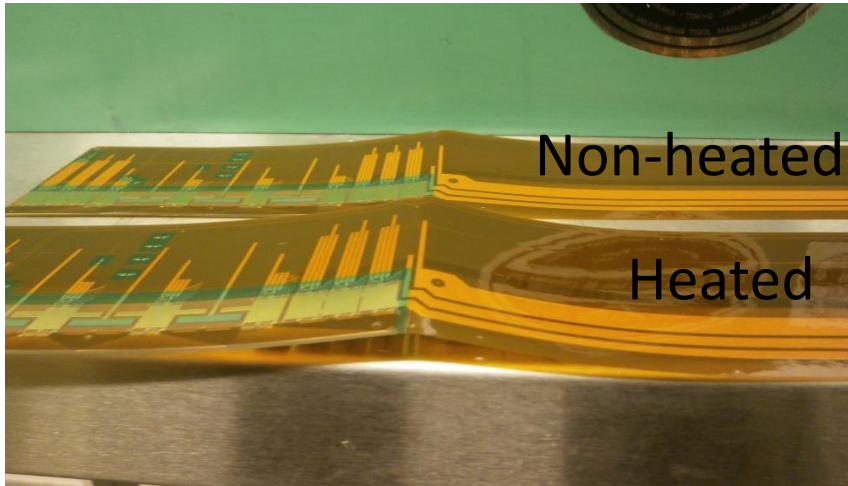
Should be bended before SMDs implementation



- Two ways of bending:
 - Non-Heated bending
 - Heated bending
- Bending jigs: V-jig and M-jig
designed and wire-cut from Al block by Sato-san.



Pre-bending of Origami+z



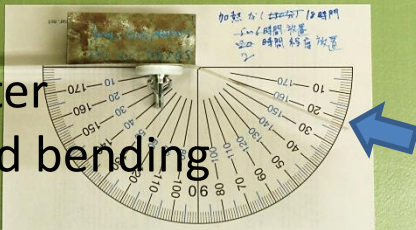
- Two ways were compared. Heated bending way is hard to be restored compared with non-heated bending way.

20 hours after heated bending



- Though we met difficulty that the bending is restored after the reflow of SMDs, we found the sample heated by hot plate setting at 260°C and bended is not restored after the reflow.

2 hours after non-heated bending (18 hours)



Plan

Ladder assembly meeting at IPMU 4th Feb.

- Production drawing of parts and jigs.
- Assembly procedure incl. gluing, bonding
- FW&BW assembly procedure
- Mech. & Elec. QA procedure...

Let's discuss what items we'll discuss at the meeting.

Items

Commissioning Elec.QA setup at IPMU

Implementation Elec. QA in the assy proc.

Study of trans/rotation w/ Mech.QA

Release of revised jigs

Manufacturing the jigs

Finalizing pre-bending procedure

Gluing study of wrapped PA

Wire-bonding study of the wrapped PA.

Mockup assembly

	Feb	Mar	Apr	May
Commissioning Elec.QA setup at IPMU	■			
Implementation Elec. QA in the assy proc.		■	■	■
Study of trans/rotation w/ Mech.QA	■			
Release of revised jigs	■			
Manufacturing the jigs	■	■	■	■
Finalizing pre-bending procedure	■			
Gluing study of wrapped PA		■	■	
Wire-bonding study of the wrapped PA.		■	■	■
Mockup assembly	■	■	■	■