

Measurements Uncertainties in VTS (at Fermilab).

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Abstract

We discuss source of errors in Q and E measurements during testing of SRF cavity in VTS (at Fermilab, as an example).

Melnychuk's error propagation analysis

SRF2013 THP095 (to follow by expanded paper

O. Melnychuk “*Error analysis for vertical test stand cavity measurements at Fermilab*”, submitted to PRSTAB)

See also Fermilab Tech Report TD-13-010

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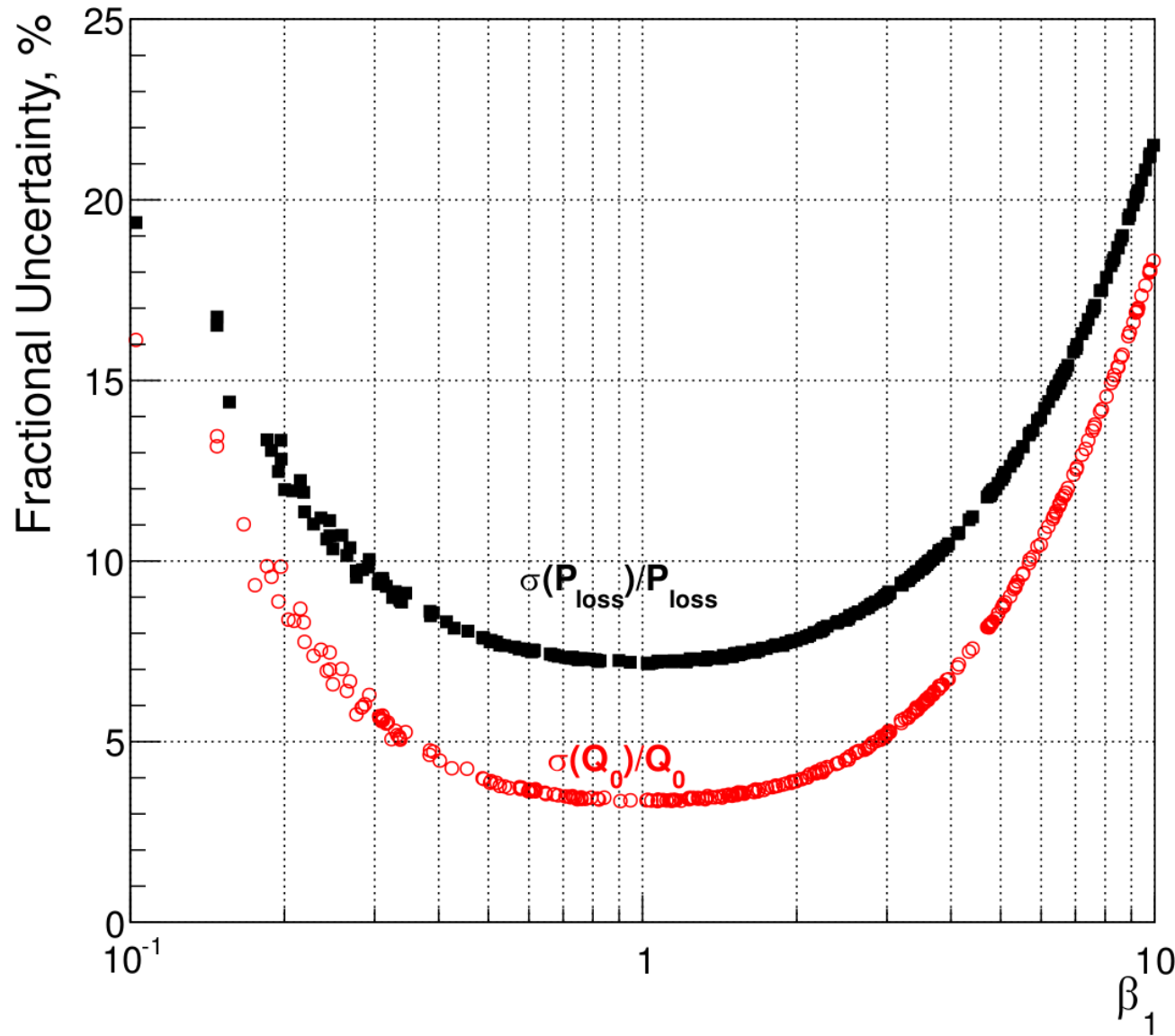
Follows and refines Tom Powers work (see e.g. SRF2011). More careful treatment of correlations between cable calibration, decay measurements, and actual CW measurements.

Melnychuk's error propagation analysis

Input uncertainties:

- Power meter sensitivity 1 nW
- Power meter precision 4.2%
- Operator error 3%
- Cable losses
 - Forward / Reflected 5%
 - Transmitted 0%
- Decay constant 3%

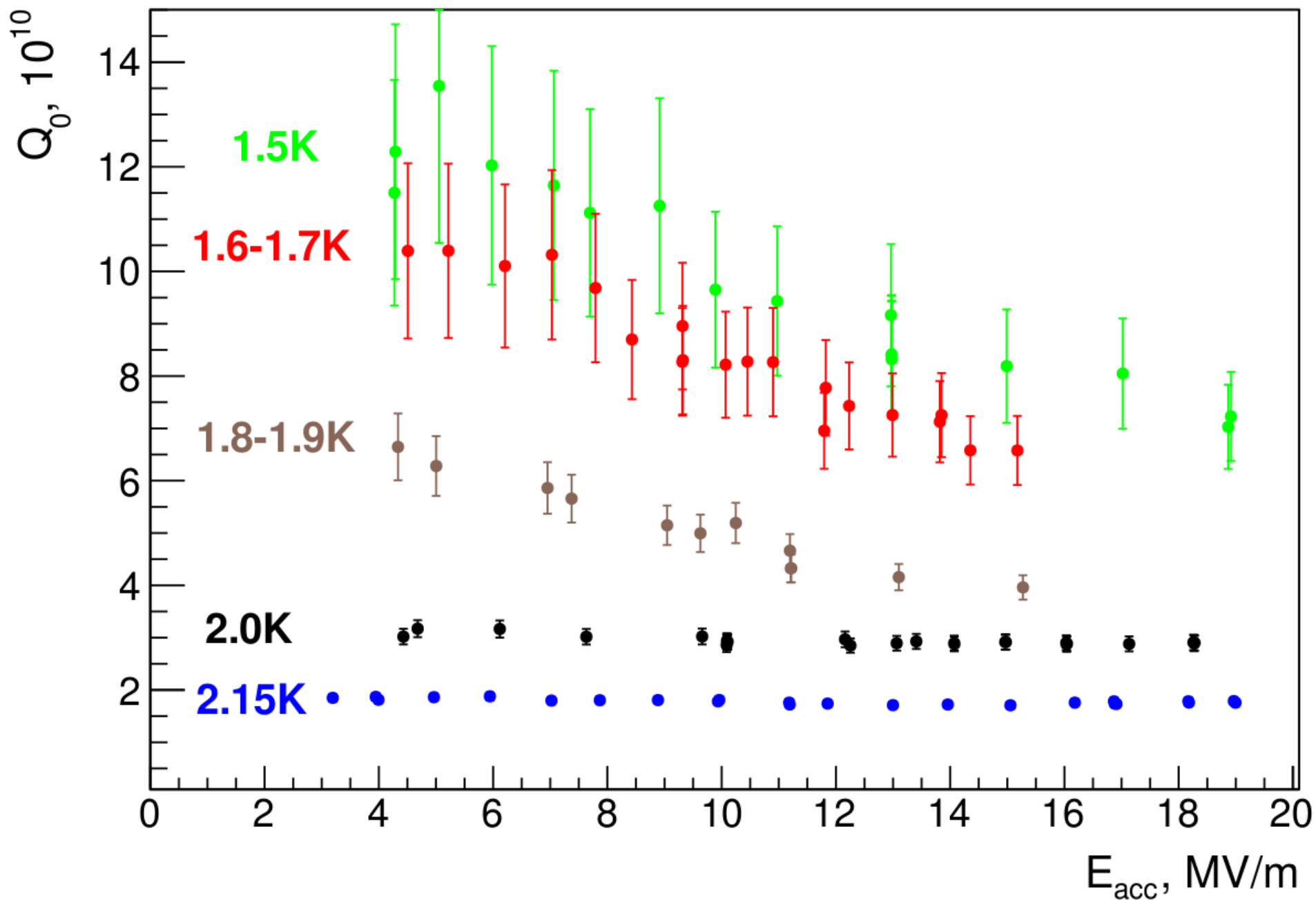
Melnychuk's error propagation analysis



For $0.5 < \beta_1 < 2.5$ $\delta Q/Q$
and $\delta E/E \sim 4\%$
(constant)

Main difference from Tom Powers' work:

- $\delta E/E$ does not depend on E
- $\delta Q/Q$ is about 2x smaller



Test of te1nr005 cavity on March 2013 on VTS1 at Fermilab.
 $\beta_1 \sim 2$ @2.15K, ~ 10 @1.5K

Directional coupler issues

Instigated by Warren Schappert (warren@fnal.gov). Still work in progress.

Directional coupler

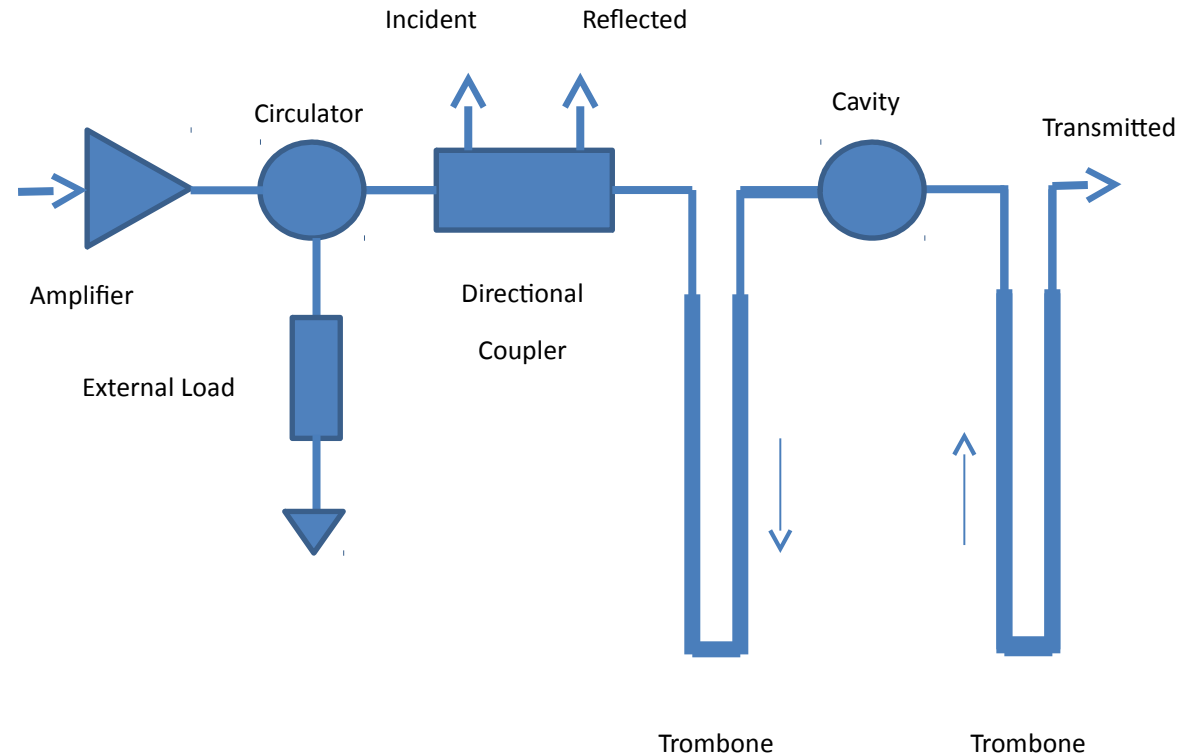
- Coupler directivity is a measure of cross-talk between the forward and reflected signals
- Trade-off between frequency response and directivity
 - Wide bandwidth => low directivity
 - High bandwidth => narrow bandwidth
- Coupler directivity can be modeled as linear mixing between the forward and reflected signals

Appendix: Directional Coupler Comparison

	Coupler		
Manufacturer	RF-Lambda	Agilent	<u>Flann</u>
Model	RFDDC1M2G20	776D	11A113
Style	Coaxial	Coaxial	Waveguide
<u>f_{Min}</u>	0.11	0.9	3.30
<u>f_{Max}</u>	2.0	1.1	4.90
Coupling	20	40	20
Insertion Loss	0.5	0.3	
Power	500	50	
Directivity	22	40	50

Experimental Setup

- Two back-to-back trombones
- Vary the length of the cable between coupler and cavity
 - Changes relative phase between forward and reflected signals
 - Phase between forward and probe remains unchanged



“Trombone”: GR874-LT Constant Impedance Variable Length Coaxial Air Line



default view | autostep | pulse

ILC 1 Cell Backup Files

HOM configuration: Zero Pwr Meters

No HOMs zero successful? YES

Cavity Ser Num TE1ACC005 Calibrate Cables

Kappa 88.47 Change RF Source

Clear Graph

data file name
TE1ACC005Q.TXT

Meas Temp

Dewar Temp from Pres [K] 4.41

Dewar Pres 0-100 Torr 105.9

Dewar Pres 0-1000 Torr 902.7

TCavTop [K] 2.243

TCavUpMid [K] 2.272

TCavLoMid [K] 2.225

TCavBot [K] 2.228

last logged point | live numbers

CW measurements

Pinc 0.534 [W]

Pref 0.001 [W]

Ptran 0.011 [W]

Ploss 0.523 [W]

P HOM A 1.00E-12 [W]

P HOM B 1.00E-12 [W]

Qo - CW 7.30E+9

Eacc - CW 5.47 [MV/m]

Frequency 1.301213978E+9 [Hz]

FREQUENCY SELECTOR
1.3GHz

RF Control

Atten (dB) 0.00

Theta [deg] 252.8

Set mixer level

Measure & Log CW

Dwell time [s] 2.000

Optimize Phase

Atten increment 0.10

B < 1 undercoupled | Coupling | B > 1 overcoupled

STATE 1 CONTROL

cur state

Acquire CW Data

Radiation vs. Time

Rad 1.27E-2 mR/hr Mute Rad Alarm

Enter Qext2 from decay meas.

Qext2 3.57E+11

% error 13.20

running

STOP

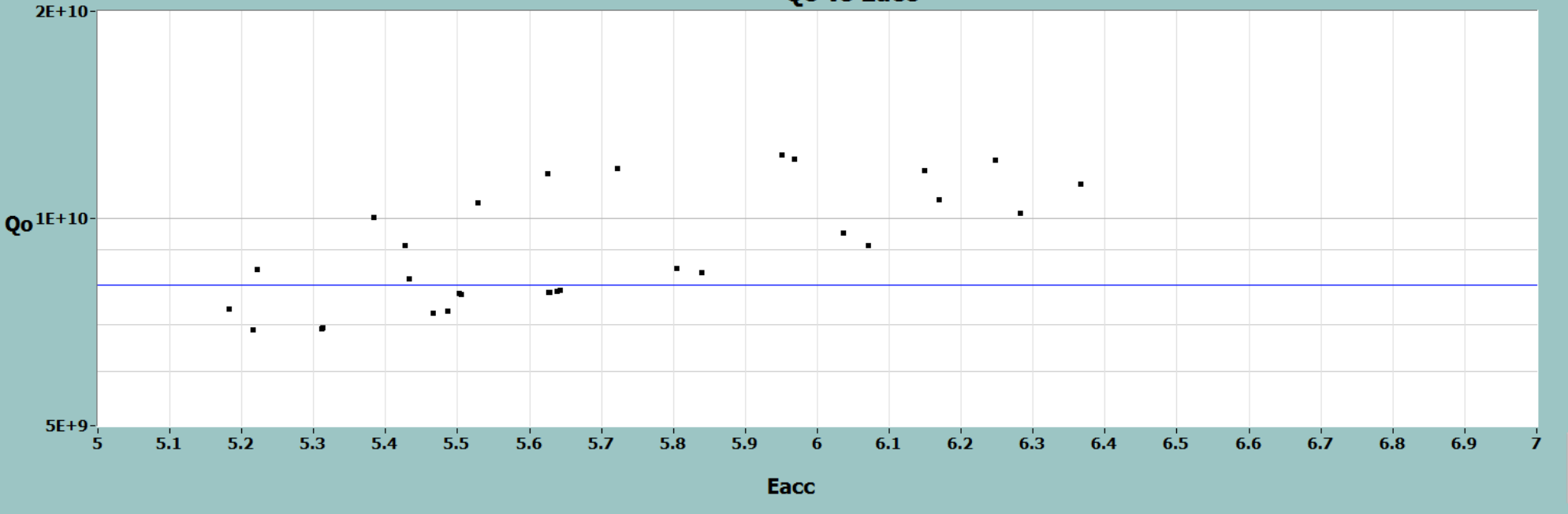
TOTAL PHASE

255.10

ATTN 16.00

Last Tau 9.29E-1

LNA status





default view autostep pulse

ILC 1 Cell Backup Files

HOM configuration: Zero Pwr Meters

No HOMs zero successful? YES

Cavity Ser Num Calibrate Cables

TE1ACC005 Change RF Source

Kappa Clear Graph

88.47

data file name

TE1ACC005Q.TXT

Meas Temp

Dewar Temp from Pres [K] 4.41

Dewar Pres 0-100 Torr 105.9

Dewar Pres 0-1000 Torr 903.2

TCavTop [K] 2.258

TCavUpMid [K] 2.288

TCavLoMid [K] 2.236

TCavBot [K] 2.238

last logged point live numbers

CW measurements

Pinc 0.525 [W]

Pref 0.018 [W]

Ptran 0.010 [W]

Ploss 0.497 [W]

P HOM A 1.00E-12 [W]

P HOM B 1.00E-12 [W]

Qo - CW 7.52E+9

Eacc - CW 5.41 [MV/m]

Frequency 1.301213968E+9 [Hz]

FREQUENCY SELECTOR

1.3GHz

RF Control

Atten (dB) 0.00

Theta [deg] 252.8

Set mixer level

Measure & Log CW

Dwell time [s] 2.000

Optimize Phase

Atten increment 0.10

B < 1 undercoupled Coupling B > 1 overcoupled

STATE 1 CONTROL

cur state

Calibrate

Radiation vs. Time

11:34:28 AM 7:34:28 PM

Decay_Folder

C:\data\Decay

Rad 1.20E-2 mR/hr Mute Rad Alarm

Enter Qext2 from decay meas.

Qext2 3.57E+11

% error 13.20

running

STOP

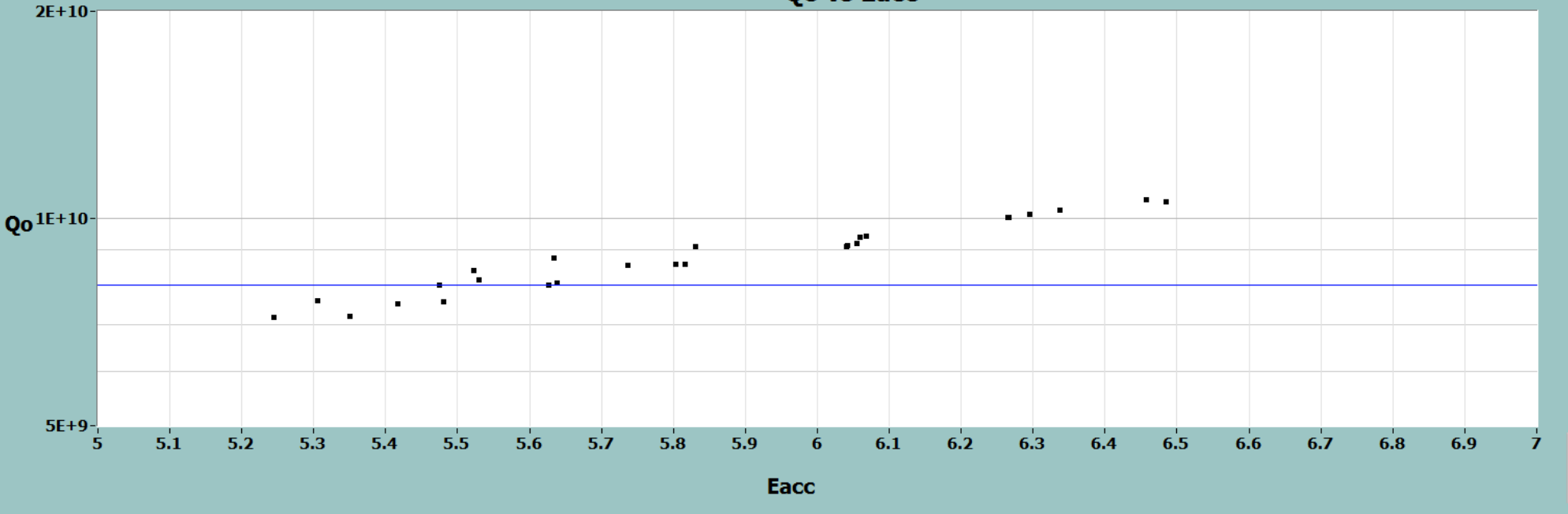
TOTAL PHASE

255.10

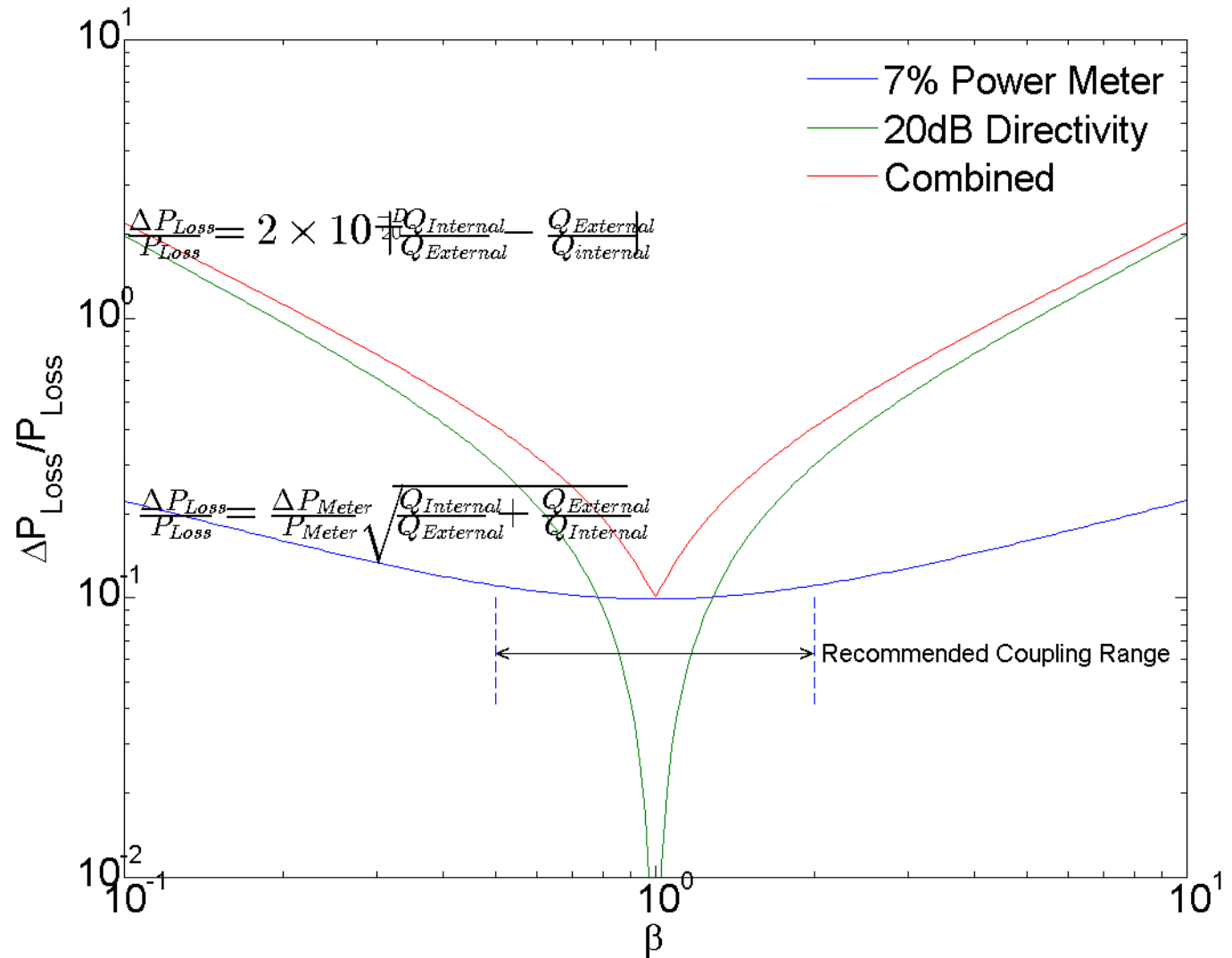
ATTN 16.00

Last Tau 9.29E-1

LNA status ON



Directivity Errors



Conclusion (W.S.)

The upgrades to the VTS in order of importance are (in my opinion)

- 1) A variable power coupler.
- 2) A high directivity directional coupler
- 3) A digital I/Q system.

The power coupler is by far the most important.

A high directivity coupler will improve both analog power and complex digital measurements but the power meter limits will still dominate in the analog case. The digital I/Q system in combination with a high directivity coupler provides sufficient information to determine the relative calibration of the forward, probe and reflected signals from the data itself. No measurements of or corrections for cable loss are required. This results in a significant reduction in the systematic uncertainties.

With a poor directivity coupler it is difficult to separate contamination in the coupler from reflections from the circulator even with a digital system. A trombone can resolve that ambiguity.

Projected VTS Systematic Error Limits

